# 304 TODD ROAD PROJECT AIR QUALITY AND GREENHOUSE GAS EMISSIONS ASSESSMENT 

## Sonoma County, California

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Prepared for:
Mr. Thomas Smith
Estimating Manager
Ghilotti Construction Company, Inc.
246 Ghilotti Avenue
Santa Rosa, CA 95407

Prepared by:
James A. Reyff and Bill Popenuck

ILLINGWORTH\& RODKIN,INC.
|IIII Acoustics • Air Quality IIII/
1 Willowbrook Court, Suite 120
Petaluma, CA 94954
(707) 794-0400

## January 2018 Revision

This report was revised in January 2018 to increase the amount of material processed through crushing operations to 50,000 cubic yards per year. The 2016 analysis addressed crushing air quality impacts as "The processing of base rock materials would be in the range of 25,000 tons annually." However, the analysis of crushing operations assumed 44 days for 8 hours per day that processed 100 tons per hour. This equates to 37,500 tons per year. In order to address a scenario that crushes 50,000 tons per year, crushing operations were increased to 63 days per year and truck trips were adjusted upward as well. Changes to the report with this revision are made in strikethrough where sections are deleted and underline where additions are made.

## Introduction

Ghilotti Construction Company, Inc. currently uses the property located at 304 Todd Road, in unincorporated Sonoma County, as a temporary contractor's equipment storage site, stockpile location for rock rip-rap material, and processing site for broken asphalt and concrete materials for recycling and reuse purposes as base rock. There are large stockpiles of soil on the southern half of the property. Ghilotti Construction Company, Inc. has submitted an application to bring the current use into compliance, pursuant to the Notice of Violation received from the County PRMD dated August 9, 2011.

The purpose of this study is to evaluate air quality impacts and greenhouse gas (GHG) emissions attributable to project operations with regard to criteria established by the Sonoma County General Plan and guidance recommended in the Bay Area Air Quality Management District's 2011 CEQA Air Quality Guidelines. The project does not require any construction activities to begin operation; therefore, this analysis addresses operational impacts. These impacts include air pollutant and GHG emissions from on-site equipment operation and vehicles using the project site. Localized impacts from emissions of toxic air contaminants (i.e., diesel particulate matter) and fine particulate matter or $\mathrm{PM}_{2.5}$, are assessed at nearby sensitive receptors.

## Project Description

Currently, the project site is used in the following ways:

1. Temporary contractor's equipment storage site
2. Stockpile location for rock rip-rap material and
3. Processing site for broken asphalt and concrete materials to recycle and reuse as base rock.

The project proposes to obtain a use permit, per the allowed zoning uses of MI Limited Rural Industrial District, for which the project site is zoned. This application is to bring the current use into compliance pursuant to the Notice of Violation received from the County PRMD dated August 9, 2011.

## Equipment Storage

The use for equipment storage is intermittent as there is an existing equipment storage yard across the access road to the east that primarily stores equipment. Equipment storage at the project site would be temporary for equipment that will be transported from projects nearby until they can be transported to the next project location. Minor equipment repairs may take place at the project site.

## Material Processing and Stockpiling

Material processing at the project site would be multi-functional. Storage of rock rip-rap for reuse on projects will take place from time to time as will the off-haul of the rock rip-rap to project sites. Stockpiling and processing of asphalt grindings, concrete and base rock materials would occur occasionally. Processing of these materials will be for trucking to and re-use in on-going countywide projects. Both stockpiling and processing of materials is on an as needed basis. Stockpiling of the materials on site will occur during the week and on Saturdays between the hours of 7:00 AM to 6:00 PM.

Processing of the materials would involve the use of a portable crushing plant powered by a diesel engine and a diesel powered front end loader. The processing of base rock materials would be in the range of $25,00050,000$ tons annually. Diesel-powered heavy-duty trucks (e.g., semi-end dumps, semi-bottom dumps and transfer trailers) would be used to truck the material to and from the project site. The number of trips per day will vary based the time of year and on import and export of the materials. The estimated range of trips would be from 0 to 50 per day. There would be no trips when processing/crushing, about $10-15$ trips per day when hauling in material to process, and 20-30 trips per day to haul material from the project site.

Site appearance will change from time to time as materials are stockpiled, processed and hauled off site. There are large stockpiles of material on the southern half of the property. These stockpiles are currently slated for the fill required on the adjacent Shamrock Property. The stockpiles would be protected from erosion using the erosion and sediment controls as described in the storm water management plan. The largest stockpile at the southerly portion of the project site consists of processed material that is weathered and covered with vegetation. Unprocessed material is typically course material in the form of broken asphalt or concrete.

## Air Quality Setting

The project is located in the Bay Area portion of Sonoma County, which is in the San Francisco Bay Area Air Basin. Ambient air quality standards have been established at both the State and federal level. The Bay Area meets all ambient air quality standards with the exception of groundlevel ozone, respirable particulate matter $\left(\mathrm{PM}_{10}\right)$, and fine particulate matter $\left(\mathrm{PM}_{2.5}\right)$.

High ozone levels are caused by the cumulative emissions of reactive organic gases (ROG) and nitrogen oxides $\left(\mathrm{NO}_{\mathrm{x}}\right)$. These precursor pollutants react under certain meteorological conditions to form high ozone levels. Controlling the emissions of these precursor pollutants is the focus of the Bay Area's attempts to reduce ozone levels. The highest ozone levels in the Bay Area occur
in the eastern and southern inland valleys that are downwind of air pollutant sources. High ozone levels aggravate respiratory and cardiovascular diseases, reduced lung function, and increase coughing and chest discomfort.

Particulate matter is another problematic air pollutant of the Bay Area. Particulate matter is assessed and measured in terms of respirable particulate matter or particles that have a diameter of 10 micrometers or less $\left(\mathrm{PM}_{10}\right)$ and fine particulate matter where particles have a diameter of 2.5 micrometers or less $\left(\mathrm{PM}_{2.5}\right)$. Elevated concentrations of $\mathrm{PM}_{10}$ and $\mathrm{PM}_{2.5}$ are the result of both region-wide (or cumulative) emissions and localized emissions. High particulate matter levels aggravate respiratory and cardiovascular diseases, reduce lung function, increase mortality (e.g., lung cancer), and result in reduced lung function growth in children.

Toxic air contaminants (TAC) are a broad class of compounds known to cause morbidity or mortality (usually because they cause cancer) and include, but are not limited to, the criteria air pollutants. TACs are found in ambient air, especially in urban areas, and are caused by industry, agriculture, fuel combustion, and commercial operations (e.g., dry cleaners). TACs are typically found in low concentrations, even near their source (e.g., diesel particulate matter (DPM) near a freeway). Because chronic exposure can result in adverse health effects, TACs are regulated at the regional, State, and federal level.

Diesel exhaust is the predominant TAC in urban air and is estimated to represent about threequarters of the cancer risk from TACs (based on the Bay Area average). According to the California Air Resources Board (CARB), diesel exhaust is a complex mixture of gases, vapors, and fine particles. This complexity makes the evaluation of health effects of diesel exhaust a complex scientific issue. Some of the chemicals in diesel exhaust, such as benzene and formaldehyde, have been previously identified as TACs by the CARB, and are listed as carcinogens either under the state's Proposition 65 or under the Federal Hazardous Air Pollutants programs.

## Regulatory Setting

The U.S. Environmental Protection Agency (U.S. EPA) is responsible for enforcing the federal Clean Air Act and the 1990 amendments to it, as well as the national ambient air quality standards (federal standards) that the U.S. EPA establishes. These standards identify levels of air quality for six criteria pollutants, which are considered the maximum levels of ambient air pollutants considered safe, with an adequate margin of safety, to protect public health and welfare. The six criteria pollutants are ozone $\left(\mathrm{O}_{3}\right)$, carbon dioxide $\left(\mathrm{CO}_{2}\right)$, nitrogen dioxide $\left(\mathrm{NO}_{2}\right)$, sulfur dioxide $\left(\mathrm{SO}_{2}\right)$, respirable particulate matter with an aerodynamic diameter of 10 micrometers ( $\mathrm{PM}_{10}$ ), fine particulate matter with an aerodynamic diameter of 2.5 micrometers $\left(\mathrm{PM}_{2.5}\right)$, and lead ( Pb ). The U.S. EPA also has regulatory and enforcement jurisdiction over emission sources beyond State waters (outer continental shelf) and sources that are under the exclusive authority of the federal government, such as aircraft, train locomotives, and interstate trucking. As part of its enforcement responsibilities, the U.S. EPA requires each State with nonattainment areas (i.e., areas that do not meet national ambient air quality standards) to prepare and submit a State Implementation Plan (SIP) that demonstrates the means to attain the federal standards. The SIP must integrate federal,

State, and local plan components and regulations to identify specific measures to reduce pollution in nonattainment areas, using a combination of performance standards and market-based programs.

The CARB, a department of the California EPA, oversees air quality planning and control throughout California. It is primarily responsible for ensuring implementation of the 1989 amendments to the California Clean Air Act (CCAA), responding to the federal Clean Air Act Amendment requirements, and regulating emissions from motor vehicles and consumer products within the state. CARB has established emission standards for vehicles sold in California and for various types of equipment available commercially. It also sets fuel specifications to further reduce vehicular emissions and develops airborne toxic control measures to reduce TACs identified under CARB regulations.

Both the U.S. EPA and CARB established ambient air quality standards for common air pollutants. These ambient air quality standards are prescribed levels of pollutants that represent safe levels that avoid specific adverse health effects associated with each pollutant. The ambient air quality standards cover what are called "criteria" pollutants because the health and other effects of each pollutant are described in criteria documents. The federal and State ambient standards were developed independently with differing purposes and methods, although both processes attempted to avoid health-related effects. As a result, federal and State standards differ in some cases. In general, California standards are more stringent. This is particularly true for ozone and $\mathrm{PM}_{10}$. The BAAQMD is the regional agency tasked with managing air quality in the region. At the State level, the CARB oversees regional air district activities and regulates air quality at the State level. The BAAQMD has published the California Environmental Quality Act (CEQA) Air Quality Guidelines that are used in this assessment to evaluate air quality impacts of projects. ${ }^{1}$

## Sensitive Receptors

There are groups of people more affected by air pollution than others. CARB has identified the following persons who are most likely to be affected by air pollution: children under 16, the elderly over 65, athletes, and people with cardiovascular and chronic respiratory diseases. These groups are classified as sensitive receptors. Locations that may contain a high concentration of these sensitive population groups include residential areas, hospitals, daycare facilities, elder care facilities, elementary schools, and parks. The closest sensitive receptors are as follows:

- A single-family residence located immediately west of the equipment storage site (about 80 feet west);
- Six single-family residences located along Langner Avenue west, southwest, and south of the site (over 400 feet to the west and southwest); and
- Single family residences opposite Todd Road to the north of the site (approximately 300 feet or further to the north)

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## Greenhouse Gases - Setting

Gases that trap heat in the atmosphere, GHGs, regulate the earth's temperature. This phenomenon, known as the greenhouse effect, is responsible for maintaining a habitable climate. The most common GHGs are carbon dioxide and water vapor but there are also several others, most importantly methane $\left(\mathrm{CH}_{4}\right)$, nitrous oxide ( $\mathrm{N}_{2} \mathrm{O}$ ), hydrofluorocarbons (HFCs), perfluorocarbons (PFCs), and sulfur hexafluoride ( $\mathrm{SF}_{6}$ ). These are released into the earth's atmosphere through a variety of natural processes and human activities. Sources of GHGs are generally as follows:

- Carbon dioxide and nitrous oxide are byproducts of fossil fuel combustion.
- Nitrous oxide is primarily associated with agricultural operations such as fertilization of crops.
- Methane is commonly created by off-gassing from agricultural practices (e.g., keeping livestock) and landfill operations.
- Chlorofluorocarbons were widely used as refrigerants, propellants, and cleaning solvents but their production has been reduced by international treaty.
- Hydrofluorocarbons are now used as a substitute for chlorofluorocarbons in refrigeration and cooling.
- Perfluorocarbons and sulfur hexafluoride emissions are commonly created by industries such as aluminum production and semi-conductor manufacturing.

Each GHG has its own potency and effect upon the earth's energy balance. This is expressed in terms of a global warming potential (GWP), with carbon dioxide being assigned a value of 1 and sulfur hexafluoride being several orders of magnitude stronger with a GWP of 23,900. In GHG emission inventories, the weight of each gas is multiplied by its GWP and is measured in units of carbon dioxide equivalents $\left(\mathrm{CO}_{2} \mathrm{e}\right)$.

An expanding body of scientific research supports the theory that global warming is currently affecting changes in weather patterns, average sea level, ocean acidification, chemical reaction rates, and precipitation rates, and that it will increasingly do so in the future. The climate and several naturally occurring resources within California could be adversely affected by the global warming trend. Increased precipitation and sea level rise could increase coastal flooding, saltwater intrusion, and degradation of wetlands. Mass migration and/or loss of plant and animal species could also occur. Potential effects of global climate change that could adversely affect human health include more extreme heat waves and heat-related stress; an increase in climate-sensitive diseases; more frequent and intense natural disasters such as flooding, hurricanes, and drought; and increased levels of air pollution.

## Significance Thresholds

In June 2010, BAAQMD adopted thresholds of significance to assist in the review of projects under CEQA. These Thresholds were designed to establish the level at which BAAQMD believed air pollution emissions would cause significant environmental impacts under CEQA and were posted on BAAQMD's website and included in the Air District's updated CEQA Guidelines (updated May 2011). The significance thresholds identified by BAAQMD and used in this analysis are summarized in Table 1.

BAAQMD's adoption of significance thresholds contained in the 2011 CEQA Air Quality Guidelines was called into question by an order issued March 5, 2012, in California Building Industry Association (CBIA) v. BAAQMD (Alameda Superior Court Case No. RGI0548693). The order requires BAAQMD to set aside its approval of the thresholds until it has conducted environmental review under CEQA. The ruling made in the case concerned the environmental impacts of adopting the thresholds and how the thresholds would indirectly affect land use development patterns. In August 2013, the Appellate Court struck down the lower court's order to set aside the thresholds. However, the California Supreme Court accepted a portion of CBIA's petition to review the appellate court's decision to uphold BAAQMD's adoption of the thresholds. The specific portion of the argument considered was whether CEQA requires consideration of the effects of the environment on a project (as contrasted to the effects of a proposed project on the environment). On December 17, 2015, the California Supreme Court ruled that CEQA generally does not require an analysis of the effects of existing environmental conditions (e.g., air quality) on a project unless the project would exacerbate those conditions somehow through its construction and/or operation. The effects of the existing environment upon the project are not addressed in this analysis.

Table 1. Air Quality Significance Thresholds

| Criteria Air Pollutant | Average Daily Emissions (lbs./day) | Average Daily Emissions (lbs./day) | Annual Average Emissions (tons/year) |
| :---: | :---: | :---: | :---: |
| ROG | 54 | 54 | 10 |
| $\mathrm{NO}_{\mathrm{x}}$ | 54 | 54 | 10 |
| $\mathrm{PM}_{10}$ | 82 (Exhaust) | 82 | 15 |
| $\mathrm{PM}_{2.5}$ | 54 (Exhaust) | 54 | 10 |
| CO | Not Applicable | 9.0 ppm (8-hr avg) or 20.0 ppm (1-hr avg) |  |
| Fugitive Dust | Construction Dust Ordinance or other Best Management Practices | Not Applicable |  |
| Health Risks and Hazards | Single Sources Within 1,000-foot Zone of Influence | Combined Sources (Cumulative from all sources within 1,000-foot zone of influence) |  |
| Excess Cancer Risk | $>10$ per one million | $>100$ per one million |  |
| Hazard Index | $>1.0$ | $>10.0$ |  |
| Incremental annual $\mathrm{PM}_{2.5}$ | $>0.3 \mu \mathrm{~g} / \mathrm{m}^{3}$ | $>0.8 \mu \mathrm{~g} / \mathrm{m}^{3}$ |  |
| Greenhouse Gas Emissions |  |  |  |
| Land use Projects | Compliance with a Qualified GHG Reduction Strategy OR 1,100 metric tons OR 4.6 metric tons/capita annually |  |  |
| Permitted Sources (e.g., stacks) | 10,000 metric tons annually |  |  |

## Impact 1: Conflict with or obstruct implementation of the applicable air quality plan? Less-than-significant.

The Bay Area Air Quality Management District (BAAQMD) is the regional agency responsible for overseeing compliance with State and Federal laws, regulations, and programs within the San Francisco Bay Area Air Basin. The BAAQMD, with assistance from the Association of Bay Area Governments and the Metropolitan Transportation Commission has prepared and implements specific plans to meet the applicable laws, regulations, and programs. Among them are the Carbon Monoxide Maintenance Plan (1994), the 2001 Ozone Attainment Plan, and the Bay Area 2010 Clean Air Plan. The BAAQMD has also developed CEQA guidelines to assist lead agencies in evaluating the significance of air quality impacts. In formulating compliance strategies, BAAQMD relies on planned land uses established by local general plans. When a project proposes to change planned uses, by requesting a general plan amendment for example, the project may depart from the assumptions used to formulate plans and compliance strategies in such a way that the cumulative result of incremental changes may hamper or prevent BAAQMD from achieving its goals. This is because land use patterns influence transportation needs, and motor vehicles are the primary source of air pollution. The most recent Clean Air Plan is the Bay Area 2010 Clean Air Plan that was adopted by BAAQMD in September 2010. The proposed project would not conflict with the latest Clean Air planning efforts since; 1) the project is consistent with the zoning and development intensity considered in the County's General Plan, 2) the project would have emissions below the BAAQMD criteria pollutant thresholds (see Impact 2), and 3) The proposed project would not cause changes to local population projections or regional changes in vehicle use. The project does not conduct any operations on-site that are subject to BAAQMD regulations, since the crushing operations are conducted on only 44 days per year or less and the equipment is considered portable. The project employs measures to reduce dust emissions from ground disturbances, crushing operations and management of soil/aggregate material.

## Impact 2: Violate any air quality standard or contribute substantially to an existing or projected air quality violation? Less than Significant

The Bay Area is considered a non-attainment area for ground-level ozone and $\mathrm{PM}_{2.5}$ under both the Federal Clean Air Act and the California Clean Air Act. The area is also considered nonattainment for $\mathrm{PM}_{10}$ under the California Clean Air Act, but not the federal act. The area has attained both State and federal ambient air quality standards for carbon monoxide. As part of an effort to attain and maintain ambient air quality standards for ozone and $\mathrm{PM}_{10}$, the BAAQMD has established thresholds of significance for these air pollutants and their precursors. These thresholds are for ozone precursor pollutants (ROG and $\mathrm{NO}_{\mathrm{x}}$ ), $\mathrm{PM}_{10}$, and $\mathrm{PM}_{2.5}$ and apply to both construction period and operational period impacts.

Ozone and particulate matter concentrations in the San Francisco Bay Area are the result of emissions (both inside and outside the air basin), meteorological conditions and complex chemical reactions that occur over time in the atmosphere. Recognizing that no single project is sufficient in size to, by itself, result in nonattainment of ambient air quality standards, BAAQMD has recommended emission-based thresholds that measure a project's contribution to cumulative emissions that could cause violations (or potential violations) of ambient air quality standards.

Ghilotti's operations at the project site result in emissions of air pollutants from the following operations:

- Fugitive dust from the handling, processing and transportation of material processed;
- Fugitive dust emissions from exposed stock piles
- Emissions from combustion equipment used on-site and to process recycled concrete and asphalt (e.g., crusher, loaders, bulldozers, excavators, grader, and forklift);
- Emissions from truck traffic generated by the site on a daily basis and trucks used to transport recyclable materials associated with crushing operations; and
- Worker traffic.


## Fugitive Dust Emissions

Average daily and maximum annual fugitive emissions of $\mathrm{PM}_{10}$ and $\mathrm{PM}_{2.5}$ from the project were computed based on the following assumptions:

1. Crushing Day - assuming a maximum processing rate of 100 tons of material per hour, for 8 hours or 800 tons of material processed per crushing day. Other off-road equipment operating during this period includes two loaders, two bulldozers, two excavators, and one grader.
2. Non-Crushing Day - the only fugitive dust sources during non-crushing days are from vehicle travel, assumed to occur 266 days per year, and wind erosion, assumed to occur 365 days per year.
3. Annual Emissions - based on $44 \underline{63}$ days of crushing and 222 days of no crushing, but ground disturbances.

Emissions were computed using emissions factors published by U.S. EPA in Chapter 11.19.2, Crushed Stone Processing and Pulverized Mineral Processing, Chapter 13.2.4, Aggregate Handling and Storage Piles. Chapter 11.9, Western Surface Coal Mining, and in Chapter 13.2.2, Unpaved Roads for vehicles traveling on unpaved surfaces at industrial sites of AP-42 (Fifth Edition, Volume I). These are the same factors BAAQMD Permit Handbook for Crushing and Grinding sources under Miscellaneous Sources ${ }^{2}$. The emissions factors included the effect of emissions control, based on facility actions and data by U.S. EPA (in AP-42, Volume I). These primarily include the effect of use of dust palliatives, watering, and reduced vehicle speeds.

The project would incorporate measures to minimize dust emissions that include routine application of a dust palliative to the general site as well as using water trucks during crushing and stockpile management operations. The crushing unit includes water spray bars that operate during crushing operations.
Sources of emissions computed from the crushing activity included a front loader feeding, crushing, screening, conveyor transfer points, loading or stockpiling, wind erosion of storage piles and disturbance from the front loaders and haul trucks. Other equipment used for crushing

[^1]activities and storage pile maintenance include bulldozers, excavators, and a grader. Daily and annual computed emissions along with emission factors and assumptions are provided in Attachment 1 of this letter.

## Exhaust Emissions

Exhaust emissions from the project were computed using the California Emissions Estimator Model (CalEEMod, Version 2016.3.1). This model was developed in collaboration with California air districts, including BAAQMD. This construction portion of this model was used to predict both on-site and combined on- and off-site emissions of ROG, NOx, PM10, PM2.5, and GHGs on an annual basis. Average daily emissions were computed by dividing the modeled annual emissions by the number of operational days, which is 266 days.

The land use category "Industrial Park" was selected in CalEEMod. Since CalEEMod requires a building size in units of 1,000 square feet, a size of " 1 " was entered. The project does not include any buildings. Since the construction portion of CalEEMod was used with project-specific inputs of equipment types and usage, the building size does not affect the results. The applicant provided a list of activity that generates air pollutant and GHG emissions in terms of on-site equipment usage and vehicle travel.

The construction phase "Site Preparation" was selected for construction modeling in CalEEMod. Two separate model runs were developed, one to represent daily activities over a 266-day period (one year) and one to represent on-site crushing activities that occur $44 \underline{63}$ days per year. On-site equipment usage assumptions, shown in Table 2, were input to the model.

The traffic report indicates that a maximum of 50 daily truck trips could occur. Based on information received from the applicant, an average of 15 trucks per day would use the site, resulting in 30 one-way trips. For on-site travel, these trips were assumed to have a distance of 0.25 miles. For off-site travel, the origin/destinations vary; therefore, the CalEEMod default distance of 20 miles for haul trips was used.

The computed annual and average daily emissions are reported in Table 3. These emissions are broken down by typical operations and crushing operations for both on- and off-site activities. Overall average daily emissions are the total emissions divided by the number of operating days (i.e., 266 days). Project annual and average daily emissions would be below the significance thresholds. Attachment 1 also includes the equipment usage assumptions and CalEEMod model output for the project.

Table 2 Equipment Usage Assumptions

| Qty | Description | Horsepower | Load <br> Factor | Engine Tier Level | Average Hrs/day |  | Avg. Hrs per day based on 260 days of operation |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily Activity |  |  |  |  |  |  |  |
| 4 | Air Compressors | 78 | 0.48 | 3 | 1 | 12 | 0.05 |
| 2 | Crawler Tractors | 208 | 0.43 | 3 | 1 | 52 | 0.20 |
| 2 | Excavators | 162 | 0.38 | 3 | 1 | 52 | 0.20 |
| 1 | Forklifts | 89 | 0.20 | 2 | 1 | 266 | 1.02 |
| 1 | Generator Sets | 84 | 0.74 | 3 | 4 | 22 | 0.34 |
| 1 | Other Material Handling Equipment | 167 | 0.40 | n/a | 1 | 52 | 0.20 |
| Crushing Activities |  |  |  |  |  |  |  |
| 2 | Rubber Tired Loaders | 199 | 0.36 | 3 | 8 | 4463 | 1.35 |
| 2 | Crawler Tractors | 208 | 0.43 | 3 | 8 | 4463 | 1.35 |
| 1 | Crushing/Proc. Equipment | 309 | 0.78 | 3 | 8 | 4463 | 1.35 |
| 2 | Excavators | 162 | 0.38 | 3 | 8 | 4463 | 1.35 |
| 1 | Graders | 174 | 0.41 | 3 | 4 | 4463 | 0.68 |

Table 3 Annual and Average Daily Project Emissions (on and off site)

| Description | Exhaust Emissions |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | ROG | NOx | PM10 | PM2.5 | GHG |
| Daily Operations (tons) | 0.0645 | 1.6307 | 0.0166 | 0.0160 | 345 MT |
| Crushing Operations (tons) | $\begin{aligned} & 0.0612 \\ & 0.0897 \end{aligned}$ | $\begin{aligned} & 1.3517 \\ & 2.0010 \end{aligned}$ | $\begin{aligned} & 0.0349 \\ & 0.0505 \end{aligned}$ | $\begin{aligned} & 0.0347 \\ & 0.0502 \end{aligned}$ | $\begin{aligned} & 284 \mathrm{MT} \\ & 420 \mathrm{MT} \end{aligned}$ |
| Fugitive Dust Emissions (tons) | -- | -- | $\begin{aligned} & 1.5524 \\ & 1.7568 \end{aligned}$ | 0.2471 0.2859 | -- |
| Total Annual Emissions (tons) | $\begin{aligned} & 0.1257 \\ & 0.1542 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.9824 \\ & 3.6317 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.6036 \\ & 1.8073 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.2978 \\ & 0.3361 \\ & \hline \end{aligned}$ | $\begin{aligned} & 629 \mathrm{MT} \\ & 765 \mathrm{MT} \\ & \hline \end{aligned}$ |
| Significance Threshold (tons/year) | 10 | 10 | 15 | 10 | 1,100 MT |
| Average Daily Emissions (lbs/day) | $\begin{aligned} & 0.9 \\ & 1.2 \\ & \hline \end{aligned}$ | $\begin{aligned} & 22.4 \\ & 27.9 \\ & \hline \end{aligned}$ | $\begin{aligned} & 12.4 \\ & 13.6 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.2 \\ & \underline{2.5} \\ & \hline \end{aligned}$ | -- |
| Significance Threshold | 54 | 54 | 54 | 54 | -- |
| Significant? | No | No | No | No | No |

Air Quality Standards for Local Air Pollutants (Carbon Monoxide from Project Traffic)
Increased intersection congestion can lead to increased localized carbon monoxide concentrations (hot spots) in the vicinity of the intersection. Typically there needs to be a substantial increase in the number of vehicles accessing an intersection and a decrease in the intersection level of service (LOS), and a very high volume of traffic in order for there to be elevated carbon monoxide concentrations of concern. The BAAQMD CEQA Air Quality Guidelines state that a proposed project would result in less than significant impacts to localized carbon monoxide concentrations if the following screening criteria are met:

1. Project is consistent with an applicable congestion management program established by the county congestion management agency for designated roads or highways, regional transportation plan, and local congestion management agency plans.
2. The project traffic would not increase traffic volumes at affected intersections to more than 44,000 vehicles per hour.
3. The project traffic would not increase traffic volumes at affected intersections to more than 24,000 vehicles per hour where vertical and/or horizontal mixing is substantially limited (e.g. tunnel, parking garage, bridge underpass, natural or urban street canyon, below grade roadway).

The project would not generate more than 50 trips in one hour during the peak hours. The project would, therefore, meet the carbon monoxide screening criteria, and less-than-significant impacts would result.

Impact 3: Result in a cumulatively considerable net increase of any criteria pollutant for which the project region is non-attainment under an applicable national or State ambient air quality standard (including releasing emissions which exceed quantitative thresholds for ozone precursors)? Less than Significant

The Bay Area is considered a non-attainment area for ground-level ozone and $\mathrm{PM}_{2.5}$ under both the Federal Clean Air Act and the California Clean Air Act. The area is also considered nonattainment for $\mathrm{PM}_{10}$ under the California Clean Air Act, but not the Federal Act. The area has attained both State and Federal ambient air quality standards for carbon monoxide. As part of an effort to attain and maintain ambient air quality standards for ozone, $\mathrm{PM}_{2.5}$ and $\mathrm{PM}_{10}$, BAAQMD has established thresholds of significance for air pollutants. These thresholds are for ozone precursor pollutants (reactive organic gases and nitrogen oxides), $\mathrm{PM}_{2.5}$ and $\mathrm{PM}_{10}$. Emissions from projects that are below these thresholds would not be cumulatively considerable. Since project emissions of ozone precursor pollutants and particulate matter (i.e., $\mathrm{PM}_{10}$ and $\mathrm{PM}_{2.5}$ ) were found to be less than BAAQMD significance thresholds, they would be considered less than significant.

## Impact 4: Expose sensitive receptors to substantial pollutant concentrations? Less than

 significantAs described above, the plant is a source of fugitive particulate matter emissions, on-site diesel exhaust emissions and off-site diesel exhaust emissions from truck traffic. The BAAQMD CEQA Air Quality Guidelines consider exposure of sensitive receptors to air pollutant levels that result in an unacceptable cancer risk or hazard to be significant. For cancer risk, BAAQMD considers an increased risk of contracting cancer that is 10 in one million chances or greater to be significant for a single source. For cumulative exposure to TACs from existing sources affecting a sensitive receptor, in addition to a proposed new source, the BAAQMD considers an increased risk of contracting cancer that is 100 in one million chances or greater to be significant. The BAAQMD CEQA Guidelines also consider exposure to annual $\mathrm{PM}_{2.5}$ concentrations that exceed 0.3 micrograms per cubic meter $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ from a single source to be significant and an annual $\mathrm{PM}_{2.5}$ concentration that exceeds $0.8 \mu \mathrm{~g} / \mathrm{m}^{3}$ from cumulative sources to be significant. The BAAQMD CEQA Guidelines recommend analyzing sources that are within 1,000 feet of sensitive receptors. The project site and nearby sensitive receptors are shown in Figure 1. The shaded red area
indicates the approximate 1,000-foot influence area and the small blue outlined areas are sensitive receptors.

Figure 1 Project Site, Sensitive Receptors and 1,000-ft Influence Area


This assessment predicts concentrations of TACs and PM2.5 at sensitive receptors within 1,000 feet of the project site and computed the excess cancer risk, annual PM2.5 concentrations and noncancer health hazard, expressed as a Hazard Index. The modeling included emissions modeling (conducted under Impact 2) that was input to a dispersion model that, using historical meteorological data, predicted annual concentrations of TACs and PM2.5. The methodology for computing these community risk impacts from modeled concentrations is described in Attachment 2.

## Project Community Risk Impacts

On-site annual emissions from diesel equipment and truck operation on or near the site were computed using CalEEMod as described above under Impact 2. Since the community risk assessment that addresses cancer risk, annual $\mathrm{PM}_{2.5}$ concentrations and non-cancer health hazards is localized, only the portion of truck travel on or near the site was included in the emissions modeling for this assessment. All equipment activity was assumed to occur on site.

TAC emissions are those from diesel exhaust, modeled as exhaust PM10. TAC and exhaust $\mathrm{PM}_{2.5}$ emissions were modeled for three portions of the site that are shown in Figure 2: 1) truck and worker parking area (indicated in green), 2) equipment yard area (indicated in yellow), and 3) crushing area (indicated in red). Fugitive dust emissions that are $\mathrm{PM}_{2.5}$, modeled under Impact 2, were included in the dispersion modeling. These areas are depicted in Figure 2 as outlined in pink for storage piles and crushing activities and in yellow and green for daily ground disturbances.

The U.S. EPA AERMOD dispersion model was used to predict concentrations of diesel particulate matter (or DPM) and $\mathrm{PM}_{2.5}$ concentrations at existing sensitive receptors in the vicinity of the project. The AERMOD dispersion model is a BAAQMD-recommended model for use in modeling analysis of these types of emission activities for CEQA projects. ${ }^{3}$ The dispersion modeling utilized four area sources to represent the on-site emissions of DPM exhaust and fugitive $\mathrm{PM}_{2.5}$ dust. For the exhaust emissions from construction equipment, an emission release height of six meters ( 19.7 feet) was used for those area sources. The elevated source height reflects the height of the equipment exhaust pipes plus an additional distance for the height of the exhaust plume above the exhaust pipes to account for plume rise of the exhaust gases. For modeling fugitive $\mathrm{PM}_{2.5}$ emissions, a near-ground level release height of two meters ( 6.6 feet) was used for the area sources. Emissions from project activities were modeled as occurring daily between 6 a.m. and 5 p.m.

The modeling used a five-year data set (2009-2013) of hourly meteorological data from the Sonoma County Airport in Santa Rosa prepared by the California Air Resources Board (CARB) for use with the AERMOD model. DPM and $\mathrm{PM}_{2.5}$ concentrations were modeled at nearby residential locations at a receptor height of 1.5 meters ( 4.9 feet) to represent the first floor building level. The maximum-modeled $\mathrm{PM}_{2.5}$ and DPM concentration occurred at a residence immediately west of the northern portion of the project site, as shown in Figure 2.

Using the risk impact assessment methodology contained in Attachment 2, cancer risk, annual $\mathrm{PM}_{2.5}$, and HI were computed at the receptor that had the maximum impact. This assessment is conservative in that it assumes nearly continuous exposure and that an infant occupies the residence where the maximum impact occurs. These results are reported in Table 4 below.

[^2]Table 4. Maximum Community Risk Impacts from Facility Operation

| Source | Cancer Risk <br> (per million) | Annual PM <br> $\mathbf{2 . 5}$ <br> $\left(\boldsymbol{\mu g} / \mathbf{m}^{\mathbf{3}}\right)$ | HI |
| :--- | :---: | :---: | :---: |
| Facility DPM and PM ${ }_{2.5}$ Sources | $7.2 \underline{9.1}$ | $0.23 \underline{0.24}$ | $<0.01$ |
| BAAQMD Single Source Threshold | 10.0 | 0.3 | 1.0 |
| Significant? | No | No | No |

## Cumulative Community Risk Impacts

The cumulative risk assessment includes the prediction of impacts from other substantial sources near the project site upon the receptor most affected by the proposed project. Cumulative sources near the project site were identified as 1) Syar Industries that operates an asphalt plant that receives used concrete and asphalt materials from contractors, which it reprocesses and sells as recycled aggregate base and other construction materials, 2) the Ghilotti construction yard that is across Ghilotti Avenue from the project site. This site is used mainly for parking or maintenance of construction vehicles, and 3) Todd Road traffic. There are two minor gas dispensing facilities but they have negligible emissions. Table 5 shows the community risks from the project and the combined risks from sources within 1,000 feet of the project site. The assessment of these cumulative sources is described below.

Table 5. Cumulative Community Risk from Combined Sources at Location of Maximum Project Impact

| Source | Maximum Cancer <br> Risk (per million) | $\mathrm{PM}_{2.5}$ concentration $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ | Hazard Index |
| :---: | :---: | :---: | :---: |
| Project TAC and fugitive sources combined | 7.29 .1 | $0.23 \underline{0.24}$ | $<0.01$ |
| Single-Source Threshold | 10.0 | 0.3 | 1.0 |
|  |  |  |  |
| Ghilotti Yard - TAC sources | 0.5 | 0.0 | 0.0 |
| Syar Industries - TAC and fugitive sources combined | 32.8 | 0.54 | 0.01 |
| Todd Road traffic - TAC and PM2.5 | 1.1 | 0.02 | $<0.01$ |
| Combined Sources | 41.643 .5 | $0.79 \underline{0.80}$ | 0.03 |
| Combined Sources | 100 | 0.8 | 10.0 |

Figure 2 Modeled Project Sources, Sensitive Receptors and Maximum Affected Receptor


## Syar Industries

A stationary Source Information Form was submitted to BAAQMD to obtain information for nearby stationary sources. BAAQMD provided the emissions information for the Syar Industries Plant. This information indicated low emissions of TACs, but high emissions of particulate matter, which are assumed to be associated with fugitive dust emissions. The $\mathrm{PM}_{2.5}$ fraction of fugitive dust is quite small. These emissions were used in dispersion modeling of this facility to predict cumulative impacts.

Not included in the BAAQMD-provided data are emissions from diesel equipment operating at that site. A review of an aerial of the site indicates there are about 6 pieces of construction equipment on site. This includes four loaders, a tractor crawler or tracked bulldozer and an excavator. This equipment was conservatively assumed to operate 8 hours per day for 260 days per year. A rough estimate of truck traffic was made that assumes 100 trucks use the site on average each day during the year. This equates to 200 trips per day. The trip length within the site and roadways within 1,000 feet of the project site were measured at 0.5 miles. The emissions from equipment usage and truck travel were modeled using CalEEMod.

Dispersion modeling of this source was conducted using the AERMOD model in a similar manner as for the proposed project. One area source was used for diesel sources operating in the general facility area. For fugitive $\mathrm{PM}_{2.5}$ emissions one area source was used to model emissions from the general facility area and three volume sources were used to model the asphalt plant equipment and material storage and handling emissions.

## Ghilotti Construction Yard

Ghilotti has a construction yard near Todd Road opposite Ghilotti Avenue from the project site. It appears that this site is used mainly for parking or maintenance of construction vehicles. This source was included in the cumulative modeling. Emissions were modeled using CalEEMod assuming 100 truck trips per average workday and use of a diesel powered forklift for 8 hours each workday. Dispersion modeling of the diesel sources was conducted in the same manner as for the project.

## Todd Road

Traffic counts for Todd Road indicate that there are less than 10,000 average daily trips per day, as the peak-hour traffic counts indicate about 600 vehicles per hour. The BAAQMD Roadway Screening Analysis Calculator was used to predict cancer risk and annual $\mathrm{PM}_{2.5}$ concentrations. This calculator requires the following inputs:
$>$ County $=$ Sonoma
$>$ Roadway orientation = East-West
$>$ Side of the roadway $=$ South
> Distance to receptor $=390$ feet
$>$ Average daily traffic volume $=10,000$ vehicles.

The computed cancer risk obtained from the calculator was adjusted upwards to account for the new BAAQMD/OEHHA guidance using a factor of 1.37.

## Supporting Documentation

The calculations and modeling assumptions used to compute cancer risks, annual $\mathrm{PM}_{2.5}$ concentrations and Hazard Index for the projected project are contained in Attachment 3. The information for cumulative sources is included in Attachment 4.

Impact 5: Create objectionable odors affecting a substantial number of people? Less-than-significant
The project generates localized emissions of diesel exhaust during equipment operation and truck activity. These emissions may be noticeable from time to time at the site boundary. The BAAQMD CEQA Air Quality Guidelines threshold is based on the number of confirmed complaints per year averaged over a three year period for land uses that are considered to be sources of odors. Construction yard facilities are not listed among the considered as sources of odors. There is no evidence of any sources of odors that would result in frequent odor complaints.

Impact 6: Generate greenhouse gas emissions, either directly or indirectly, that may have a significant impact on the environment? Less than Significant

The BAAQMD CEQA Air Quality Guidelines contain methodology and thresholds of significance for evaluating greenhouse gas (GHG) emissions from land use type projects. The BAAQMD thresholds were developed specifically for the Bay Area after considering the latest Bay Area GHG inventory and the effects of AB 32 scoping plan measures that would reduce regional emissions. BAAQMD intends to achieve GHG reductions from new land use developments to close the gap between projected regional emissions with AB 32 scoping plan measures and the AB 32 targets. The BAAQMD applies GHG efficiency thresholds to projects with emissions of 1,100 metric tons (MT) of CO2e (carbon dioxide equivalency) or greater. Projects that have emissions below 1,100 MT of CO2e per year are considered to have less than significant GHG emissions.

The potential sources of greenhouse gas emissions from the project would be from 1) use of onsite off-road diesel powered equipment to process material and 2) truck traffic associated with the facility. The GHG emissions from these sources were modeled using CalEEMod and reported in Table 3. Annual emissions from the project would be 629 metric tons (MT) per year.

The BAAQMD CEQA Air Quality Guidelines recommend a threshold of 1,100 metric tons per year that is used by the City to judge the significance of greenhouse gas emissions from projects. The project would, therefore, not generate greenhouse gas emissions that would have a significant impact on the environment, nor conflict with an applicable plan, policy or regulation adopted for the purpose of reducing the emissions of greenhouse gases.

Attachment 1: Fugitive $\mathbf{P M 1 0}$ and $\mathbf{P M}_{2.5}$ Emission Calculations and Project CalEEMod Modeling and Equipment Usage Assumptions

Table F1
Ghilotti - 304 Todd Road, Santa Ros
PM10 and PM2.5 Emissions From Material Processing Equipment
Recycle Materail Processing and Facility Operation Information

| Annual Raw Materail Process Rate (ton/yr) $=$ | 50,400 |
| :--- | :--- |
| Hourly Process rate (ton/hr) | 100 |
| Average Daily Process Rate (ton/day) | 800 |
| Days to Process Annual Amount $=$ | 63 |
| Average Hours per day Processing $($ hrs $)=$ | 8 |
| Annual Facility Operation (days) $)$ | 266 |


| Equipment Type | Percent of Input | $\begin{gathered} \text { Process } \\ \text { Rate } \\ \text { (ton/hr) } \end{gathered}$ | Number of Transfers | Daily Operation (hours) | Emission <br> $\begin{array}{c}\text { Factor } \\ \text { (lb/ton) }\end{array}$ | PM10 Emissions |  |  | Emission <br> $\begin{array}{c}\text { Factor } \\ \text { (lb/ton) }\end{array}$ | PM2.5 Emissions |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Hourly <br> (lb/hr) | $\begin{gathered} \hline \text { Average } \\ \text { Daily } \\ \text { (lb/day) } \\ \hline \end{gathered}$ | $\begin{aligned} & \text { Anual } \\ & (\operatorname{ton} / \mathrm{y}) \end{aligned}$ |  | $\begin{aligned} & \text { Hourly } \\ & \text { (lb/hr) } \end{aligned}$ | $\begin{gathered} \hline \text { Average } \\ \text { Daily } \\ \text { (Ib/day) } \end{gathered}$ | $\begin{aligned} & \text { Annual } \\ & (\text { ton } 1 \text { ) } \end{aligned}$ |
| Crushing Equipment |  |  |  |  |  |  |  |  |  |  |  |  |
| Feed Hopper | 100\% | 100 | 1 | 8.0 | 0.000016 | 0.002 | 0.003 | 0.0004 | 0.000003 | 0.0003 | 0.0006 | 0.0001 |
| Conveyor to Crusher | 100\% | 100 | 1 | 8.0 | 0.00058 | 0.0582 | 0.110 | 0.0147 | 0.000240 | 0.024 | 0.045 | 0.0060 |
| Crusher | 100\% | 100 | 1 | 8.0 | 0.00054 | 0.054 | 0.102 | 0.0136 | 0.00010 | 0.010 | 0.019 | 0.0025 |
| Crusher Conveyor to Loadout Pile | 100\% | 100 | 2 | 8.0 | 0.00058 | 0.1163 | 0.220 | 0.0293 | 0.000240 | 0.048 | 0.091 | 0.0121 |
| Total |  |  |  |  |  | 0.2 | 0.44 | 0.06 |  | 0.08 | 0.16 | 0.02 |

Table F2
Ghilotti - 304 Todd Road, Santa Rosa
PM10 and PM2.5 From Facility Fugitive Emission Sources

|  | Operation |  |  |  |  |  | Emission Factors |  |  | PM10 Emissions |  |  | PM2.5 Emissions |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \text { Process } \\ \text { Rate } \\ \hline \end{gathered}$ | $\begin{array}{\|c} \text { Process } \\ \text { Rate Units } \\ \hline \end{array}$ | No. of Equip. | Daily Hours (hours/day) | $\begin{gathered} \text { Days } \\ \text { per } \\ \text { Year } \end{gathered}$ | Total <br> Annual <br> Hours <br> (hours/yr) | PM10 <br> Emission Factor | PM2.5 <br> Emission Factor | Emission Factor Units | Ave <br> Hourly <br> (lb/hr) | $\begin{array}{\|c\|} \hline \text { Ave Daily } \\ \text { (lb/day) } \end{array}$ | Annual <br> Average (ton/yr) | Ave <br> Hourly <br> (lb/hr) | Ave Daily (lb/day) | Annual <br> Average (ton/yr) |
| Loaders - Loader Travel <br> Processing - Crush \& Screening Feed | 4.7 | mile/day | 1 | 8 | 63 | 504 | 0.81 | 0.08 | lb/VMT | 0.48 | 0.90 | 0.12 | 0.05 | 0.09 | 0.01 |
| Processing - Truck Loading Areas/Pile Maintenance | 4.7 | mile/day | 1 | 8 | 63 | 504 | 0.81 | 0.08 | lb/vMT | 0.48 | 0.90 | 0.12 | 0.05 | 0.09 | 0.01 |
| Subtotal - Loader Travel Emissions |  |  |  |  |  |  |  |  |  |  | 1.80 | 0.24 |  | 0.18 | 0.02 |
| Loaders - Truck Loading |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Processing Area - Haul Truck Loading (via loader) | 100 | ton/hr | 2 | 8 | 63 | 1008 | 0.0011 | 0.00017 | lb/ton | 0.22 | 0.42 | 0.06 | 0.03 | 0.06 | 0.009 |
| Other Off-Road Equipment |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Bulldozing | - | - | 1 | 8 | 63 | 504 | 0.38 | 0.21 | lb/hr | 0.38 | 0.71 | 0.09 | 0.21 | 0.39 | 0.05 |
| Grading | 12 | mile/day | 1 | 4 | 63 | 252 | 0.124 | 0.009 | lb/vMT | 0.37 | 0.35 | 0.05 | 0.03 | 0.02 | 0.003 |
| Excavator | 100 | ton/hr | 1 | 8 | 63 | 504 | 0.0011 | 0.00017 | lb/ton | 0.11 | 0.21 | 0.03 | 0.02 | 0.03 | 0.004 |
| Subtotal - Off-Road Equipment Emissions |  |  |  |  |  |  |  |  |  |  | 1.28 | 0.17 |  | 0.45 | 0.06 |
| On-Site Haul Trucks - Unpaved Road Travel |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Operational Haul Trucks | 756 | mile/yr | - | - | - | - | 0.226 | 0.023 | lb/vMT | - | 0.64 | 0.09 | - | 0.06 | 0.01 |
| Recycle Processing Haul Trucks | 1,090 | mile/yr | - | - | - | - | 0.284 | 0.028 | lb/VMT | - | 1.16 | 0.15 | - | 0.12 | 0.02 |
| Subtotal |  |  |  |  |  |  |  |  |  |  | 1.80 | 0.24 |  | 0.18 | 0.02 |
| Wind Erosion (annual) | 4.0 | acres | - | 24 | 365 | 8760 | 1.36 | 0.20 | lb/acre/day | - | 5.44 | 0.99 |  | 0.82 | 0.15 |
| Total Excavation/Processing Fugitives |  |  |  |  |  |  |  |  |  | - | 10.7 | 1.70 | - | 1.7 | 0.27 |
| Total Operation and Processing Fugitives and Crushing E | Equipment | Emissions |  |  |  |  |  |  |  | - | 13.2 | 1.7568 | - | 2.1 | 0.2859 |

Table F3
Ghilotti - 304 Todd Road, Santa Rosa
Emissions Factors Used For Facility Operation and Processing Fugitive PM10 \& PM2.5 Emissions

| Emission Source | PM10 Emission Factors |  |  | PM2.5 Emission Factors |  |  | Units | Reference |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Uncontrolled | $\begin{gathered} \% \\ \text { Control } \\ \hline \end{gathered}$ | Controlled | Uncontrolled | $\begin{gathered} \text { Fraction of } \\ \text { PM10 } \\ \hline \end{gathered}$ | Controlled |  |  |
| Feed Hopper | 0.000016 | 0\% | 0.000016 | 0.000003 | 0.20 | 0.000003 | 13/ton | 8/04AP-42 Section 11.19.2 (Crushed Stone Processing) - uncontrolled |
| Primary Crushing | - | - | 0.00054 | - | - | 0.00010 | 1b/ton | 8/04 AP-42 Section 11.19.2 (Crushed Stone Processing) - tertiary crushing (estimate for primary crusher) |
| Secondary Crushing | - | - | 0.00054 |  | - | 0.00010 | 1b/ton | 8/04 AP-42 Section 11.19.2 (Crushed Stone Processing) - tertiary crushing (estimate for secondary crusher) |
| Fines Crushing | 0.015 |  | 0.0012 |  | - | 0.00007 | 1b/ton | 8/04AP-42 Section 11.19.2 (Crushed Stone Processing) - Fines Crushing |
| Screening | 0.0087 | - | 0.00074 | - | - | 0.00005 | 1b/ton | 8/04AP-42 Section 11.19.2 (Crushed Stone Processing) - Screening |
| Fines Screening | 0.072 | - | 0.0022 | - | - | 0.00005 | 1b/ton | 8/04AP-42 Section 11.19.2 (Crushed Stone Processing) - Fines screening |
| Conveyor Transfer Points | 0.0011 | - | 0.000046 | 0.00031 | - | 0.000013 | 1b/ton | 8/04 AP-42 Section 11.19.2 (Crushed Stone Processing) - Conveyor transfer point |
| Loading/tockpiling | 0.0011 | 0\% | 0.0011 | 0.00017 | 0.15 | 0.00017 | 1b/ton | 11/06 AP-42 Section 13.2.4 (Aggregate handling and Storage Piles) - Material drop operations |
| Avg of Conveyor Transfer + Stockpiling | - |  | 0.00058 | - | - | 0.000240 | 1b/ton | uncontrolled drop to conveyor \& controlled loadout |
| Operation - Haul Truck Unpaved Travel (daily)* | 1.88 | 85\% | 0.282 | 0.188 | - | 0.028 | lb/VmT | AP-42 Unpaved Roads |
| Operation - Haul Truck Unpaved Travel (Annual)* | 1.50 | 85\% | 0.226 | 0.150 | - | 0.023 | lb/VmT | AP-42 Unpaved Roads |
| Processing - Haul Truck Unpaved Travel (daily)* | 2.37 | 85\% | 0.355 | 0.237 | - | 0.036 | lb/VmT | AP-42 Unpaved Roads |
| Processing - Haul Truck Unpaved Travel (Annual)* | 1.89 | 85\% | 0.284 | 0.189 | - | 0.028 | 1b/VMT | AP-42 Unpaved Roads |
| Bulldozing (lb/hr)** | 0.75 | 50\% | 0.38 | 0.41 | - | 0.21 | 1b/hr | AP-42 Western Surface Coal Mining (overburden dozing) |
| Wind Erosion for Storage Piles | 1.7 | 0\% | 1.7 | 0.26 | 0.15 | 0.26 | 1b/acre-day | BAAQMD Permit Handbook, Section 11.7 Crushing and Grinding |
| Wind Erosion for Storage Piles (annual) | 1.4 | 0\% | 1.4 | 0.20 | 0.15 | 0.20 | 1b/acre-day | BAAQMD Permit Handbook, Section 11.7 Crushing and Grinding |

Note: * Controlled emission factor assumes $85 \%$ control effectiveness for use of cheical du
$* *$ Controlled emission factor assumes $50 \%$ control effectivenes for use of watering
On-Site Equipment/Vehicles Unpaved Road Emission Factors

|  | Average <br> Weight <br> (tons) | Silt** <br> Cquipment Type <br> Cont <br> (\%) | PM10 <br> Uncontrolled <br> Factor <br> (lb/VMT) | PM10** <br> Controlled <br> Factor <br> (lb/VMT) | PM2.5 <br> Uncontrolled <br> Factor <br> (lb/VMT) | PM2.5** <br> Controlled <br> Factor <br> (b/VMT) |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Loaders (Cat 980) | 33.5 | 6.9 | 2.70 | 0.81 | 0.27 | 0.08 |
| Motor Grader*** | - | 3 mph | 0.28 | 0.12 | 0.02 | 0.01 |

** Controlled emission factor assumes $70 \%$ control effectiveness for watering and reduced speeds for equipment travel and $55 \%$ for grading for watering
*** AP-42 Western Surface Coal Mining (Table 11.9.1 - grading)

| $\|$Vehicle/Process/Emission Factor Information   <br> Loader Capacity $=$ 5 cubic yards <br> Loader Capacity $=$ 6.5 tons <br> Operation Truck Travel Distance $=$ 1,000 round-trip feet <br> Recycle Processing Truck Travel Distance $=$ 2,283 round-trip feet <br> Haul Truck Capacity (CY) $=$ 15 per truck <br> Haul Truck Capacity (tons) $=$ 20.0 per truck <br> Haul Truck Weight (unloaded $=$ 15.0 tons <br> Average Haul Truck Wt. (load \& no load) 25.0 tons <br> Operation - Annual No. Trucks $=$ 3,990 trucks/year <br> Recycle Processing - Annual No. Trucks $=$ 2,520 trucks/year <br> Average wind speed (mph) 5.26 Santa Rosa Airport (2001-2005 from BAAQMD) <br> No. days with precip. > 0.01 inch 73 NWS Station, Santa Rosa, Ca <br> Recycle Material Moisture content $(\%)=$ 2.1 AP-42 \& BAAQMD <br> Site Area Material Moisture content $(\%)=$ 7.9 CalEEMod <br> Site Area Silt Content $(\%)$ 6.9 CalEEMod |
| :--- |

# 304 Todd Road - Ghiolotti Yard (Yellow and Green Area) 

## Sonoma-San Francisco County, Annual

### 1.0 Project Characteristics

### 1.1 Land Usage

| Industrial Park | 1.00 | 1000sqft | 19.00 | 1,000.00 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: |

### 1.2 Other Project Characteristics

| Urbanization | Urban | Wind Speed (m/s) | 2.2 | Precipitation Freq (Days) <br> Operational Year | 2019 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Climate Zone | 4 |  |  |  |  |
| Utility Company | Pacific Gas \& Electric Company |  |  |  |  |
| CO2 Intensity <br> (Ib/MWhr) | 430 | CH4 Intensity <br> (Ib/MWhr) | 0.029 | N2O Intensity <br> (Ib/MWhr) | 0.006 |

### 1.3 User Entered Comments \& Non-Default Data

## Project Characteristics - PG\&E current rate

Land Use - No real structures on site
Construction Phase - Use construction to model annual operational emissions
Off-road Equipment - based on provided list
Off-road Equipment - Based on provided list
Trips and VMT - Assumes 15 roundtrips per day for 266 trips per year at 20 miles per trip. Assume 3 workers per average day (or 10 daily trips) Grading - Assumes each acre is disturbed daily
Vehicle Trips - Using construciton to model operational since construction yard
Construction Off-road Equipment Mitigation - Used project equipment list that includes Tier level

| Table Name | Column Name | Default Value | New Value |
| :---: | :---: | :---: | :---: |
| tblConstDustMitigation | WaterUnpavedRoadVehicleSpeed | 40 | 15 |
| tbiConstEquipMinitigation |  | 0.00 | 4.00 |
| tblConstEquipMitigation | NumberOfEquipmentMitigated | 0.00 | 2.00 |
| tblConstEquipMitigation | NumberOfEquipmentMitigated | 0.00 | 2.00 |
| tbiConstEquipMitigation | NumberOfEquipmentMitigated | 0.00 | 1.00 |
| tblConstEquipMitigation | Tier | No Change | Tier 4 Interim |
| tblConstEquipMitigation | Tier | No Change | Tier 3 |
| tbiConstEquipMitigation | Tier | No Change | Tier 3 |
| tbiConstEquipMitigation | Tier | No Change | Tier 2 |
| tblConstEquipMitigation | Tier | No Change | Tier 2 |
| tblConstEquipMitigation | Tier | No Change | Tier 2 |
| tblConstEquipMitigation | Tier | No Change | Tier 2 |
| tblConstructionPhase | NumDays | 10.00 | 260.00 |
| tblGrading | AcresOfGrading | 6.50 | 33.15 |
| tbiLandUse | LotAcreage | 0.02 | 19.00 |
| tblOffRoadEquipment | OffRoadEquipmentUnitAmount | 3.00 | 0.00 |
| tbiOffRoadEquipment | OffRoadEquipmentUnitAmount | 4.00 | 0.00 |
| tblProjectCharacteristics | CO2IntensityFactor | 641.35 | 430 |
| tbIProjectCharacteristics | OperationalYear | 2018 | 2019 |
| tbiTripsAndVMT | Hauling TripNumber | 0.00 | 7,980.00 |
| tbiTripsAndVMT | WorkerTripNumber | 25.00 | 10.00 |


| tbivehicleTrips | ST_TR | 2.49 | 0.01 |
| :---: | :---: | :---: | :---: |
| tbivehicleTrips | SU_TR | 0.73 | 0.01 |
| tbiVehicleTrips | WD_TR | 6.83 | 0.01 |

### 2.0 Emissions Summary

### 2.1 Overall Construction

Unmitigated Construction

|  | ROG | NOX | CO | SO2 | Fugitive PM10 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | PM10 Total | Fugitive PM2.5 | $\begin{gathered} \text { Exhaust } \\ \text { PM2.5 } \end{gathered}$ | PM2.5 Total | Bio- CO2 | NBioCO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Year | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| 2017 | 0.0761 | 1.6968 | 0.4932 | $3.5600 \mathrm{e}-$ 003 | 0.0940 | 0.0228 | 0.1169 | 0.0228 | 0.0216 | 0.0444 | 0.0000 | 344.0413 | 344.0413 | 0.0257 | 0.0000 | 344.6834 |
| Maximum | 0.0761 | 1.6968 | 0.4932 | $\begin{gathered} 3.5600 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0940 | 0.0228 | 0.1169 | 0.0228 | 0.0216 | 0.0444 | 0.0000 | 344.0413 | 344.0413 | 0.0257 | 0.0000 | 344.6834 |

## Mitigated Construction



| Quarter | Start Date | End Date | Maximum Unmitigated ROG + NOX (tons/quarter) | Maximum Mitigated ROG + NOX (tons/quarter) |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 1-1-2017 | 3-31-2017 | 0.4420 | 0.4228 |
| 2 | 4-1-2017 | 6-30-2017 | 0.4354 | 0.4160 |
| 3 | 7-1-2017 | 9-30-2017 | 0.4402 | 0.4206 |
|  |  | Highest | 0.4420 | 0.4228 |

### 3.0 Construction Detail

## Construction Phase

| Phase Number | Phase Name | Phase Type | Start Date | End Date | Num Days Week | Num Days | Phase Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Site Preparation | Site Preparation | 1/1/2017 | 12/29/2017 | 5 | 260 |  |

## Acres of Grading (Site Preparation Phase): 33.15

## Acres of Grading (Grading Phase): 0

Acres of Paving: 0
Residential Indoor: 0; Residential Outdoor: 0; Non-Residential Indoor: 0; Non-Residential Outdoor: 0; Striped Parking Area: 0

OffRoad Equipment

| Phase Name | Offroad Equipment Type | Amount | Usage Hours | Horse Power | Load Factor |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Site Preparation | Air Compressors | 4 | 0.10 | 78 | 0.48 |
| Site Preparation | Crawler Tractors | 2 | 0.20 | 212 | 0.43 |
| Site Preparation | Excavators | 2 | 0.20 | 158 | 0.38 |
| Site Preparation | Forklifts | 1 | 2.00 | 89 | 0.20 |
| Site Preparation | Other Construction Equipment | 0 | 0.50 | 172 | 0.42 |
| Site Preparation | Other General Industrial Equipment | 0 | 0.50 | 88 | 0.34 |
| Site Preparation | Other Material Handling Equipment | 1 | 0.20 | 168 | 0.40 |
| Site Preparation | Rubber Tired Dozers | 0 | 8.00 | 247 | 0.40 |
| Site Preparation | Tractors/Loaders/Backhoes | 0 | 8.00 | 97 | 0.37 |

## Trips and VMT

| Phase Name | Offroad Equipment Count | Worker Trip Number | Vendor Trip Number | Hauling Trip Number | Worker Trip Length | Vendor Trip Length | Hauling Trip Length | Worker Vehicle Class | Vendor Vehicle Class | Hauling Vehicle Class |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Site Preparation | 10 | 10.00 | 0.00 | 7,980.00 | 10.80 | 7.30 | 20.00 | LD_Mix | HDT_Mix | HHDT |

### 3.1 Mitigation Measures Construction

Use Cleaner Engines for Construction Equipment
Use Soil Stabilizer
Reduce Vehicle Speed on Unpaved Roads
Clean Paved Roads

### 3.2 Site Preparation-2017

## Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | $\begin{aligned} & \text { Fugitive } \\ & \text { PM10 } \end{aligned}$ | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | $\begin{gathered} \text { NBio- } \\ \text { CO2 } \end{gathered}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 0.0176 | 0.0000 | 0.0176 | $\begin{gathered} 1.9000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | $\begin{aligned} & 1.9000 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | 0.0182 | 0.1812 | 0.1096 | $\begin{gathered} 1.8000 \mathrm{e}- \\ 004 \end{gathered}$ |  | 0.0109 | 0.0109 |  | 0.0101 | 0.0101 | 0.0000 | 16.4131 | 16.4131 | $\begin{gathered} 4.5800 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 16.5278 |
| Total | 0.0182 | 0.1812 | 0.1096 | $\begin{gathered} 1.8000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0176 | 0.0109 | 0.0285 | $\begin{gathered} 1.9000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0101 | 0.0120 | 0.0000 | 16.4131 | 16.4131 | $\begin{gathered} 4.5800 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 16.5278 |

## Unmitigated Construction Off-Site

|  | ROG | NOX | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBioCO2 | Total CO2 | CH4 | N2O | co2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0496 | 1.5089 | 0.3187 | $\begin{gathered} 3.2700 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0662 | 0.0119 | 0.0781 | 0.0182 | 0.0114 | 0.0295 | 0.0000 | 317.3673 | 317.3673 | 0.0206 | 0.0000 | 317.8820 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | $\begin{gathered} 8.3300 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 6.6100 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0649 | $\begin{gathered} 1.1000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0102 | $9.0000 \mathrm{e}-$ $005$ | 0.0103 | $\begin{gathered} 2.7200 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{aligned} & 9.0000 \mathrm{e}- \\ & 005 \end{aligned}$ | $\begin{gathered} 2.8000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 10.2609 | 10.2609 | $\begin{gathered} 5.1000 \mathrm{e} \\ 004 \end{gathered}$ | 0.0000 | 10.2736 |
| Total | 0.0579 | 1.5155 | 0.3836 | $\begin{gathered} 3.3800 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0764 | 0.0120 | 0.0884 | 0.0209 | 0.0115 | 0.0323 | 0.0000 | 327.6282 | 327.6282 | 0.0211 | 0.0000 | 328.1556 |

## Mitigated Construction On-Site

|  | ROG | NOX | CO | SO2 | Fugitive PM10 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | $\begin{aligned} & \text { Fugitive } \\ & \text { PM2.5 } \end{aligned}$ | $\begin{gathered} \text { Exhaust } \\ \text { PM2.5 } \end{gathered}$ | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 0.0176 | 0.0000 | 0.0176 | $\begin{gathered} 1.9000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | $\begin{gathered} 1.9000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | en | 0.1152 | 0.1192 | $1.8000 \mathrm{e}-$ 004 |  | $4.6000 \mathrm{e}-$ 003 | $\begin{gathered} 4.6000 \mathrm{e}- \\ 003 \end{gathered}$ |  | $\begin{gathered} 4.5300 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 4.5300 \mathrm{e}-\mathrm{a} \\ 003 \end{gathered}$ | 0.0000 | 16.4131 | 16.4131 | $\begin{gathered} 4.5800 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 16.5277 |
| Total | $\begin{aligned} & 6.5400 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.1152 | 0.1192 | $\begin{gathered} 1.8000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0176 | $\begin{gathered} 4.6000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0222 | $\begin{gathered} 1.9000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 4.5300 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{array}{\|c\|} \hline 6.4300 \mathrm{e}- \\ 003 \end{array}$ | 0.0000 | 16.4131 | 16.4131 | $\begin{gathered} 4.5800 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 16.5277 |

## Mitigated Construction Off-Site

|  | ROG | NOX | CO | SO2 | $\begin{aligned} & \text { Fugitive } \\ & \text { PM10 } \end{aligned}$ | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | $\begin{aligned} & \text { Fugitive } \\ & \text { PM2.5 } \end{aligned}$ | $\begin{gathered} \text { Exhaust } \\ \text { PM2.5 } \end{gathered}$ | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | co2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0496 | 1.5089 | 0.3187 | $\begin{gathered} 3.2700 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0662 | 0.0119 | 0.0781 | 0.0182 | 0.0114 | 0.0295 | 0.0000 | 317.3673 | 317.3673 | 0.0206 | 0.0000 | 317.8820 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | $\begin{gathered} 8.3300 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{aligned} & 6.6100 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.0649 | $\begin{gathered} 1.1000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0102 | $9.0000 \mathrm{e}-$ 005 | 0.0103 | $\begin{gathered} 2.7200 \mathrm{e} \\ 003 \end{gathered}$ | 9.0000e005 | $\begin{gathered} 2.8000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 10.2609 | 10.2609 | $5.1000 \mathrm{e}-$ 004 | 0.0000 | 10.2736 |
| Total | 0.0579 | 1.5155 | 0.3836 | $3.3800 \mathrm{e}-$ 003 | 0.0764 | 0.0120 | 0.0884 | 0.0209 | 0.0115 | 0.0323 | 0.0000 | 327.6282 | 327.6282 | 0.0211 | 0.0000 | 328.1556 |

304 Todd Road - Ghiolotti Yard (Crushing - Red Area) - Sonoma-San Francisco County, Annual

## 304 Todd Road - Ghiolotti Yard (Crushing - Red Area)

## Sonoma-San Francisco County, Annua

Updated in Jan. 2018

### 1.0 Project Characteristics

### 1.1 Land Usage

| Land Uses | Size | Metric | Lot Acreage | Floor Surface Area | Population |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Industrial Park | 1.00 | 1000sqft | 19.00 | 1,000.00 | 0 |

### 1.2 Other Project Characteristics

| Urbanization | Urban | Wind Speed (m/s) | 2.2 | Precipitation Freq (Days) |
| :--- | :--- | :--- | :--- | :--- |
| Climate Zone | 4 |  | Operational Year |  |

### 1.3 User Entered Comments \& Non-Default Data

Project Characteristics - PG\&E current rate
Land Use - No real structures on site
Construction Phase - Use construction to model annual operational emissions - Crushing $=63$ days/year $=50,400$ tons
Off-road Equipment - based on provided list
Off-road Equipment - Based on provided list - but using 68 days/year (50,000tons)
Trips and VMT - Assumes 50,000 tons at 20 tons/roundtrip assume no new employees
Grading - fugitive calculations separate
Vehicle Trips - Using construciton to model operational since construction yard
Construction Off-road Equipment Mitigation - Used project equipment list that includes Tier level
Table Name

### 2.0 Emissions Summary

2.1 Overall Construction

Mitigated Construction

|  | ROG | NOx | CO | SO2 | $\begin{aligned} & \text { Fugitive } \\ & \text { PM10 } \end{aligned}$ | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | $\begin{aligned} & \hline \text { Fugitive } \\ & \text { PM2.5 } \end{aligned}$ | $\begin{gathered} \text { Exhaust } \\ \text { PM2.5 } \end{gathered}$ | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Year | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| 2017 | 0.0897 | 2.0010 | 1.4989 | $\begin{gathered} 4.3500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.4266 | 0.0505 | 0.4771 | 0.2214 | 0.0502 | 0.2716 | 0.0000 | 418.2887 | 418.2887 | 0.0590 | 0.0000 | 419.7644 |
| Maximum | 0.0897 | 2.0010 | 1.4989 | $\begin{gathered} 4.3500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.4266 | 0.0505 | 0.4771 | 0.2214 | 0.0502 | 0.2716 | 0.0000 | 418.2887 | 418.2887 | 0.0590 | 0.0000 | 419.7644 |



### 3.0 Construction Detail

## Construction Phase

| Phase Number | Phase Name | Phase Type | Start Date | End Date | Num Days Week | Num Days | Phase Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Site Preparation | Site Preparation | 1/1/2017 | 3/29/2017 | 5 | 63 |  |

## Acres of Grading (Site Preparation Phase): 0

Acres of Grading (Grading Phase): 0

## Acres of Paving: 0

Residential Indoor: 0; Residential Outdoor: 0; Non-Residential Indoor: 0; Non-Residential Outdoor: 0; Striped Parking Area: 0

## OffRoad Equipment

| Phase Name | Offroad Equipment Type | Amount | Usage Hours | Horse Power | Load Factor |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Site Preparation | Crawler Tractors | 2 | 8.00 | 212 | 0.43 |
| Site Preparation | Crushing/Proc. Equipment | 1 | 8.00 | 309 | 0.78 |
| Site Preparation | Excavators | 2 | 8.00 | 158 | 0.38 |
|  | Generator Sets | 1 | 4.00 | 84 | 0.74 |
| Site Preparation | Graders | 1 | 4.00 | 187 | 0.41 |
| Site Preparation | Rubber Tired Dozers | 2 | 8.00 | 247 | 0.40 |
| Site Preparation | Tractors/Loaders/Backhoes | 0 | 8.00 | 97 | 0.37 |

## Trips and VMT

| Phase Name | Offroad Equipment Count | Worker Trip Number | Vendor Trip Number | Hauling Trip Number | Worker Trip Length | Vendor Trip Length | Hauling Trip Length | Worker Vehicle Class | Vendor Vehicle Class |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Site Preparation | 9 | 23.00 | 0.00 | 5,000.00 | 10.80 | 7.30 | 20.00 | LD_Mix | [HDT_Mix | IHHDT |

### 3.1 Mitigation Measures Construction

Use Cleaner Engines for Construction Equipment
Use Soil Stabilizer
Reduce Vehicle Speed on Unpaved Roads

### 3.2 Site Preparation - 2017

## Unmitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | $\begin{gathered} \text { Exhaust } \\ \text { PM2.5 } \end{gathered}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 0.3794 | 0.0000 | 0.3794 | 0.2085 | 0.0000 | 0.2085 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Rowa | 0.2041 | 2.2087 | 0.9181 | $\begin{gathered} \text { 2".2400" } \\ 003 \end{gathered}$ |  | 0.09060 | 0.0660 |  | ${ }^{10.08060}$ | 0.00'0896 | 0.0000 | 213.7187 | 21317187 | 0.0459 | 0.0000 | 211.8640 |
| Total | 0.2041 | 2.2087 | 0.9181 | $\begin{gathered} 2.2400 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3794 | 0.0960 | 0.4754 | 0.2085 | 0.0896 | 0.2982 | 0.0000 | 213.7187 | 213.7187 | 0.0459 | 0.0000 | 214.8649 |


|  | ROG | NOx | CO | SO2 | $\begin{aligned} & \text { Fugitive } \\ & \text { PM10 } \end{aligned}$ | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0311 | 0.9454 | 0.1997 | $\begin{gathered} 2.0500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0415 | $\begin{gathered} 7.4500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0489 | 0.0114 | $\begin{gathered} 7.1200 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0185 | 0.0000 | 198.8517 | 198.8517 | 0.0129 | 0.0000 | 199.1742 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | $\begin{gathered} 4.6400 \mathrm{e}-\mathrm{c} \\ 003 \end{gathered}$ | $\begin{gathered} 3.6800 \mathrm{e}-\mathrm{c} \\ 003 \end{gathered}$ | 0.0362 | $\begin{gathered} 6.0000 e-1 " ~ \\ 005 \end{gathered}$ | $\begin{gathered} 5.6900 \mathrm{e} \\ 003 \end{gathered}$ | $\begin{gathered} 5.0000 \mathrm{e}-\mathrm{i} \\ 005 \end{gathered}$ | $\begin{gathered} 5.7400 \mathrm{e}-\mathrm{c} \\ 003 \end{gathered}$ | $\begin{gathered} 1.5100 e- \\ 003 \end{gathered}$ | $\begin{gathered} 5.0000 \mathrm{e} \\ 005 \end{gathered}$ | $\begin{gathered} 1.5600 \mathrm{e} \\ 003 \end{gathered}$ | 0.0000 | 5.7185 | 5.7185 | $\begin{gathered} 2.8000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 5.7255 |
| Total | 0.0357 | 0.9491 | 0.2359 | $\begin{gathered} 2.1100 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0472 | $\begin{gathered} 7.5000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0547 | 0.0129 | $\begin{gathered} 7.1700 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0201 | 0.0000 | 204.5702 | 204.5702 | 0.0132 | 0.0000 | 204.8998 |

## Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | $\begin{aligned} & \text { Fugitive } \\ & \text { PM10 } \end{aligned}$ | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | PM10 <br> Total | $\begin{aligned} & \text { Fugitive } \\ & \text { PM2.5 } \end{aligned}$ | $\begin{gathered} \text { Exhaust } \\ \text { PM2.5 } \end{gathered}$ | PM2.5 <br> Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 0.3794 | 0.0000 | 0.3794 | 0.2085 | 0.0000 | 0.2085 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | 0.0540 | 1.0518 | 1.2630 | $\begin{gathered} 2.2400 \mathrm{e}-\mathrm{m} \\ 003 \end{gathered}$ |  | 0.0430 | 0.0430 |  | 0.0430 | 0.0430 | 0.0000 | 213.7185 | 213.7185 | 0.0459 | 0.0000 | 214.8647 |
| Total | 0.0540 | 1.0518 | 1.2630 | $\begin{gathered} 2.2400 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3794 | 0.0430 | 0.4224 | 0.2085 | 0.0430 | 0.2516 | 0.0000 | 213.7185 | 213.7185 | 0.0459 | 0.0000 | 214.8647 |

[^3]|  | ROG | NOx | CO | SO2 | $\begin{aligned} & \text { Fugitive } \\ & \text { PM10 } \end{aligned}$ | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | $\begin{aligned} & \text { Fugitive } \\ & \text { PM2.5 } \end{aligned}$ | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0311 | 0.9454 | 0.1997 | $\begin{gathered} 2.0500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0415 | $\begin{gathered} 7.4500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0489 | 0.0114 | $\begin{gathered} 7.1200 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0185 | 0.0000 | 198.8517 ] | 198.8517 | 0.0129 | 0.0000 | 199.1742 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | 4.64400e- 003 | $\begin{gathered} 3.6800- \\ 003 \end{gathered}$ | 0.0362 | $\begin{gathered} 6.0000-1 \\ 005 \end{gathered}$ | $\begin{gathered} 5.6900-1 \\ 003 \end{gathered}$ | $\begin{gathered} 5.00000-1 \\ 005 \end{gathered}$ | $\begin{gathered} 5.7400=- \\ 003 \end{gathered}$ | $\begin{gathered} 1.5100-1 \\ 003 \end{gathered}$ | $\begin{gathered} 5.0000-1 \\ 005 \end{gathered}$ | $\begin{gathered} 1.5600 \mathrm{e} \\ 003 \end{gathered}$ | 0.00000 | 5.7185 | 5.7185 | $\begin{gathered} 2.8000=- \\ 004 \end{gathered}$ | 0.00000 | 5.7255 |
| Total | 0.0357 | 0.9491 | 0.2359 | $\begin{gathered} 2.1100 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0472 | $\begin{gathered} 7.5000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0547 | 0.0129 | $\begin{gathered} 7.1700 \mathrm{e} \\ 003 \end{gathered}$ | 0.0201 | 0.0000 | 204.5702 | 204.5702 | 0.0132 | 0.0000 | 204.8998 |


|  |  | Data Request for Onsite Equipment Use |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ject Name: |  | Ghilotti | Construction |  |  |  |  |  |  |  | Complete ALL Portions in Yellow |
|  | Project Size | 19 | total acres |  | 19 | acres disturb |  |  |  |  |  |
|  |  | 0 | s.f. buildings |  |  |  |  |  |  |  |  |
|  | Typical operation Hours | 7 | am to |  | 6 | pm |  |  |  |  |  |
| Qty | Description | HP | Load Factor | $\begin{array}{\|c} \text { Tier Level } \\ 0,2,3,4) \\ \hline \end{array}$ | Average <br> Hours/day | Total Work Days/year | Avg. Hours per day based on 260 days of | horsepower hours | Annual Hours | Work Area (see attached) | Comments |
|  | Aerial Lifts | 62 | 0.31 | 4 |  |  |  |  | 0 |  |  |
| 4 | Air Compressors | 78 | 0.48 | 3 | 1 | 12 | 0.05 |  | 12 | ov |  |
|  | Bore/Drill Rigs | 205 | 0.5 | N/A |  |  |  |  | 0 |  |  |
|  | Cement and Mortar Mixers | 9 | 0.56 | N/A |  |  |  |  | 0 |  |  |
|  | Concrete/Industrial Saws | 81 | 0.73 | N/A |  |  |  |  | 0 |  |  |
|  | Cranes | 226 | 0.29 | N/A |  |  |  |  | , |  |  |
| 2 | Crawler Tractors | 208 | 0.43 | 3 | 1 | 266 | 1.02 | 23,791 | 266 | Yellow | In addition, there are 44 days @ 8 hours per day = 352 hrs. |
| 2 | Crawler Tractors | 208 | 0.43 | 3 | 8 | 44 | 1.35 | 31,483 | 352 | Red |  |
| 1 | Crushing/Proc. Equipment | 309 | 0.78 | 3 | 8 | 44 | 1.35 | 84,839 | 352 | Red |  |
| 15 | Dump Trucks | 16 | 0.38 | 3 | 1 | 266 | 1.02 |  | 266 | Green | Trucks modeled as on-road vehicles |
| 2 | Excavators | 162 | 0.38 | 3 | 1 | 266 | 1.02 | 16,375 | 266 | Yellow | In addition, there are 44 days @ 8 hours per day $=352$ hrs. |
| 2 | Excavators | 162 | 0.38 | 3 | 8 | 44 | 1.35 | 21,669 | 352 | Red |  |
| 1 | Forklifts | 89 | 0.2 | 2 | 2 | 266 | 2.05 | 9,470 | 532 | Yellow |  |
| 1 | Generator Sets | 84 | 0.74 | 3 | 4 | 22 | 0.34 | 5,470 | 88 | Red |  |
| 1 | Graders | 174 | 0.41 | 3 | 4 | 44 | 0.68 | 12,556 | 176 | Red |  |
|  | Off-Highway Tractors | 122 | 0.44 | N/A |  |  |  |  | 0 |  | 44 days crushing |
|  | Off-Highway Trucks | 400 | 0.38 | N/A |  |  |  |  | 0 |  | day |
| 1 | Other Construction Equipment | 171 | 0.42 | N/A | 1 | 266 | 1.02 | 19,104 | 266 | Yellow | changed to-63-day |
| 1 | Other General Industrial Equipment | 150 | 0.34 | N/A | 1 | 266 | 1.02 | 13,566 | 266 | Yellow | angeatersays |
| 1 | Other Material Handling Equipment | 167 | 0.40 | N/A | 1 | 266 | 1.02 | 17,769 | 266 | Yellow |  |
|  | Pavers | 125 | 0.42 | 4 |  |  |  |  | 0 |  |  |
|  | Paving Equipment | 130 | 0.36 | 3 |  |  |  |  | 0 |  |  |
|  | Plate Compactors | 8 | 0.43 | N/A |  |  |  |  | 0 |  |  |
|  | Pressure Washers | 13 | 0.2 | N/A |  |  |  |  | 0 |  |  |
|  | Pumps | 84 | 0.74 | N/A |  |  |  |  | , |  |  |
|  | Rollers | 80 | 0.38 | 3 |  |  |  |  | 0 |  |  |
|  | Rough Terrain Forklifts | 100 | 0.4 | 2 |  |  |  |  | 0 |  |  |
| 2 | Rubber Tired Dozers | 255 | 0.4 | N/A |  |  |  |  | 0 |  |  |
|  | Rubber Tired Loaders | 199 | 0.36 | 3 | 8 | 44 | 1.35 | 25,217 | 352 | Red |  |
|  | Scrapers | 361 | 0.48 | 3 |  |  |  |  | 0 |  |  |
|  | Signal Boards | 6 | 0.82 | N/A |  |  |  |  | 0 |  |  |
|  | Skid Steer Loaders | 64 | 0.37 | 3 |  |  |  |  | 0 |  |  |
|  | Surfacing Equipment | 253 | 0.3 | N/A |  |  |  |  | , |  |  |
|  | Sweepers/Scrubbers | 64 | 0.46 | 3 |  |  |  |  | 0 |  |  |
|  | Tractors/Loaders/Backhoes | 97 | 0.37 | 3 |  |  |  |  | 0 |  |  |
|  | Trenchers | 80 | 0.5 | N/A |  |  |  |  | 0 |  |  |
|  | Welders | 46 | 0.45 | N/A |  |  |  |  | 0 |  |  |
|  |  |  |  |  |  |  |  | 281309 |  |  |  |
|  |  |  |  |  |  |  |  | 122612 |  |  |  |

## Attachment 2: Health Risk Calculation Methodology

A health risk assessment (HRA) for exposure to Toxic Air Contaminates (TACs) requires the application of a risk characterization model to the results from the air dispersion model to estimate potential health risk at each sensitive receptor location. The State of California Office of Environmental Health Hazard Assessment (OEHHA) and California Air Resources Board (CARB) develop recommended methods for conducting health risk assessments. The most recent OEHHA risk assessment guidelines were published in February of 2015. ${ }^{4}$ These guidelines incorporate substantial changes designed to provide for enhanced protection of children, as required by State law, compared to previous published risk assessment guidelines. CARB has provided additional guidance on implementing OEHHA's recommended methods. ${ }^{5}$ This HRA used the recent 2015 OEHHA risk assessment guidelines and CARB guidance. The BAAQMD has adopted recommended procedures for applying the newest OEHHA guidelines as part of Regulation 2, Rule 5: New Source Review of Toxic Air Contaminants. ${ }^{6}$ Exposure parameters from the OEHHA guidelines and the recent BAAQMD HRA Guidelines were used in this evaluation.

## Cancer Risk

Potential increased cancer risk from inhalation of TACs are calculated based on the TAC concentration over the period of exposure, inhalation dose, the TAC cancer potency factor, and an age sensitivity factor to reflect the greater sensitivity of infants and children to cancer causing TACs. The inhalation dose depends on a person's breathing rate, exposure time and frequency of exposure, and the exposure duration. These parameters vary depending on the age, or age range, of the persons being exposed and whether the exposure is considered to occur at a residential location or other sensitive receptor location.

The current OEHHA guidance recommends that cancer risk be calculated by age groups to account for different breathing rates and sensitivity to TACs. Specifically, they recommend evaluating risks for the third trimester of pregnancy to age zero, ages zero to less than two (infant exposure), ages two to less than 16 (child exposure), and ages 16 to 70 (adult exposure). Age sensitivity factors (ASFs) associated with the different types of exposure are an ASF of 10 for the third trimester and infant exposures, an ASF of 3 for a child exposure, and an ASF of 1 for an adult exposure. Also associated with each exposure type are different breathing rates, expressed as liters per kilogram of body weight per day (L/kg-day). As recommended by the BAAQMD, $95^{\text {th }}$ percentile breathing rates are used for the third trimester and infant exposures, and $80^{\text {th }}$ percentile breathing rates for child and adult exposures. Additionally, CARB and the BAAQMD recommend the use of a residential exposure duration of 30 years for sources with longterm emissions (e.g., roadways).

Under previous OEHHA and BAAQMD HRA guidance, residential receptors are assumed to be at their home 24 hours a day, or 100 percent of the time. In the 2015 Risk Assessment Guidance, OEHHA includes adjustments to exposure duration to account for the fraction of time at home (FAH), which can be less than 100 percent of the time, based on updated population and activity statistics. The FAH factors are age-specific and are: 0.85 for third trimester of pregnancy to less than 2 years old, 0.72 for ages 2 to less than 16 years, and 0.73 for ages 16 to 70 years. Use of the FAH factors is allowed by the BAAQMD if there are no schools in the project vicinity that would have a cancer risk of one in a million or greater assuming 100 percent exposure ( $\mathrm{FAH}=1.0$ ).

Functionally, cancer risk is calculated using the following parameters and formulas:
Cancer Risk (per million) $=$ CPF x Inhalation Dose x ASF x ED/AT x FAH x $10^{6}$
Where:

```
CPF = Cancer potency factor (mg/kg-day)}\mp@subsup{}{}{-1
ASF = Age sensitivity factor for specified age group
ED = Exposure duration (years)
```

[^4]AT = Averaging time for lifetime cancer risk (years) FAH $=$ Fraction of time spent at home (unitless)

```
Inhalation Dose = Cair }\times\mathrm{ DBR }\timesA\times(EF/365) \times 10-6
    Where:
    Cair = concentration in air ( }\mu\textrm{g}/\mp@subsup{\textrm{m}}{}{3}
    DBR = daily breathing rate (L/kg body weight-day)
    A = Inhalation absorption factor
    EF = Exposure frequency (days/year)
    10-6}=\mathrm{ Conversion factor
```

The health risk parameters used in this evaluation are summarized as follows:

| Parameter | Exposure Type $\boldsymbol{\rightarrow}$ |  | Infant |  | Child |  |
| :--- | ---: | :---: | :---: | :---: | :---: | :---: |
|  | Age Range $\boldsymbol{\rightarrow}$ | $\mathbf{3}^{\text {rd }}$ Trimester | $\mathbf{0}<\mathbf{2}$ | $\mathbf{2}<\mathbf{9}$ | $\mathbf{2}<\mathbf{1 6}$ | $\mathbf{1 6}-\mathbf{3 0}$ |
| DPM Cancer Potency Factor (mg/kg-day) ${ }^{-1}$ | $1.10 \mathrm{E}+00$ | $1.10 \mathrm{E}+00$ | $1.10 \mathrm{E}+00$ | $1.10 \mathrm{E}+00$ | $1.10 \mathrm{E}+00$ |  |
| Daily Breathing Rate (L/kg-day)* | 361 | 1,090 | 631 | 572 | 261 |  |
| Inhalation Absorption Factor | 1 | 1 | 1 | 1 | 1 |  |
| Averaging Time (years) | 70 | 70 | 70 | 70 | 70 |  |
| Exposure Duration (years) | 0.25 | 2 | 14 | 14 | 14 |  |
| Exposure Frequency (days/year) | 350 | 350 | 350 | 350 | 350 |  |
| Age Sensitivity Factor | 10 | 10 | 3 | 3 | 1 |  |
| Fraction of Time at Home | $0.85-1.0$ | $0.85-1.0$ | $0.72-1.0$ | $0.72-1.0$ | 0.73 |  |

* $95^{\text {th }}$ percentile breathing rates for $3^{\text {rd }}$ trimester and infants and $80^{\text {th }}$ percentile for children and adults


## Non-Cancer Hazards

Potential non-cancer health hazards from TAC exposure are expressed in terms of a hazard index (HI), which is the ratio of the TAC concentration to a reference exposure level (REL). OEHHA has defined acceptable concentration levels for contaminants that pose non-cancer health hazards. TAC concentrations below the REL are not expected to cause adverse health impacts, even for sensitive individuals. The total HI is calculated as the sum of the HIs for each TAC evaluated and the total HI is compared to the BAAQMD significance thresholds to determine whether a significant non-cancer health impact from a project would occur.

Typically, for residential projects located near roadways with substantial TAC emissions, the primary TAC of concern with non-cancer health effects is diesel particulate matter (DPM). For DPM, the chronic inhalation REL is 5 micrograms per cubic meter $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$.

## Annual PM 2.5 Concentrations

While not a TAC, fine particulate matter ( $\mathrm{PM}_{2.5}$ ) has been identified by the BAAQMD as a pollutant with potential non-cancer health effects that should be included when evaluating potential community health impacts under the California Environmental Quality Act (CEQA). The thresholds of significance for $\mathrm{PM}_{2.5}$ (project level and cumulative) are in terms of an increase in the annual average concentration. When considering $\mathrm{PM}_{2.5}$ impacts, the contribution from all sources of $\mathrm{PM}_{2.5}$ emissions should be included. For projects with potential impacts from nearby local roadways, the $\mathrm{PM}_{2.5}$ impacts should include those from vehicle exhaust emissions, $\mathrm{PM}_{2.5}$ generated from vehicle tire and brake wear, and fugitive emissions from re-suspended dust on the roads.

## Attachment 3: Project Community Risk Assessment

Ghilotti - Santa Rosa, CA
DPM Emissions and Modeling Emission Rates - Unmitigated

| Emissions <br> Model <br> Year | Activity | $\begin{gathered} \text { DPM } \\ \text { (ton/year) } \end{gathered}$ | Area <br> Source | DPM Emissions |  |  | Modeled <br> Area $\left(\mathrm{m}^{2}\right)$ | DPMEmissionRate$\left(\mathrm{g} / \mathrm{s} / \mathrm{m}^{2}\right)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | (lb/yr) | (lb/hr) | (g/s) |  |  |
| 2017 | North Trucks | 0.0009 | DPM_N_T | 1.8 | 0.00046 | 5.77E-05 | 6,989 | 8.26E-09 |
| 2017 | North Equipment | 0.0046 | DPM_N_E | 9.2 | 0.00229 | $2.89 \mathrm{E}-04$ | 8,010 | $3.60 \mathrm{E}-08$ |
| 2017 | Crushing Equip | 0.0430 | DPM_C_E | 86.0 | 0.02142 | 2.70E-03 | 9,752 | $2.77 \mathrm{E}-07$ |
| 2017 | Crushing Trucks | 0.0008 | DPM_C_T | 1.7 | 0.00041 | $5.21 \mathrm{E}-05$ | 24,889 | $2.09 \mathrm{E}-09$ |
| Total |  | 0.0494 |  | 99 | 0.0246 | 0.0031 |  |  |

Operation Hours

| $\mathrm{hr} /$ day $=$ | 11 | $(6 \mathrm{am}-5 \mathrm{pm})$ |
| ---: | :---: | ---: |
| days/yr $=$ | 365 |  |
| hours/year $=$ | 4015 |  |

PM2.5 Fugitive Dust Emissions for Modeling - Unmitigated

| Construction |  |  |  |  |  |  |  | PM2.5 <br> Modeled <br> Emission |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Year |  |  |  |  |  |  |  |  |

Note: * Wind erosion emissions assumed to occur during any hour of the day

| Operation Hours |  |  |
| :---: | :---: | :---: |
| hr/day = | 11 | (6am - 5pm) |
| days/yr = | 365 |  |
| hours/year = | 4015 |  |

Ghilotti - Santa Rosa, CA - Facility Health Impact Summary
Maximum Impacts at Off-Site Residences

| Emissions Year | Maximum Concentrations |  | Cancer Risk (per million) |  | Hazard Index$(-)$ | Maximum Annual PM2.5 Concentration $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Exhaust PM10/DPM $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ | Fugitive PM2.5$\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ |  |  |  |  |
|  |  |  | Child | Adult |  |  |
| 2017 | 0.0154 | 0.2276 | 9.1 | 1.3 | 0.003 | 0.243 |

Ghilotti - 304 Todd Road, Santa Rosa, CA - Construction Impacts
Maximum DPM Cancer Risk Calculations From Construction
Off-Site Residential Receptor Locations - $\mathbf{1 . 5}$ meters


Construction Cancer Risk by Year - Maximum Impact Receptor Location

| Exposure Year | Exposure Duration (years) | Age | Infant/Child - Exposure Information |  |  | $\begin{aligned} & \hline \text { Infant/Child } \\ & \text { Cancer } \\ & \text { Risk } \\ & \text { (per million) } \\ & \hline \end{aligned}$ | Adult - Exposure Information |  |  | AdultCancerRisk(per million) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | DPM Conc (ug/m3) |  | Age Sensitivity Factor |  | Modeled |  | Age Sensitivity Factor |  |
|  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | Year | Annual |  |  | Year | Annual |  |  |
| 0 | 0.25 | -0.25-0* | 2017 | 0.0154 | 10 | 0.18 | 2017 | 0.0154 | - | - |
| 1 | 1 | 0-1 | 2017 | 0.0154 | 10 | 2.15 | 2017 | 0.0154 | 1 | 0.04 |
| 2 | 1 | 1-2 | 2018 | 0.0154 | 10 | 2.15 | 2018 | 0.0154 | 1 | 0.04 |
| 3 | 1 | 2-3 | 2019 | 0.0154 | 3 | 0.29 | 2019 | 0.0154 | 1 | 0.04 |
| 4 | 1 | 3-4 |  | 0.0154 | 3 | 0.29 | 2020 | 0.0154 | 1 | 0.04 |
| 5 | 1 | 4-5 |  | 0.0154 | 3 | 0.29 | 2021 | 0.0154 | 1 | 0.04 |
| 6 | 1 | 5-6 |  | 0.0154 | 3 | 0.29 | 2022 | 0.0154 | 1 | 0.04 |
| 7 | 1 | 6-7 |  | 0.0154 | 3 | 0.29 | 2023 | 0.0154 | 1 | 0.04 |
| 8 | 1 | 7-8 |  | 0.0154 | 3 | 0.29 | 2024 | 0.0154 | 1 | 0.04 |
| 9 | 1 | 8-9 |  | 0.0154 | 3 | 0.29 | 2025 | 0.0154 | 1 | 0.04 |
| 10 | 1 | 9-10 |  | 0.0154 | 3 | 0.29 | 2026 | 0.0154 | 1 | 0.04 |
| 11 | 1 | 10-11 |  | 0.0154 | 3 | 0.29 | 2027 | 0.0154 | 1 | 0.04 |
| 12 | 1 | 11-12 |  | 0.0154 | 3 | 0.29 | 2028 | 0.0154 | 1 | 0.04 |
| 13 | 1 | 12-13 |  | 0.0154 | 3 | 0.29 | 2029 | 0.0154 | 1 | 0.04 |
| 14 | 1 | 13-14 |  | 0.0154 | 3 | 0.29 | 2030 | 0.0154 | 1 | 0.04 |
| 15 | 1 | 14-15 |  | 0.0154 | 3 | 0.29 | 2031 | 0.0154 | 1 | 0.04 |
| 16 | 1 | 15-16 |  | 0.0154 | 3 | 0.29 | 2032 | 0.0154 | 1 | 0.04 |
| 17 | 1 | 16-17 |  | 0.0154 | 1 | 0.04 | 2033 | 0.0154 | 1 | 0.04 |
| 18 | 1 | 17-18 |  | 0.0154 | 1 | 0.04 | 2034 | 0.0154 | 1 | 0.04 |
| 19 | 1 | 18-19 |  | 0.0154 | 1 | 0.04 | 2035 | 0.0154 | 1 | 0.04 |
| 20 | 1 | 19-20 |  | 0.0154 | 1 | 0.04 | 2036 | 0.0154 | 1 | 0.04 |
| 21 | 1 | 20-21 |  | 0.0154 | 1 | 0.04 | 2037 | 0.0154 | 1 | 0.04 |
| 22 | 1 | 21-22 |  | 0.0154 | 1 | 0.04 | 2038 | 0.0154 | 1 | 0.04 |
| 23 | 1 | 22-23 |  | 0.0154 | 1 | 0.04 | 2039 | 0.0154 | 1 | 0.04 |
| 24 | 1 | 23-24 |  | 0.0154 | 1 | 0.04 | 2040 | 0.0154 | 1 | 0.04 |
| 25 | 1 | 24-25 |  | 0.0154 | 1 | 0.04 | 2041 | 0.0154 | 1 | 0.04 |
| 26 | 1 | 25-26 |  | 0.0154 | 1 | 0.04 | 2042 | 0.0154 | 1 | 0.04 |
| 27 | 1 | 26-27 |  | 0.0154 | 1 | 0.04 | 2043 | 0.0154 | 1 | 0.04 |
| 28 | 1 | 27-28 |  | 0.0154 | 1 | 0.04 | 2044 | 0.0154 | 1 | 0.04 |
| 29 | 1 | 28-29 |  | 0.0154 | 1 | 0.04 | 2045 | 0.0154 | 1 | 0.04 |
| 30 | 1 | 29-30 |  | 0.0154 | 1 | 0.04 | 2046 | 0.0154 | 1 | 0.04 |
| Total Increased Cancer Risk |  |  |  |  |  | 9.10 |  |  |  | 1.32 |

Fugitive Total
PM2.5 PM2.5
$0.2276 \quad 0.243$

# 304 Todd Road - Ghiolotti Yard (Yellow and Green Area) Sonoma-San Francisco County, Annual Onsite Emissions Only 

### 1.0 Project Characteristics

### 1.1 Land Usage

| Industrial Park | 1.00 | 1000sqft | 19.00 | 1,000.00 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: |

### 1.2 Other Project Characteristics

| Urbanization | Urban | Wind Speed (m/s) | 2.2 | Precipitation Freq (Days) <br> Operational Year | 2019 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Climate Zone | 4 |  |  |  |  |
| Utility Company | Pacific Gas \& Electric Company |  |  |  |  |
| CO2 Intensity <br> (Ib/MWhr) | 430 | CH4 Intensity <br> (Ib/MWhr) | 0.029 | N2O Intensity <br> (Ib/MWhr) | 0.006 |

### 1.3 User Entered Comments \& Non-Default Data

Project Characteristics - PG\&E current rate
Land Use - No real structures on site
Construction Phase - Use construction to model annual operational emissions
Off-road Equipment - based on provided list
Off-road Equipment - Based on provided list
Trips and VMT - Assumes 15 roundtrips per day for 266 trips per year at 20 miles per trip. Assume 3 workers per average day (or 10 daily trips) Grading - Assumes each acre is disturbed daily
Vehicle Trips - Using construciton to model operational since construction yard
Construction Off-road Equipment Mitigation - Used project equipment list that includes Tier level

| Table Name | Column Name | Default Value | New Value |
| :---: | :---: | :---: | :---: |
| tblConstDustMitigation | WaterUnpavedRoadVehicleSpeed | 40 | 15 |
|  |  | 0.00 | 4.00 |
| tbiConstEquipMitigation | NumberOfEquipmentMitigated | 0.00 | 2.00 |
| tbiConstEquipMitigation | NumberOfEquipmentMitigated | 0.00 | 2.00 |
|  |  | 0.00 | 1.00 |
| tbiConstEquipMitigation | Tier | No Change | Tier 4 Interim |
| tbiConstEquipMitigation | Tier | No Change | Tier 3 |
|  | Tier | No Change | Tier 3 |
| tbiConstEquipMitigation | Tier | No Change | Tier 2 |
| tbiConstEquipMitigation | Tier | No Change | Tier 2 |
| tbiConstEquipMitio.......................... | Tier | No Change | Tier 2 |
| tbiConstEquipMitigation | Tier | No Change | Tier 2 |
| tblConstructionPhase | NumDays | 10.00 | 260.00 |
| tblGrading | AcresOfGrading | 6.50 | 33.15 |
| tbiLandUse | LotAcreage | 0.02 | 19.00 |
| tbIOffRoadEquipment | OffRoadEquipmentUnitAmount | 3.00 | 0.00 |
| tbiOffRoadEquipment | OffRoadEquipmentUnitAmount | 4.00 | 0.00 |
| tblProjectCharacteristics | CO2IntensityFactor | 641.35 | 430 |
| tblProjectCharacteristics | OperationalYear | 2018 | 2019 |
| tbiTripsAndVMT | HaulingTripLength | 20.00 | 0.25 |
| tbiTripsAndVMT | Hauling TripNumber | 0.00 | 7,980.00 |


| tblTripsAndVMT | VendorTripLength | 7.30 | 0.25 |
| :---: | :---: | :---: | :---: |
| tblTripsAndVMT | WorkerTripLength | 10.80 | 0.25 |
| tblicripsAndVMT | WorkerTripNumber | 25.00 | 10.00 |
| tbivehicleTrips | ST_TR | 2.49 | 0.01 |
| tbiVehicleTrips | SU_TR | 0.73 | 0.01 |
| tblVehicleTrips | WD_TR | 6.83 | 0.01 |

### 2.0 Emissions Summary

### 2.1 Overall Construction

Unmitigated Construction


## Mitigated Construction




### 3.0 Construction Detail

## Construction Phase

| Phase Number | Phase Name | Phase Type | Start Date | End Date | Num Days Week | Num Days | Phase Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Site Preparation | Site Preparation | 1/1/2017 | 12/29/2017 | 5 | 260 |  |

## Acres of Grading (Site Preparation Phase): 33.15

Acres of Grading (Grading Phase): 0

## Acres of Paving: 0

Residential Indoor: 0; Residential Outdoor: 0; Non-Residential Indoor: 0; Non-Residential Outdoor: 0; Striped Parking Area: 0
OffRoad Equipment

| Phase Name | Offroad Equipment Type | Amount | Usage Hours | Horse Power | Load Factor |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Site Preparation | Air Compressors | 4 | 0.10 | 78 | 0.48 |
| Site Preparation | Crawler Tractors | 2 | 0.20 | 212 | 0.43 |
| Site Preparation | Excavators | 2 | 0.20 | 158 | 0.38 |
| Site Preparation | Forklifts | 1 | 2.00 | 89 | 0.20 |
| Site Preparation | Other Construction Equipment | 0 | 0.50 | 172 | 0.42 |
| Site Preparation | Other General Industrial Equipment | 0 | 0.50 | 88 | 0.34 |
| Site Preparation | Other Material Handling Equipment | 1 | 0.20 | 168 | 0.40 |
| Site Preparation | Rubber Tired Dozers | 0 | 8.00 | 247 | 0.40 |
| Site Preparation | Tractors/Loaders/Backhoes | 0 | 8.00 | 97 | 0.37 |

## Trips and VMT

| Phase Name | Offroad Equipment Count | Worker Trip Number | Vendor Trip Number | Hauling Trip Number | Worker Trip Length | Vendor Trip Length | $\begin{aligned} & \text { Hauling Trip } \\ & \text { Length } \end{aligned}$ | Worker Vehicle Class | Vendor Vehicle Class | Hauling Vehicle Class |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Site Preparation | 10 | 10.00 | 0.00 | 7,980.00 | 0.25 | 0.25 | 0.25 | D_Mix | [HDT_Mix | HHDT |

### 3.1 Mitigation Measures Construction

Use Cleaner Engines for Construction Equipment
Use Soil Stabilizer
Reduce Vehicle Speed on Unpaved Roads
Clean Paved Roads

### 3.2 Site Preparation-2017

## Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | $\begin{aligned} & \text { Fugitive } \\ & \text { PM10 } \end{aligned}$ | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | $\begin{gathered} \text { NBio- } \\ \text { CO2 } \end{gathered}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 0.0176 | 0.0000 | 0.0176 | $\begin{gathered} 1.9000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | $\begin{gathered} 1.9000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | 0.0182 | 0.1812 | 0.1096 | $\begin{gathered} 1.8000 \mathrm{e}- \\ 004 \end{gathered}$ |  | 0.0109 | 0.0109 |  | 0.0101 | 0.0101 | 0.0000 | 16.4131 | 16.4131 | ${ }^{4.5800 e-}$ | 0.0000 | 16.5278 |
| Total | 0.0182 | 0.1812 | 0.1096 | $\begin{gathered} 1.8000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0176 | 0.0109 | 0.0285 | $\begin{gathered} 1.9000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0101 | 0.0120 | 0.0000 | 16.4131 | 16.4131 | $\begin{gathered} 4.5800 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 16.5278 |

## Unmitigated Construction Off-Site

|  | ROG | NOX | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust <br> PM2.5 | PM2.5 <br> Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0108 | 0.4054 | 0.0858 | $\begin{gathered} 3.4000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 9.1000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 9.1000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 1.8200 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 2.6000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 8.7000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{aligned} & 1.1300 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.0000 | 33.2627 | 33.2627 | $8.1000 \mathrm{e}-$ 003 | 0.0000 | 33.4651 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | $\begin{gathered} 2.3900 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.0300 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0142 | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 2.5000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e} \\ 005 \end{gathered}$ | $\begin{aligned} & 2.6000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 7.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{aligned} & 8.0000 \mathrm{e}- \\ & 005 \end{aligned}$ | 0.0000 | 0.5235 | 0.5235 | 8.0000 e 005 | 0.0000 | 0.5254 |
| Total | 0.0132 | 0.4065 | 0.0999 | $\begin{gathered} 3.5000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 1.1600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 9.2000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 2.0800 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.3000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 8.8000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 1.2100 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 33.7862 | 33.7862 | $\begin{gathered} 8.1800 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 33.9905 |


|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- $\mathrm{CO} 2$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 0.0176 | 0.0000 | 0.0176 | $\begin{gathered} 1.9000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | $\begin{gathered} 1.9000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | $6.5400 \mathrm{e}-$ 003 | 0.1152 | 0.1192 | $1.8000 \mathrm{e}-$ 004 |  | $4.6000 \mathrm{e}-$ 003 | 4.6000e- 003 |  | 4.5300e- 003 | 4.5300e- 003 | 0.0000 | 16.4131 | 16.4131 | 4.5800e- 003 | 0.0000 | 16.5277 |
| Total | $\begin{gathered} 6.5400 \mathrm{e}- \\ 003 \end{gathered}$ | 0.1152 | 0.1192 | $\begin{gathered} 1.8000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0176 | $\begin{gathered} 4.6000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0222 | $\begin{gathered} 1.9000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 4.5300 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 6.4300 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 16.4131 | 16.4131 | $\begin{gathered} 4.5800 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 16.5277 |

## Mitigated Construction Off-Site

|  | ROG | NOX | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0108 | 0.4054 | 0.0858 | $\begin{gathered} 3.4000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 9.1000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 9.1000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 1.8200 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 2.6000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 8.7000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 1.1300 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 33.2627 | 33.2627 | $8.1000 \mathrm{e}-$ 003 | 0.0000 | 33.4651 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | $2.3900 \mathrm{e}-$ 003 | $\begin{gathered} 1.0300 \mathrm{e} \\ 003 \end{gathered}$ | 0.0142 | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 2.5000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 2.6000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{aligned} & 7.0000 \mathrm{e} \\ & 005 \end{aligned}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 8.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | 0.5235 | 0.5235 | $8.0000 \mathrm{e}-$ 005 | 0.0000 | 0.5254 |
| Total | 0.0132 | 0.4065 | 0.0999 | $\begin{gathered} 3.5000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 1.1600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 9.2000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{array}{\|c\|} \hline 2.0800 \mathrm{e}- \\ 003 \end{array}$ | $\begin{gathered} 3.3000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 8.8000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 1.2100 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 33.7862 | 33.7862 | $\begin{gathered} 8.1800 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 33.9905 |

Attachment 4: Cumulative Source Community Risk Assessment


## Roadway Screening Analysis Calculator



## Notes and Refere

1. Emissions were developed using EMFAC2011 for fleet mix in 2014 assuming 10,000 AADT and includes impacts from diesel and gasoline vehicle exhaust, brake and tire wear, and resuspended dus.
2. Roadways were modeled using EALNE Cal3qhcr air dispersion model assuming a source length of one kilometer. Meteorological data used to estimate the screening values are noted at the bottom of the "Results" box.
3. Cancer risks were estimated for 70 year lifetime exposure starting in 2014 that includes sensitivity values for early life exposures and OEHHA toxicity values adopted in 2013
```
Syar Industries Emission data obtained from BAAQMD
BAY AREA AIR QUALITY MANAGEMENT DISTRICT Printed: NOV 3,2016
DETAIL POLLUTANTS - ABATED
MOST RECENT P/O APPROVED (2016)
Syar Industries Inc (P# 2157)
```



```
22 Asphalt Drum Mixer
    C2830189
            Benzene 41 6.07E-04
            Formaldehyde 124 7.13E-03
            Toluene 293 3.23E-04
            Organics (other, including 990 5.44E-01
            Particulates (part not spe 1990 2.85E-03
            Nitrous Oxide (N2O) 2030 2.20E-02
            Nitrogen Oxides (part not 2990 3.81E-01
            Sulfur Dioxide (SO2) }3990\mathrm{ 5.41E-02
            Carbon Monoxide (CO) pollu 4990 5.71E+00
            Carbon Dioxide, non-biogen 6960 1.17E+04
            Methane (CH4) }6970\mathrm{ 1.81E-01
        G4077030
            Organics (other, including 990 9.29E+00
            Particulates (part not spe 1990 2.95E+00
            Nitrogen Oxides (part not 2990 9.29E+00
            Sulfur Dioxide (SO2) }3990\mathrm{ 9.62E+00
            Carbon Monoxide (CO) pollu 4990 8.96E+00
23 Asphalt Storage Tank Model C-TA-30E/DC, 30,000 Gal
    T43??030
            Asphalt 30 0.00E+00
24 Asphalt Storage Tank, 30,000 Gallon, with Natural Gas Heater
    T43??030
            Asphalt 30 0.00E+00
PLANT TOTAL:
lbs/day Pollutant
0.00E+00 Asphalt (30)
9.63E-04 Benzene (41)
1.85E+04 Carbon Dioxide, non-biogenic CO2 (6960)
1.66E+01 Carbon Monoxide (CO) pollutant (4990)
1.55E-02 Distillate oil (315)
1.13E-02 Formaldehyde (124)
2.87E-01 Methane (CH4) (6970)
1.75E+01 Nitrogen Oxides (part not spec elsewhere) (2990)
3.49E-02 Nitrous Oxide (N2O) (2030)
1.02E+01 Organics (other, including CH4) (990)
1.09E+02 Particulates (part not spec elsewhere) (1990)
9.71E+00 Sulfur Dioxide (SO2) (3990)
5.13E-04 Toluene (293)
```

Ghilotti Cumulative Sources - Sonoma-San Francisco County, Annual
Ghilotti Cumulative Sources

## Sonoma-San Francisco County, Annual

Syar Off Road and Trucks

### 1.0 Project Characteristics

### 1.1 Land Usage

| Industrial Park | 1.00 | 1000sqft | 10.00 | 1,000.00 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: |

### 1.2 Other Project Characteristics

| Urbanization | Urban | Wind Speed (m/s) | 2.2 | Precipitation Freq (Days) <br> Operational Year | 2018 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Climate Zone | 4 |  |  |  |  |
| Utility Company | Pacific Gas \& Electric Company |  |  |  |  |
| CO2 Intensity <br> (Ib/MWhr) | 430 | CH4 Intensity <br> (Ib/MWhr) | 0.029 | N2O Intensity <br> (Ib/MWhr) | 0.006 |

### 1.3 User Entered Comments \& Non-Default Data

Project Characteristics - current PG\&E factor
Land Use - Use Industrial Park - emissions computed based on construction Construction Phase - Using construciton to compute equipment and truck traffic
Off-road Equipment -
Off-road Equipment - Based on estimated equipment
Trips and VMT - Estimated average daily condition of 200 truck trips/day

| tblConstructionPhase | NumDays | 10.00 | 260.00 |
| :---: | :---: | :---: | :---: |
| tbigrading | AcresOfGrading | 130.00 | 0.00 |
| tbiLandUse | LotAcreage | 0.02 | 10.00 |
| tblOffRoadEquipment | OffRoadEquipmentUnitAmount | 3.00 | 4.00 |
| tbiOffRoadEquipment | OffRoadEquipmentUnitAmount | 4.00 | 0.00 |
| tblProjectCharacteristics | CO2IntensityFactor | 641.35 | 430 |
| tbiTripsAndVMT | HaulingTripLength | 20.00 | 0.50 |
| tbiTripsAndVMT | Hauling TripNumber | 0.00 | 53,200.00 |
| tbiTripsAndVMT | VendorTripLength | 7.30 | 0.50 |
| tbiTripsAndVMT | WorkerTripLength | 10.80 | 0.50 |
| tbiTripsAndVMT | WorkerTripNumber | 15.00 | 20.00 |

### 2.0 Emissions Summary

### 2.1 Overall Construction

Unmitigated Construction

|  | ROG | NOX | CO | SO2 | Fugitive PM10 | $\begin{gathered} \hline \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | $\begin{aligned} & \hline \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBioCO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Year | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| 2017 | 0.8564 | 11.4621 | 3.8258 | $\begin{gathered} 8.6800 \mathrm{e}- \\ 003 \end{gathered}$ | 3.1440 | 0.4183 | 3.5623 | 1.7248 | 0.3851 | 2.1099 | 0.0000 | 816.5463 | 816.5463 | 0.2297 | 0.0000 | 822.2875 |
| Maximum | 0.8564 | 11.4621 | 3.8258 | $\begin{gathered} 8.6800 \mathrm{e}- \\ 003 \end{gathered}$ | 3.1440 | 0.4183 | 3.5623 | 1.7248 | 0.3851 | 2.1099 | 0.0000 | 816.5463 | 816.5463 | 0.2297 | 0.0000 | 822.2875 |

## Mitigated Construction



| Quarter | Start Date | End Date | Maximum Unmitigated ROG + NOX (tons/quarter) | Maximum Mitigated ROG + NOX (tons/quarter) |
| :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | $\mathbf{1 1 - 2 9 - 2 0 1 6}$ | $\mathbf{2 - 2 7 - 2 0 1 7}$ | 1.9548 | 1.9548 |
| 2 | $2-28-2017$ | $5-28-2017$ | 3.0465 | 3.0465 |
| 3 | $5-29-2017$ | $8-28-2017$ | 3.1217 | 3.1217 |
| 4 | $8-29-2017$ | $9-30-2017$ | 1.1197 | 1.1197 |
|  |  | Highest | 3.1217 | 3.1217 |

### 3.0 Construction Detail

## Construction Phase

| Phase Number | Phase Name | Phase Type | Start Date | End Date | Num Days Week | Num Days | Phase Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Site Preparation | Site Preparation | 1/1/2017 | 12/29/2017 | 5 | 260 |  |

## Acres of Grading (Site Preparation Phase): 0

Acres of Grading (Grading Phase): 0
Acres of Paving: 0
Residential Indoor: 0; Residential Outdoor: 0; Non-Residential Indoor: 0; Non-Residential Outdoor: 0; Striped Parking Area: 0
OffRoad Equipment

| Phase Name | Offroad Equipment Type | Amount | Usage Hours | Horse Power | Load Factor |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Site Preparation | Crawler Tractors | 1 | 8.00 | 212 | 0.43 |
| Site Preparation | Excavators | 1 | 8.00 | 158 | 0.38 |
| Site Preparation | Rubber Tired Dozers | 4 | 8.00 | 247 | 0.40 |
| Site Preparation | Tractors/Loaders/Backhoes | 0 | 8.00 | 97 | 0.37 |

## Trips and VMT

| Phase Name | $\begin{aligned} & \text { Offroad Equipment } \\ & \text { Count } \end{aligned}$ | Worker Trip Number | Vendor Trip Number | Hauling Trip <br> Number | Worker Trip Length | Vendor Trip Length | Hauling Trip Length | Worker Vehicle Class | Vendor Vehicle Class | Hauling Vehicle Class |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Site Preparation | 6 | 20.00 | 0.00 | 53,200.00 | 0.50 | 0.50 | 0.50 | LD_Mix | [HDT_Mix | HHDT |

### 3.1 Mitigation Measures Construction

|  | ROG | NOX | CO | SO2 | Fugitive PM10 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 3.1315 | 0.0000 | 3.1315 | 1.7213 | 0.0000 | 1.7213 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | 0.7759 | 8.6638 | 3.2037 | $\begin{gathered} 6.1300 \mathrm{e} \\ 003 \end{gathered}$ |  | 0.4113 | 0.4113 |  | 0.3784 | 0.3784 | 0.0000 | 569.3117 | 569.3117 | 0.1744 | 0.0000 | 573.6726 |
| Total | 0.7759 | 8.6638 | 3.2037 | $\begin{gathered} \text { 6.1300e- } \\ 003 \end{gathered}$ | 3.1315 | 0.4113 | 3.5427 | 1.7213 | 0.3784 | 2.0997 | 0.0000 | 569.3117 | 569.3117 | 0.1744 | 0.0000 | 573.6726 |

## Unmitigated Construction Off-Site

|  | ROG | NOX | CO | SO2 | $\begin{aligned} & \text { Fugitive } \\ & \text { PM10 } \end{aligned}$ | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 <br> Tota | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0754 | 2.7960 | 0.5913 | $\begin{gathered} 2.5300 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0116 | $\begin{gathered} 7.0100 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0186 | $\begin{gathered} 3.2200 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 6.7000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{array}{\|c} \hline 9.9200 \mathrm{e}- \\ 003 \end{array}$ | 0.0000 | 245.7261 | 245.7261 | 0.0550 | 0.0000 | 247.1021 |
| Vendor | $0.0000$ | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | $5.0500 \mathrm{e}-$ 003 | $\begin{gathered} 2.3200 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0307 | $\begin{gathered} 2.00000- \\ 005 \end{gathered}$ | $\begin{gathered} 9.7000 \mathrm{e} \\ 004 \end{gathered}$ | $\begin{gathered} 3.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 1.00000- \\ 003 \end{gathered}$ | $\begin{gathered} 2.60000=- \\ 004 \end{gathered}$ | $\begin{gathered} 3.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 2.9000 \mathrm{e}-\mathrm{C} \\ 004 \end{gathered}$ | 0.0000 | 1.5085 | 1.5085 | 1.7000 e 004 | 0.0000 | 1.5129 |
| Total | 0.0804 | 2.7983 | 0.6221 | $\begin{gathered} 2.5500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0125 | $\begin{gathered} 7.0400 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0196 | $\begin{gathered} 3.4800 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 6.7300 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0102 | 0.0000 | 247.2346 | 247.2346 | 0.0552 | 0.0000 | 248.6149 |

## Mitigated Construction On-Site

|  | ROG | NOX | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBioCO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 3.1315 | 0.0000 | 3.1315 | 1.7213 | 0.0000 | 1.7213 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | 0.7759 | 8.6638 | 3.2037 | $\begin{gathered} 6.1300 \mathrm{e}- \\ 003 \end{gathered}$ |  | 0.4113 | 0.4113 |  | 0.3784 | 0.3784 | 0.0000 | 569.3110 | 569.3110 | 0.1744 | 0.0000 | 573.6719 |
| Total | 0.7759 | 8.6638 | 3.2037 | $\begin{gathered} \text { 6.1300e- } \\ 003 \end{gathered}$ | 3.1315 | 0.4113 | 3.5427 | 1.7213 | 0.3784 | 2.0997 | 0.0000 | 569.3110 | 569.3110 | 0.1744 | 0.0000 | 573.6719 |

## Mitigated Construction Off-Site

|  | ROG | NOX | CO | SO2 | $\begin{aligned} & \text { Fugitive } \\ & \text { PM10 } \end{aligned}$ | $\begin{array}{\|c} \hline \text { Exhaust } \\ \text { PM10 } \end{array}$ | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0754 | 2.7960 | 0.5913 | $\begin{gathered} 2.5300 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0116 | $\begin{array}{\|c} \hline 7.0100 \mathrm{e}- \\ 003 \end{array}$ | 0.0186 | $\begin{gathered} 3.2200 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 6.7000 e- \\ 003 \end{gathered}$ | $\begin{gathered} 9.9200 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 245.7261 | 245.7261 | 0.0550 | 0.0000 | 247.1021 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | $\begin{gathered} 5.0500 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 2.3200 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0307 | $\begin{gathered} 2.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 9.7000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 3.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 2.6000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 3.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 2.9000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 1.5085 | 1.5085 | $\begin{gathered} 1.7000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 1.5129 |
| Total | 0.0804 | 2.7983 | 0.6221 | $\begin{gathered} 2.5500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0125 | $\begin{gathered} 7.0400 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0196 | $\begin{gathered} 3.4800 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 6.7300 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0102 | 0.0000 | 247.2346 | 247.2346 | 0.0552 | 0.0000 | 248.6149 |

Ghilotti Cumulative Sources - Sonoma-San Francisco County, Annual
Ghilotti Cumulative Sources
Sonoma-San Francisco County, Annual
Ghilotti Yard adjacent to site

### 1.0 Project Characteristics

### 1.1 Land Usage

| Land Uses | Size | Metric | Lot Acreage | Floor Surface Area | Population |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Industrial Park | 1.00 | 1000 sqft | 10.00 | $1,000.00$ |  |

### 1.2 Other Project Characteristics

| Urbanization | Urban | Wind Speed (m/s) | 2.2 | Precipitation Freq (Days) <br> Operational Year | 2018 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Climate Zone | 4 |  |  |  |  |
| Utility Company | Pacific Gas \& Electric Company |  |  |  |  |
| CO2 Intensity <br> (Ib/MWhr) | 430 | CH4 Intensity <br> (Ib/MWhr) | 0.029 | N2O Intensity <br> (Ib/MWhr) | 0.006 |

### 1.3 User Entered Comments \& Non-Default Data

Project Characteristics - current PG\&E factor
Land Use - Use Industrial Park - emissions computed based on construction Construction Phase - Using construciton to compute equipment and truck traffic
Off-road Equipment -
Off-road Equipment - Based on estimated equipment
Trips and VMT - Estimated average daily condition

| Table Name | Column Name | Default Value | New Value |
| :---: | :---: | :---: | :---: |
| tblConstructionPhase | NumDays | 10.00 | 260.00 |
| tbiConstructionPhase | PhaseEndDate | 11/28/2016 | 12/29/2017 |
| tblConstructionPhase | PhaseStartDate | 11/29/2016 | 1/1/2017 |
| tbiLandUse | LotAcreage | 0.02 | 10.00 |
| tblOffRoadEquipment | LoadFactor | 0.20 | 0.20 |
| tblOffRoadEquipment | OffRoadEquipment ${ }^{\text {ape }}$ |  | Crawler Tractors |
| tblOffRoadEquipment | OffRoadEquipmentType |  | Excavators |
| tblOffRoadEquipment | OffRoadEquipmentType |  | Forklifts |
| tblOffRoadEquipment | OffRoadEquipmentUnitAmount | 4.00 | 0.00 |
| tblOffRoadEquipment | OffRoadEquipmentUnitAmount | 3.00 | 0.00 |
| tblProjectCharacteristics | CO2IntensityFactor | 641.35 | 430 |
| tbiTripsAndVMT | HaulingTripLength | 20.00 | 0.25 |
| tbiTripsAndVMT | Hauling TripNumber | 0.00 | 26,600.00 |
| tbiTripsAndVMT | VendorTripLength | 7.30 | 0.25 |
| tbiTripsAndVMT | WorkerTripLength | 10.80 | 0.25 |
| tbiTripsAndVMT | WorkerTripNumber | 3.00 | 20.00 |

### 2.0 Emissions Summary

### 2.1 Overall Construction

## Unmitigated Construction

|  | ROG | NOX | CO | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | $\begin{gathered} \hline \text { Exhaust } \\ \text { PM2.5 } \end{gathered}$ | $\begin{gathered} \hline \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | NBioCO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Year | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| 2017 | 0.0684 | 1.5921 | 0.4774 | $\begin{gathered} 1.3500 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.5200 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0228 | 0.0263 | $\begin{gathered} 9.9000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0210 | 0.0220 | 0.0000 | 130.4424 | 130.4424 | 0.0328 | 0.0000 | 131.2629 |
| Maximum | 0.0684 | 1.5921 | 0.4774 | $\begin{gathered} 1.3500 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.5200 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0228 | 0.0263 | $\begin{gathered} 9.9000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0210 | 0.0220 | 0.0000 | 130.4424 | 130.4424 | 0.0328 | 0.0000 | 131.2629 |

## Mitigated Construction



| Quarter | Start Date | End Date | Maximum Unmitigated ROG + NOX (tons/quarter) | Maximum Mitigated ROG + NOX (tons/quarter) |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 11-29-2016 | 2-27-2017 | 0.2604 | 0.2604 |
| 2 | 2-28-2017 | 5-28-2017 | 0.4112 | 0.4112 |
| 3 | 5-29-2017 | 8-28-2017 | 0.4243 | 0.4243 |
| 4 | 8-29-2017 | 9-30-2017 | 0.1522 | 0.1522 |
|  |  | Highest | 0.4243 | 0.4243 |

### 3.0 Construction Detail

## Construction Phase

| Phase Number | Phase Name | Phase Type | Start Date | End Date | Num Days Week | Num Days | Phase Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Site Preparation | Site Preparation | 1/1/2017 | 12/29/2017 | 5 | 260 |  |

## Acres of Grading (Site Preparation Phase): 0

Acres of Grading (Grading Phase): 0

## Acres of Paving: 0

Residential Indoor: 0; Residential Outdoor: 0; Non-Residential Indoor: 0; Non-Residential Outdoor: 0; Striped Parking Area: 0
OffRoad Equipment

| Phase Name | Offroad Equipment Type | Amount | Usage Hours | Horse Power | Load Factor |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Site Preparation | Crawler Tractors | 0 | 8.00 | 212 | 0.43 |
| Site Preparation | Excavators | 0 | 8.00 | 158 | 0.38 |
| Site Preparation | Forklifts | 1 | 8.00 | 89 | 0.20 |
| Site Preparation | Tractors/Loaders/Backhoes | 0 | 8.00 | 97 | 0.37 |
| Site Preparation | Rubber Tired Dozers | 0 | 8.00 | 247 | 0.40 |

## Trips and VMT

| Phase Name | Offroad Equipment Count | Worker Trip Number | Vendor Trip Number | Hauling Trip Number | Worker Trip Length | Vendor Trip Length | Hauling Trip | Worker Vehicle Class | Vendor Vehicle Class | Hauling Vehicle Class |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Site Preparation | 1 | 20.00 | 0.00 | 26,600.00 | 0.25 | 0.25 | 0.25 | _Mix | [HDT_Mix | HHDT |

### 3.1 Mitigation Measures Construction

### 3.2 Site Preparation - 2017

## Unmitigated Construction On-Site

|  | ROG | NOX | CO | SO2 | $\begin{gathered} \text { Fugitive } \\ \text { PM10 } \end{gathered}$ | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | $\begin{aligned} & \text { Fugitive } \\ & \text { PM2.5 } \end{aligned}$ | $\begin{gathered} \text { Exhaust } \\ \text { PM2.5 } \end{gathered}$ | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | 0.0276 | 0.2386 | 0.1632 | $\begin{gathered} 2.0000 \mathrm{e}- \\ 004 \end{gathered}$ |  | 0.0197 | 0.0197 |  | 0.0181 | 0.0181 | 0.0000 | 18.5199 | 18.5199 | $\begin{gathered} 5.6700 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 18.6618 |
| Total | 0.0276 | 0.2386 | 0.1632 | 2.0000e004 | 0.0000 | 0.0197 | 0.0197 | 0.0000 | 0.0181 | 0.0181 | 0.0000 | 18.5199 | 18.5199 | $5.6700 \mathrm{e}-$ 003 | 0.0000 | 18.6618 |

## Unmitigated Construction Off-Site

|  | ROG | NOX | CO | SO2 | Fugitive PM10 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBioCO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0361 | 1.3514 | 0.2858 | $\begin{gathered} 1.1400 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.0200 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.0400 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{array}{\|c} \hline 6.0700 \mathrm{e}- \\ 003 \end{array}$ | $\begin{gathered} 8.5000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 2.9100 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.7600 e- \\ 003 \end{gathered}$ | 0.0000 | 110.8755 | 110.8755 | 0.0270 | 0.0000 | 111.5503 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | $\begin{gathered} 4.7700 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 2.0500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0283 | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 5.0000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 3.0000 \mathrm{e}-\mathrm{e} \\ 005 \end{gathered}$ | $\begin{gathered} 5.2000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 1.4000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 2.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 1.6000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 1.0470 | 1.0470 | $\begin{gathered} 1.5000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 1.0509 |
| Total | 0.0408 | 1.3535 | 0.3142 | $\begin{gathered} 1.1500 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.5200 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.0700 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} \hline 6.5900 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 9.9000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 2.9300 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.9200 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 111.9225 | 111.9225 | 0.0271 | 0.0000 | 112.6012 |

## Mitigated Construction On-Site

|  | ROG | NOX | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBioCO2 | Total CO2 | CH4 | N2O | co2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | 0.0276 | 0.2386 | 0.1632 | $\begin{gathered} 2.0000 \mathrm{e}- \\ 004 \end{gathered}$ |  | 0.0197 | 0.0197 |  | 0.0181 | 0.0181 | 0.0000 | 18.5199 | 18.5199 | 5.6700 e 003 | 0.0000 | 18.6617 |
| Total | 0.0276 | 0.2386 | 0.1632 | $\begin{gathered} 2.0000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 0.0197 | 0.0197 | 0.0000 | 0.0181 | 0.0181 | 0.0000 | 18.5199 | 18.5199 | $\begin{gathered} 5.6700 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 18.6617 |

Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling |  | 1.3514 | 0.2858 | $\begin{gathered} 1.1400 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.0200 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.0400 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 6.0700 \mathrm{e}- \\ 003 \end{gathered}$ | 8.5000e- <br> 004 | $\begin{gathered} 2.9100 e- \\ 003 \end{gathered}$ | $3.7600 e-$ 003 | 0.0000 | 110.8755 | 110.8755 | 0.0270 | 0.0000 | 111.5503 |


| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Worker | $\begin{gathered} 4.7700 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 2.0500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0283 | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{aligned} & 5.0000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 3.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 5.2000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 1.4000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 2.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 1.6000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 1.0470 | 1.0470 | $\begin{gathered} 1.5000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 1.0509 |
| Total | 0.0408 | 1.3535 | 0.3142 | $\begin{gathered} 1.1500 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.5200 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.0700 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} \text { 6.5900e- } \\ 003 \end{gathered}$ | $\begin{gathered} 9.9000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 2.9300 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.9200 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 111.9225 | 111.9225 | 0.0271 | 0.0000 | 112.6012 |

## Air Quality Modeling Calculations



Syar Asphalt - Santa Rosa, CA
DPM Emissions and Modeling Emission Rates

| Emissions <br> Model <br> Year | Activity | $\begin{gathered} \text { DPM } \\ \text { (ton/year) } \end{gathered}$ | Area <br> Source | DPM Emissions |  |  | Modeled Area (m) | $\begin{gathered} \hline \text { DPM } \\ \text { Emission } \\ \text { Rate } \\ \left(\mathrm{g} / \mathrm{s} / \mathrm{m}^{2}\right) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | (lb/yr) | (lb/hr) | (g/s) |  |  |
| 2017 | Syar Equipment | 0.4183 | DPM_SYAR | 836.6 | 0.20837 | 2.63E-02 | 22,638 | 1.16E-06 |
| Total |  | 0.4183 |  | 836.6 | 0.2084 | 0.0263 |  |  |
| Operation Hours |  |  |  |  |  |  |  |  |
|  |  | hr/day = | 11 | (6am - 5 |  |  |  |  |
|  |  | days/yr = | 365 |  |  |  |  |  |
|  |  | hours/year = | 4015 |  |  |  |  |  |

Syar - Santa Rosa, CA - Facility Health Impact Summary
Maximum Impacts at Ghilotti Facility MEI Location

| Emissions <br> Year | Maximum Concentrations |  | Cancer Risk (per million) |  | Hazard Index$(-)$ | Maximum <br> Annual PM2.5 <br> Concentration <br> $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Exhaust <br> PM10/DPM <br> $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ | $\begin{gathered} \hline \text { Fugitive } \\ \text { PM2.5 } \\ \left(\mu \mathrm{g} / \mathbf{m}^{3}\right) \\ \hline \end{gathered}$ |  |  |  |  |
|  |  |  | Child | Adult |  |  |
| 2017 | 0.0554 | 0.4842 | 32.8 | 4.8 | 0.011 | 0.54 |

Syar - Santa Rosa, CA - On-Site Equipment \& Truck Operation Impacts
Maximum DPM Cancer Risk Calculations From Construction
Impacts at Ghilotti Facility MEI Location
Cancer Risk (per million) = CPF x Inhalation Dose x ASF x ED/AT x FAH x 1.0E6
Where: CPF $=$ Cancer potency factor $(\mathrm{mg} / \mathrm{kg} \text {-day })^{-1}$
ASF = Age sensitivity factor for specified age group
ED = Exposure duration (years)
AT = Averaging time for lifetime cancer risk (years)
FAH $=$ Fraction of time spent at home (unitless)
Inhalation Dose $=\mathrm{C}_{\text {air }} \times \mathrm{DBR} \times \mathrm{A} \times(\mathrm{EF} / 365) \times 10^{-6}$
Where: $\mathrm{C}_{\text {air }}=$ concentration in air $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$
DBR = daily breathing rate ( $\mathrm{L} / \mathrm{kg}$ body weight-day)
A = Inhalation absorption factor
$\mathrm{EF}=$ Exposure frequency (days/year)
$10^{-6}=$ Conversion factor
Values

|  | Infant/Child |  |  |  | Adult |
| ---: | :---: | :---: | :---: | :---: | :---: |
| Age --> | 3rd Trimester | $\mathbf{0 - 2}$ | $\mathbf{2 - 9}$ | $\mathbf{2 - 1 6}$ | $\mathbf{1 6 - 3 0}$ |
| Parameter |  |  |  |  |  |
| ASF $=$ | 10 | 10 | 3 | 3 | 1 |
| $\mathrm{CPF}=$ | $1.10 \mathrm{E}+00$ | $1.10 \mathrm{E}+00$ | $1.10 \mathrm{E}+00$ | $1.10 \mathrm{E}+00$ | $1.10 \mathrm{E}+00$ |
| $\mathrm{DBR}^{*}=$ | 361 | 1090 | 631 | 572 | 261 |
| $\mathrm{~A}=$ | 1 | 1 | 1 | 1 | 1 |
| $\mathrm{EF}=$ | 350 | 350 | 350 | 350 | 350 |
| $\mathrm{AT}=$ | 70 | 70 | 70 | 70 | 70 |
| $\mathrm{FAH}=$ | 0.85 | 0.85 | 0.72 | 0.72 | 0.73 |

* 95th percentile breathing rates for infants and 80th percentile for children and adults

Construction Cancer Risk by Year - Maximum Impact Receptor Location

| Exposure Year | Exposure <br> Duration <br> (years) | Age | Infant/Child - Exposure Informatior |  |  | Infant/Child <br> Cancer <br> Risk <br> (per million) | Adult - Exposure Information |  |  | AdultCancerRisk(per million) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Age Sensitivity Factor |  |  | eled | Age Sensitivity Factor |  |
|  |  |  | DPM Conc (ug/m3) |  |  |  | DPM Conc (ug/m3) |  |  |  |
|  |  |  | Year | Annual |  |  | Year | Annual |  |  |
| 0 | 0.25 | -0.25-0* | 2017 | 0.0554 | 10 | 0.64 | 2017 | 0.0554 | - | - |
| 1 | 1 | 0-1 | 2017 | 0.0554 | 10 | 7.73 | 2017 | 0.0554 | 1 | 0.16 |
| 2 | 1 | 1-2 | 2018 | 0.0554 | 10 | 7.73 | 2018 | 0.0554 | 1 | 0.16 |
| 3 | 1 | 2-3 | 2019 | 0.0554 | 3 | 1.03 | 2019 | 0.0554 | 1 | 0.16 |
| 4 | 1 | 3-4 |  | 0.0554 | 3 | 1.03 | 2020 | 0.0554 | 1 | 0.16 |
| 5 | 1 | 4-5 |  | 0.0554 | 3 | 1.03 | 2021 | 0.0554 | 1 | 0.16 |
| 6 | 1 | 5-6 |  | 0.0554 | 3 | 1.03 | 2022 | 0.0554 | 1 | 0.16 |
| 7 | 1 | 6-7 |  | 0.0554 | 3 | 1.03 | 2023 | 0.0554 | 1 | 0.16 |
| 8 | 1 | 7-8 |  | 0.0554 | 3 | 1.03 | 2024 | 0.0554 | 1 | 0.16 |
| 9 | 1 | 8-9 |  | 0.0554 | 3 | 1.03 | 2025 | 0.0554 | 1 | 0.16 |
| 10 | 1 | 9-10 |  | 0.0554 | 3 | 1.03 | 2026 | 0.0554 | 1 | 0.16 |
| 11 | 1 | 10-11 |  | 0.0554 | 3 | 1.03 | 2027 | 0.0554 | 1 | 0.16 |
| 12 | 1 | 11-12 |  | 0.0554 | 3 | 1.03 | 2028 | 0.0554 | 1 | 0.16 |
| 13 | 1 | 12-13 |  | 0.0554 | 3 | 1.03 | 2029 | 0.0554 | 1 | 0.16 |
| 14 | 1 | 13-14 |  | 0.0554 | 3 | 1.03 | 2030 | 0.0554 | 1 | 0.16 |
| 15 | 1 | 14-15 |  | 0.0554 | 3 | 1.03 | 2031 | 0.0554 | 1 | 0.16 |
| 16 | 1 | 15-16 |  | 0.0554 | 3 | 1.03 | 2032 | 0.0554 | 1 | 0.16 |
| 17 | 1 | 16-17 |  | 0.0554 | 1 | 0.16 | 2033 | 0.0554 | 1 | 0.16 |
| 18 | 1 | 17-18 |  | 0.0554 | 1 | 0.16 | 2034 | 0.0554 | 1 | 0.16 |
| 19 | 1 | 18-19 |  | 0.0554 | 1 | 0.16 | 2035 | 0.0554 | 1 | 0.16 |
| 20 | 1 | 19-20 |  | 0.0554 | 1 | 0.16 | 2036 | 0.0554 | 1 | 0.16 |
| 21 | 1 | 20-21 |  | 0.0554 | 1 | 0.16 | 2037 | 0.0554 | 1 | 0.16 |
| 22 | 1 | 21-22 |  | 0.0554 | 1 | 0.16 | 2038 | 0.0554 | 1 | 0.16 |
| 23 | 1 | 22-23 |  | 0.0554 | 1 | 0.16 | 2039 | 0.0554 | 1 | 0.16 |
| 24 | 1 | 23-24 |  | 0.0554 | 1 | 0.16 | 2040 | 0.0554 | 1 | 0.16 |
| 25 | 1 | 24-25 |  | 0.0554 | 1 | 0.16 | 2041 | 0.0554 | 1 | 0.16 |
| 26 | 1 | 25-26 |  | 0.0554 | 1 | 0.16 | 2042 | 0.0554 | 1 | 0.16 |
| 27 | 1 | 26-27 |  | 0.0554 | 1 | 0.16 | 2043 | 0.0554 | 1 | 0.16 |
| 28 | 1 | 27-28 |  | 0.0554 | 1 | 0.16 | 2044 | 0.0554 | 1 | 0.16 |
| 29 | 1 | 28-29 |  | 0.0554 | 1 | 0.16 | 2045 | 0.0554 | 1 | 0.16 |
| 30 | 1 | 29-30 |  | 0.0554 | 1 | 0.16 | 2046 | 0.0554 | 1 | 0.16 |
| Total Increased Cancer Risk |  |  |  |  |  | 32.75 |  |  |  | 4.77 |


| Fugitive | Total |
| :---: | :---: |
| PM2.5 | PM2.5 |
|  |  |
| 0.4842 | 0.540 |

[^5]Ghilotti Yard - Santa Rosa, CA
DPM Emissions and Modeling Emission Rates

| Emissions <br> Model <br> Year | Activity | $\begin{gathered} \text { DPM } \\ \text { (ton/year) } \end{gathered}$ | Area <br> Source | DPM Emissions |  |  | Modeled <br> Area $\left(\mathrm{m}^{2}\right)$ | DPMEmissionRate$\left(\mathrm{g} / \mathrm{s} / \mathrm{m}^{2}\right)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | (lb/yr) | (lb/hr) | (g/s) |  |  |
| 2017 | Equipment \& Truck: | 0.0228 | DPM_SYAR | 45.6 | 0.01136 | $1.43 \mathrm{E}-03$ | 9,942 | $1.44 \mathrm{E}-07$ |
| Total |  | 0.0228 |  | 45.6 | 0.0114 | 0.0014 |  |  |
| Operation Hours |  |  |  |  |  |  |  |  |
|  |  | hr/day = days/yr = ours/year = | $11$ <br> 365 <br> 4015 | (6am-5 |  |  |  |  |

Ghilotti Yard - Santa Rosa, CA - Health Impact Summary
Maximum Impacts at Ghilotti Facility MEI Location

| Emissions <br> Year | Maximum Concentrations |  | Cancer Risk (per million) |  | Hazard Index <br> (-) | Maximum Annual PM2.5 Concentration $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Exhaust PM10/DPM <br> $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ | Fugitive <br> PM2.5 $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ |  |  |  |  |
|  |  |  | Child | Adult |  |  |
| 2017 | 0.0009 | 0.0000 | 0.5 | 0.1 | 0.000 | 0.00 |

Ghilotti Yard - Santa Rosa, CA - On-Site Equipment \& Truck Operation Impacts
Maximum DPM Cancer Risk Calculations From Construction
Impacts at Ghilotti Facility MEI Location
Cancer Risk (per million) = CPF x Inhalation Dose x ASF x ED/AT x FAH x 1.0E6
Where: CPF = Cancer potency factor ( $\mathrm{mg} / \mathrm{kg}$-day $)^{-1}$
ASF = Age sensitivity factor for specified age group
ED = Exposure duration (years)
$\mathrm{AT}=$ Averaging time for lifetime cancer risk (years)
FAH $=$ Fraction of time spent at home (unitless)
Inhalation Dose $=\mathrm{C}_{\text {air }} \times$ DBR $\times \mathrm{A} \times(\mathrm{EF} / 365) \times 10^{-6}$
Where: $\mathrm{C}_{\text {air }}=$ concentration in air $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$
DBR = daily breathing rate (L/kg body weight-day)
A = Inhalation absorption factor
$\mathrm{EF}=$ Exposure frequency (days/year)
$10^{-6}=$ Conversion factor
Values

|  | Infant/Child |  |  |  | Adult |
| ---: | :---: | :---: | :---: | :---: | :---: |
| Age --> | 3rd Trimester | $\mathbf{0 - 2}$ | $\mathbf{2 - 9}$ | $\mathbf{2 - 1 6}$ | $\mathbf{1 6 - 3 0}$ |
| Parameter |  |  |  |  |  |
| ASF $=$ | 10 | 10 | 3 | 3 | 1 |
| $\mathrm{CPF}=$ | $1.10 \mathrm{E}+00$ | $1.10 \mathrm{E}+00$ | $1.10 \mathrm{E}+00$ | $1.10 \mathrm{E}+00$ | $1.10 \mathrm{E}+00$ |
| $\mathrm{DBR}^{*}=$ | 361 | 1090 | 631 | 572 | 261 |
| $\mathrm{~A}=$ | 1 | 1 | 1 | 1 | 1 |
| $\mathrm{EF}=$ | 350 | 350 | 350 | 350 | 350 |
| $\mathrm{AT}=$ | 70 | 70 | 70 | 70 | 70 |
| $\mathrm{FAH}=$ | 0.85 | 0.85 | 0.72 | 0.72 | 0.73 |

* 95th percentile breathing rates for infants and 80th percentile for children and adults

Construction Cancer Risk by Year - Maximum Impact Receptor Location

| Exposure <br> Year | Exposure <br> Duration <br> (years) | Age | Infant/Child - Exposure Informatior |  |  | Infant/ChildCancerRisk(per million) | Adult - Exposure Information |  |  | AdultCancerRisk(per million) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | DPM Conc (ug/m3) |  | Age Sensitivity Factor |  |  | eled | Age Sensitivity Factor |  |
|  |  |  |  |  | DPM Conc (ug/m3) |  |  |  |
|  |  |  | Year | Annual |  |  | Year | Annual |  |  |
| 0 | 0.25 | -0.25-0* | 2017 | 0.0009 |  | 10 | 0.01 | 2017 | 0.0009 | - | - |
| 1 | 1 | 0-1 | 2017 | 0.0009 | 10 | 0.12 | 2017 | 0.0009 | 1 | 0.00 |
| 2 | 1 | 1-2 | 2018 | 0.0009 | 10 | 0.12 | 2018 | 0.0009 | 1 | 0.00 |
| 3 | 1 | 2-3 | 2019 | 0.0009 | 3 | 0.02 | 2019 | 0.0009 | 1 | 0.00 |
| 4 | 1 | 3-4 |  | 0.0009 | 3 | 0.02 | 2020 | 0.0009 | 1 | 0.00 |
| 5 | 1 | 4-5 |  | 0.0009 | 3 | 0.02 | 2021 | 0.0009 | 1 | 0.00 |
| 6 | 1 | 5-6 |  | 0.0009 | 3 | 0.02 | 2022 | 0.0009 | 1 | 0.00 |
| 7 | 1 | 6-7 |  | 0.0009 | 3 | 0.02 | 2023 | 0.0009 | 1 | 0.00 |
| 8 | 1 | 7-8 |  | 0.0009 | 3 | 0.02 | 2024 | 0.0009 | 1 | 0.00 |
| 9 | 1 | 8-9 |  | 0.0009 | 3 | 0.02 | 2025 | 0.0009 | 1 | 0.00 |
| 10 | 1 | 9-10 |  | 0.0009 | 3 | 0.02 | 2026 | 0.0009 | 1 | 0.00 |
| 11 | 1 | 10-11 |  | 0.0009 | 3 | 0.02 | 2027 | 0.0009 | 1 | 0.00 |
| 12 | 1 | 11-12 |  | 0.0009 | 3 | 0.02 | 2028 | 0.0009 | 1 | 0.00 |
| 13 | 1 | 12-13 |  | 0.0009 | 3 | 0.02 | 2029 | 0.0009 | 1 | 0.00 |
| 14 | 1 | 13-14 |  | 0.0009 | 3 | 0.02 | 2030 | 0.0009 | 1 | 0.00 |
| 15 | 1 | 14-15 |  | 0.0009 | 3 | 0.02 | 2031 | 0.0009 | 1 | 0.00 |
| 16 | 1 | 15-16 |  | 0.0009 | 3 | 0.02 | 2032 | 0.0009 | 1 | 0.00 |
| 17 | 1 | 16-17 |  | 0.0009 | 1 | 0.00 | 2033 | 0.0009 | 1 | 0.00 |
| 18 | 1 | 17-18 |  | 0.0009 | 1 | 0.00 | 2034 | 0.0009 | 1 | 0.00 |
| 19 | 1 | 18-19 |  | 0.0009 | 1 | 0.00 | 2035 | 0.0009 | 1 | 0.00 |
| 20 | 1 | 19-20 |  | 0.0009 | 1 | 0.00 | 2036 | 0.0009 | 1 | 0.00 |
| 21 | 1 | 20-21 |  | 0.0009 | 1 | 0.00 | 2037 | 0.0009 | 1 | 0.00 |
| 22 | 1 | 21-22 |  | 0.0009 | 1 | 0.00 | 2038 | 0.0009 | 1 | 0.00 |
| 23 | 1 | 22-23 |  | 0.0009 | 1 | 0.00 | 2039 | 0.0009 | 1 | 0.00 |
| 24 | 1 | 23-24 |  | 0.0009 | 1 | 0.00 | 2040 | 0.0009 | 1 | 0.00 |
| 25 | 1 | 24-25 |  | 0.0009 | 1 | 0.00 | 2041 | 0.0009 | 1 | 0.00 |
| 26 | 1 | 25-26 |  | 0.0009 | 1 | 0.00 | 2042 | 0.0009 | 1 | 0.00 |
| 27 | 1 | 26-27 |  | 0.0009 | 1 | 0.00 | 2043 | 0.0009 | 1 | 0.00 |
| 28 | 1 | 27-28 |  | 0.0009 | 1 | 0.00 | 2044 | 0.0009 | 1 | 0.00 |
| 29 | 1 | 28-29 |  | 0.0009 | 1 | 0.00 | 2045 | 0.0009 | , | 0.00 |
| 30 | 1 | 29-30 |  | 0.0009 | 1 | 0.00 | 2046 | 0.0009 | 1 | 0.00 |
| Total Increased Cancer Risk |  |  |  |  |  | 0.52 |  |  |  | 0.08 |


| Fugitive | Total |
| :---: | :---: |
| PM2.5 | PM2.5 |
|  |  |
| 0.0000 | 0.001 |

[^6]
## ( w -Trans

## Final Traffic Impact Study for the Ghilotti Construction Yard



Prepared for the County of Sonoma

Submitted by
W-Trans

March 7, 2018

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## Executive Summary

The proposed project would update the Ghilotti Construction Use Permit to reflect existing non-compliant uses. It is understood the property is zoned M3 (Limited Rural Industrial), and is currently being used to temporarily store contractor's equipment, stockpile rock rip-rap material, and process broken asphalt and concrete for recycling and reuse. The project is expected to generate a maximum of 50 new truck trips per day including a maximum of 30 trips during either the a.m. or p.m. peak hour.

The study area includes the intersections of Todd Road with Standish Avenue-Ghilotti Avenue, Moorland Avenue, US 101 North and South ramps, and Santa Rosa Avenue. Analysis indicates that the study intersections are operating acceptably under Existing Conditions except for Todd Road/Standish Avenue-Ghilotti Avenue, which operates unacceptably at LOS E during the p.m. peak hour. Existing p.m. peak hour volumes meet warrants for a traffic signal.

Upon the addition of project-generated traffic to Existing volumes, the study intersections are expected to continue operating acceptably during the a.m. peak hour, but Todd Road/Standish Avenue-Ghilotti Avenue is expected to deteriorate to LOS F during the p.m. peak hour with an increase in average delay that exceeds the five seconds allowed under County Standards.

Under Baseline Conditions, all study intersections would operate acceptably with or without project-related trips except for Todd Road/Standish Avenue-Ghilotti Avenue, which would be expected to deteriorate to LOS F with an increase in delay that exceeds five seconds upon the addition of project-related traffic. Under the anticipated Future volumes, the intersections of Todd Road with the US 101 North and South ramps and Todd Road/Moorland Avenue are expected to continue operating acceptably overall during both peak hours; Todd Road/Standish Avenue-Ghilotti Avenue and Todd Road/Santa Rosa Avenue are expected to operate unacceptably at LOS F during both peak hours. The intersections would continue operating at the same levels of service with the addition of project-related traffic. Although Todd Road/Santa Rosa Avenue is projected to deteriorate to LOS F, the project would add less than five seconds of delay so the impact would be considered less-than-significant per County standards.

Upon installation of a traffic signal and southbound left-turn lane at Todd Road/Standish Avenue-Ghilotti Avenue, the intersection would operate acceptably during both peak hours and for all evaluated scenarios; the project applicant should pay a proportional share fee of 11.1 percent toward these improvements.

The project would not cause any queues to exceed available storage that would not be expected to do so otherwise.

Pedestrian and transit facilities are adequate to serve the project site given the site location and anticipated demand and bicycle facilities would be adequate upon completion of the planned Class II bike lanes on Todd Road. Because the project site shares frontage with Todd Road, the applicant should make an in-lieu payment toward the cost of the future striping project, as opposed to striping an isolated short bike lane segment at this time.

Sight distances along Todd Road at Ghilotti Avenue are adequate for the measured approach speeds and the posted speed limit; however the bushes/trees along the roadway frontage west of Ghilotti Avenue should be trimmed regularly to maintain adequate sight lines.

## Introduction

This report presents an analysis of the potential traffic impacts that would be associated with development of a construction yard at 304 Todd Road in the County of Sonoma. The traffic study was completed in accordance with the criteria established by the County of Sonoma, and is consistent with standard traffic engineering techniques. The scope of work and methodology reflect direction obtained from County staff.

## Prelude

The purpose of a traffic impact study is to provide County staff and policy makers with data that they can use to make an informed decision regarding the potential traffic impacts of a proposed project, and any associated improvements that would be required to mitigate these impacts to a level of insignificance as defined by the County's General Plan or other policies. Vehicular traffic impacts are typically evaluated by determining the number of new trips that the proposed use would be expected to generate, distributing these trips to the surrounding street system based on existing travel patterns or anticipated travel patterns specific to the proposed project, then analyzing the impact the new traffic would be expected to have on critical intersections or roadway segments. Impacts relative to access for pedestrians, bicyclists, and to transit are also addressed.

## Project Profile

The proposed project is a modification of the Ghilotti Construction Use Permit to reflect existing non-compliant uses pursuant to the Notice of Violation received from the County dated August 9, 2011. The property is zoned M3 (Limited Rural Industrial), and is currently being used to temporarily store contractor's equipment, stockpile rock rip-rap material, and process broken asphalt and concrete for recycling and reuse. The requested permit would bring the most recent previous use into compliance.

The project site is located at 304 Todd Road in the County of Sonoma, as shown in Figure 1.


## Transportation Setting

## Operational Analysis

## Study Area and Periods

The study area selected with input from County staff consists of the section of Todd Road fronting the project and the project access point as well as the following intersections.

1. Todd Road/Standish Avenue-Ghilotti Avenue
2. Todd Road/Moorland Avenue
3. Todd Road/US 101 South Ramps
4. Todd Road/US 101 North Ramps
5. Todd Road/Santa Rosa Avenue

Operating conditions during the weekday a.m. and p.m. peak periods were evaluated to capture the highest potential impacts for the proposed project as well as the highest volumes on the local transportation network. The morning peak hour occurs between 7:00 and 9:00 a.m. and reflects conditions during the home to work or school commute, while the p.m. peak hour occurs between 4:00 and 6:00 p.m. and typically reflects the highest level of congestion during the homeward bound commute. At the study intersections, the a.m. peak hour generally occurred between 7:30 and 8:30 a.m. and the p.m. peak hour occurred between 4:15 and 5:15 p.m.

## Study Intersections

Todd Road/Standish Avenue-Ghilotti Avenue is an unsignalized four-way intersection stop-controlled on the Standish Avenue and Ghilotti Avenue approaches, which are offset by approximately 40 feet. Left-turn lanes are present on the eastbound and westbound Todd Road approaches.

Todd Road/Moorland Avenue is an unsignalized tee intersection, stop-controlled on the southbound Moorland Avenue approach. There is a left-turn lane provided on the eastbound approach and a two-way left-turn lane on the westbound approach between Moorland Avenue and South Moorland Avenue. Additionally, there is a private driveway that intersects Todd Road from the south.

Todd Road/US 101 South Ramps is a signalized tee intersection with left-turn pockets and protected left-turn phasing on the northbound and westbound approaches. A marked crosswalk is present on the west leg.

Todd Road/US 101 North Ramps is a signalized tee intersection with left-turn pockets and protected left-turn phasing on the northbound and westbound approaches. Additionally, a left-turn lane on the eastbound approach provides access to the service station located northwest of the intersection.

Todd Road/Santa Rosa Avenue is a signalized intersection with left-turn pockets provided on all four approaches and protected left-turn phasing on the northbound and southbound approaches; the eastbound and westbound approaches have split phasing. The northbound, southbound, and eastbound approaches have dedicated rightturn lanes, and marked crosswalks are provided on the south, east, and west legs.

The locations of the study intersections and the existing lane configurations and controls are shown in Figure 1.

## Study Roadway

Todd Road in the project vicinity is a two-lane county road running east-west; it is discontinuous at US 101, and east of Santa Rosa Avenue the roadway is known as East Todd Road. Within the project vicinity, the street ranges from 20 feet wide to 68 feet wide depending on the presence of turn lanes, width of the travel lanes, and width of the shoulders. Adjacent to the project site the posted speed limit is 35 miles per hour ( mph ). Vehicles are the primary mode of travel in the surrounding network as there are no bicycle lanes present and pedestrian facilities are limited.

## Collision History

The collision history for the study area was reviewed to determine any trends or patterns that may indicate a safety issue. Collision rates were calculated based on records available from the California Highway Patrol as published in their Statewide Integrated Traffic Records System (SWITRS) reports. The most current five-year period available is January 1, 2012 through December 31, 2016.

As presented in Table 1, the calculated collision rates for the study intersections were compared to average collision rates for similar facilities statewide, as indicated in 2013 Collision Data on California State Highways, California Department of Transportation (Caltrans). The signalized intersections have collision rates comparable to statewide averages indicating that the intersections are operating as expected with regards to safety, though it is noted that Todd Road/Santa Rosa Avenue had a collision rate slightly higher than the statewide average and both of the unsignalized intersections have collision rates higher than the statewide averages which warranted further analysis.

| Table 1 - Collision Rates at the Study Intersections |  |  |  |
| :--- | :---: | :---: | :---: |
| Study Intersection | Number of <br> Collisions <br> (2012-2016) | Calculated <br> Collision Rate <br> (c/mve) | Statewide Average <br> Collision Rate <br> (c/mve) |
| 1. Todd Rd/Standish Ave-Ghilotti Ave | 10 | $\mathbf{0 . 4 6}$ | 0.26 |
| 2. $\quad$ Todd Rd/Moorland Ave | 17 | $\mathbf{0 . 6 4}$ | 0.14 |
| 2. $\quad$ Todd Rd/US 101 South Ramps | 12 | 0.37 | 0.43 |
| 2. Todd Rd/US 101 North Ramps | 8 | 0.25 | 0.27 |
| 3. $\quad$ Todd Rd/Santa Rosa Ave | 27 | $\mathbf{0 . 4 9}$ | 0.43 |

Note: $\quad c / m v e=$ collisions per million vehicles entering; Bold $=$ above-average collision rate

Further review of the individual collisions that occurred at Todd Road/Standish Avenue-Ghilotti Avenue revealed that of the ten total collisions, seven were either a broadside or sideswipe. Similarly, over half of the collisions at Todd Road/Moorland Avenue were either a broadside or sideswipe. Signalization of the intersections could help to reduce the frequency of these types of collisions. The collision rate at Santa Rosa Avenue/Todd Road is higher than the statewide average largely due to the proximity of the gas stations on the northwest and southwest corners. Both of the gas stations have driveways within 90 feet of the intersection that create additional conflict zones. Consolidation of the driveways or restricting access to right-in right-out movements only could help to reduce the incidence of collisions. The collision rate calculations for the study intersections are provided in Appendix A.

## Alternative Modes

## Pedestrian Facilities

Pedestrian facilities include sidewalks, crosswalks, pedestrian signal phases, curb ramps, curb extensions, and various streetscape amenities such as lighting, benches, etc. As might be expected given the rural location of the project site, a connected pedestrian network is lacking.

## Bicycle Facilities

The Highway Design Manual, Caltrans, 2012, classifies bikeways into three categories:

- Class I Multi-Use Path - a completely separated right-of-way for the exclusive use of bicycles and pedestrians with cross flows of motorized traffic minimized.
- Class II Bike Lane - a striped and signed lane for one-way bike travel on a street or highway.
- Class III Bike Route - signing only for shared use with motor vehicles within the same travel lane on a street or highway.

Although there are no existing bicycle facilities in the project area, there are plans to construct Class II bike lanes on Todd Road between Llano Road and Santa Rosa Avenue and on Standish Avenue. Additionally, the Sonoma Marin Area Rail Transit (SMART) Pathway is located approximately 600 feet east of the project site and would provide access to a Class I regional trail. Table 2 summarizes the planned bicycle facilities in the project vicinity, as contained in the 2010 Santa Rosa Bicycle and Pedestrian Master Plan, and the existing and planned alternative modes in the project vicinity are shown in Figure 2

## Table 2 - Planned Bicycle Facilities

| Facility | Class | Length <br> (miles) | Begin Point | End Point |
| :--- | :---: | :---: | :---: | :---: |
| SMART Pathway | I | Regional |  |  |
| Standish Ave | II | 0.5 | Todd Rd | W Robles Ave |
| Todd Rd | II | 2.8 | Llano Rd | Santa Rosa Ave |

Source: 2010 Santa Rosa Bicycle and Pedestrian Master Plan

## Transit Facilities

Sonoma County Transit (SCT) provides fixed route bus service in Sonoma County. SCT Route 42 serves the bus stops on Todd Road adjacent to the project site and provides weekday commute service between the industrial area in which the project is located and the Santa Rosa Transit Mall.

Two bicycles can be carried on most SCT buses. Bike rack space is on a first come, first served basis. Additional bicycles are allowed on SCT buses at the discretion of the driver.

Dial-a-ride, also known as paratransit, or door-to-door service, is available for those who are unable to independently use the transit system due to a physical or mental disability. Volunteer Wheels, the ADA paratransit operator for Sonoma County Transit, is designed to serve the needs of individuals with disabilities within the incorporated areas of Sonoma County, the Greater Santa Rosa Area, and between the County's nine incorporated cities.


## Capacity Analysis

## Intersection Level of Service Methodologies

Level of Service (LOS) is used to rank traffic operation on various types of facilities based on traffic volumes and roadway capacity using a series of letter designations ranging from A to F. Generally, Level of Service A represents free flow conditions and Level of Service F represents forced flow or breakdown conditions. A unit of measure that indicates a level of delay generally accompanies the LOS designation.

The study intersections were analyzed using methodologies published in the Highway Capacity Manual (HCM), Transportation Research Board, 2010. This source contains methodologies for various types of intersection control, all of which are related to a measurement of delay in average number of seconds per vehicle.

The Levels of Service for the intersections of Todd Road with Standish Avenue-Ghilotti Avenue and Moorland Avenue, which have side-street stop controls, were analyzed using the "Two-Way Stop-Controlled" intersection capacity method from the HCM. This methodology determines a level of service for each minor turning movement by estimating the level of average delay in seconds per vehicle. Results are presented for individual movements together with the weighted overall average delay for the intersection.

The study intersections that are controlled by a traffic signal, or may be in the future, were evaluated using the signalized methodology from the HCM. This methodology is based on factors including traffic volumes, green time for each movement, phasing, whether or not the signals are coordinated, truck traffic, and pedestrian activity. Average stopped delay per vehicle in seconds is used as the basis for evaluation in this LOS methodology. Delays were calculated using signal timing provided by County and Caltrans staff, though for the Future conditions scenarios delays were calculated using optimized signal timing.

The Vistro software was used to analyze the intersections of Todd Road with Standish Avenue-Ghilotti Avenue and Moorland Avenue. The signalized intersections included in the study area were analyzed using microsimulation and the SimTraffic software to account for the proximity of the intersections. The average delays for ten microsimulation runs were calculated to determine the resulting Levels of Service for each scenario.

The ranges of delay associated with the various levels of service are indicated in Table 3.

## Table 3 - Intersection Level of Service Criteria

| LOS | Two-Way Stop-Controlled | Signalized |
| :---: | :--- | :--- |
| A | Delay of 0 to 10 seconds. Gaps in traffic are readily <br> available for drivers exiting the minor street. | Delay of 0 to 10 seconds. Most vehicles arrive <br> during the green phase, so do not stop at all. |
| B | Delay of 10 to 15 seconds. Gaps in traffic are <br> somewhat less readily available than with LOS A, but <br> no queuing occurs on the minor street. | Delay of 10 to 20 seconds. More vehicles stop than <br> with LOS A, but many drivers still do not have to <br> stop. |
| C | Delay of 15 to 25 seconds. Acceptable gaps in traffic <br> are less frequent, and drivers may approach while <br> another vehicle is already waiting to exit the side <br> street. | Delay of 20 to 35 seconds. The number of vehicles <br> stopping is significant, although many still pass <br> through without stopping. |
| D | Delay of 25 to 35 seconds. There are fewer acceptable <br> gaps in traffic, and drivers may enter a queue of one or <br> two vehicles on the side street. | Delay of 35 to 55 seconds. The influence of <br> congestion is noticeable, and most vehicles have to <br> stop. |
| E | Delay of 35 to 50 seconds. Few acceptable gaps in <br> traffic are available, and longer queues may form on <br> the side street. | Delay of 55 to 80 seconds. Most, if not all, vehicles <br> must stop and drivers consider the delay excessive. |
| F | Delay of more than 50 seconds. Drivers may wait for <br> long periods before there is an acceptable gap in <br> traffic for exiting the side streets, creating long queues. | Delay of more than 80 seconds. Vehicles may wait <br> through more than one cycle to clear the <br> intersection. |

Reference: Highway Capacity Manual, Transportation Research Board, 2000

## Traffic Operation Standards

Based on the most recent criteria published by the County of Sonoma, the project would have a significant traffic impact if it results in any of the following conditions.

1. On-site roads and frontage improvements - Proposed on-site circulation and street frontage would not meet the County's minimum standards for roadway or driveway design, or potentially result in safety hazards, as determined by the County in consultation with a registered traffic engineer.
2. Parking - Proposed on-site parking supply would not be adequate to accommodate parking demand.
3. Emergency Access - The project site would have inadequate emergency access.
4. Alternative Transportation - The project provides inadequate facilities for alternative transportation modes (e.g., bus turnouts, bicycle racks, pedestrian pathways) and/or the project creates potential conflicts with adopted policies, plans, or programs supporting alternative transportation.
5. Road Hazards - Hazards are increased due to a design feature (e.g., sharp curves or dangerous intersections) or incompatible uses (e.g., farm equipment, heavy pedestrian or truck traffic).
6. Vehicle Queues - The addition of project traffic causes the $95^{\text {th }}$ percentile queue length to exceed roadway turn lane storage capacity.
7. Signal Warrants - The addition of the project's vehicle or pedestrian traffic causes an intersection to meet or exceed Caltrans signal warrant criteria.
8. Turn Lanes - The addition of project traffic causes an intersection to meet or exceed criteria for provision of a right or left turn lane on an intersection approach.
9. Sight Lines - The project constructs an unsignalized intersection (including driveways) or adds traffic to an existing unsignalized intersection approach that does not have adequate sight lines based upon Caltrans criteria for state highway intersections and County criteria for County roadway intersections.
10. Intersections - The County Level of Service standard for intersections is Level of Service D. The project would have a significant traffic impact if the project's traffic would cause an intersection currently operating at an acceptable level of service (LOS D or better) to operate below the standard (LOS E or F).

If the intersection currently operates or is projected to operate below the County standard (at LOS E or F), the project's impact is significant and cumulatively considerable if it causes the delay for any critical movement to increase by five seconds or more. The delay will be determined by comparing intersection operation with and without the project's traffic for both the existing near-term and projected future conditions. These criteria apply to all controlled or uncontrolled intersections with projected traffic volumes over 30 vehicles per hour per approach or per exclusive left turn movement.
11. Roadway Operation - The Level of Service Standard for County roadway operations is to maintain a Level of Service C per Policy CT-3.1.

## Caltrans

In the Guide for the Preparation of Traffic Impact Studies, Caltrans indicates that they endeavor to maintain operation at the transition from LOS C to LOS D. The Caltrans criteria was applied to the intersections of Todd Road with the US 101 North and South ramps.

## Existing Conditions

Standard traffic engineering practice for conducting traffic studies includes the assessment of existing conditions and the evaluation of conditions that would be associated with the operation or occupation of a proposed project. For the purposes of analyzing traffic impacts associated with updating a Use Permit to reflect existing activity, traffic anticipated to be generated by the proposed uses were deducted from the volumes collected in October 2016 and May 2017 to document "Existing Conditions," or those without the construction yard.

Under Existing Conditions the study intersections operate acceptably at LOS B or better overall during the a.m. peak hour; however, Todd Road/Standish Avenue-Ghilotti Avenue operates unacceptably at LOS E overall during the p.m. peak hour and the southbound Standish Avenue approach operates at LOS F during both peaks. It is noted the southbound approach at Todd Road/Moorland Avenue operates at LOS E and F during the morning and evening peak hours, respectively; however, the intersection operates at LOS A overall during both peak hours.

The Existing traffic volumes are shown in Figure 3. A summary of the intersection level of service calculations is contained in Table 4, and copies of the Level of Service calculations for all evaluated scenarios for the unsignalized intersections are provided in Appendix B; Level of Service calculations for the signalized intersections are provided in Appendix C. It should be noted that because microsimulation was used to evaluate the signalized intersections the calculated delay can vary between runs, and while results were reported based on the average of ten runs in an attempt to converge on a single value, it is important to view the results with an understanding that there is a certain amount of fluctuation involved.

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Table 4 - Existing Peak Hour Intersection Levels of Service

| Study Intersection Approach | AM Peak |  | PM Peak |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Delay | LOS | Delay | LOS |
| 1. Todd Rd/Standish Ave-Ghilotti Ave | 10.3 | B | 38.4 | E |
| Northbound (Ghilotti Ave) Approach | 13.6 | $B$ | 12.7 | $B$ |
| Southbound (Standish Ave) Approach | 52.1 | $F$ | ** | $F$ |
| Install signal and restripe to add SB left-turn lane | 16.9 | B | 18.2 | B |
| 2. Todd Rd/Moorland Ave | 5.4 | A | 9.6 | A |
| Southbound (Moorland Ave) Approach | 44.3 | $E$ | 78.2 | $F$ |
| 3. Todd Rd/US 101 South Ramps | 17.8 | B | 22.7 | C |
| 4. Todd Rd/US 101 North Ramps | 7.4 | A | 6.3 | A |
| 5. Todd Rd/Santa Rosa Ave | 10.9 | B | 18.6 | B |

Notes: Delay is measured in average seconds per vehicle; LOS = Level of Service; Results for minor approaches to two-way stop-controlled intersections are indicated in italics; ${ }^{* *}=$ delay greater than 120 seconds; Bold text $=$ deficient operation; Shaded cells = conditions with recommended improvements

Due to high delay calculated at Todd Road/Standish Avenue-Ghilotti Avenue during the p.m. peak hour, a signal warrant analysis was performed to determine potential need for a traffic signal. Chapter 4C of the California Manual on Uniform Traffic Control Devices (CA-MUTCD) provides guidance on when a traffic signal should be considered based on nine different warrants, or criteria. For the purposes of this study, Warrant 3, the Peak Hour volume warrant, which determines the need for traffic control based on the highest volume hour of the day, was used as an initial indication of traffic control needs. The use of this signal warrant is common practice for planning studies.

Existing volumes at Todd Toad/Standish Avenue-Ghilotti Avenue are sufficient to meet the criteria established by Warrant 3, and for this reason, it is recommended that the County consider installing a traffic signal at the intersection and restriping the Standish Avenue approach to provide a southbound left-turn lane in order to reduce delay during the p.m. peak hour. Upon completion of these improvements, the intersection would be expected to operate acceptably during both peak hours, as shown in Table 4. Further, a signal would address the pattern of crashes that resulted in an above-average collision rate at this location. The delays upon installation of a traffic signal were calculated assuming split phasing as the north and south legs are offset and optimized signal timing. A copy of the signal warrant analysis spreadsheet is included in Appendix D.

## Baseline Conditions

Baseline operating conditions were assessed to reflect the addition of traffic associated with projects that are approved in the study area and would potentially be operational within the near-term. County Staff identified the following project to be included in this scenario.

- Shamrock Materials - An approved materials processing plant that would be accessed via Ghilotti Avenue and located just south of the Ghilotti Construction offices. The project would include a concrete batching facility, recycling operation, composting facility, sand and gravel processing plant, maintenance shop, and associated offices. As contained in the Shamrock Materials Traffic Impact Study Updated Report, prepared by W-Trans, the project would be expected to generate 231 new trips per day, including 16 trips during the morning peak hour and 10 during the evening peak hour. The same trip distribution assumptions used in the traffic study for the project were used in this analysis, including 45 percent to/from both US 101 North and South and five percent via Todd Road to both the east and west.


## Intersection Levels of Service

The anticipated traffic associated with the Shamrock project was added to the volumes analyzed in the Existing Conditions scenario in order to determine Baseline volumes. Under these conditions, the study intersections are projected to continue operating at the same levels of service as Existing Conditions. These results are summarized in Table 5 and Baseline volumes are shown in Figure 4.

Table 5 - Baseline Peak Hour Intersection Levels of Service

| Study Intersection Approach | AM Peak |  | PM Peak |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Delay | LOS | Delay | LOS |
| 1. Todd Rd/Standish Ave-Ghilotti Ave | 11.5 | B | 42.0 | E |
| Northbound (Ghilotti Ave) Approach | 13.2 | $B$ | 12.4 | B |
| Southbound (Standish Ave) Approach | 59.0 | $F$ | ** | $F$ |
| Install signal and restripe to add SB left-turn lane | 17.5 | B | 18.6 | B |
| 2. Todd Rd/Moorland Ave | 5.6 | A | 9.9 | A |
| Southbound (Moorland Ave) Approach | 46.4 | E | 81.4 | F |
| 3. Todd Rd/US 101 South Ramps | 16.9 | B | 17.9 | B |
| 4. Todd Rd/US 101 North Ramps | 7.1 | A | 7.2 | A |
| 5. Todd Rd/Santa Rosa Ave | 10.9 | B | 19.8 | B |

Notes: Delay is measured in average seconds per vehicle; LOS = Level of Service; Results for minor approaches to two-way stop-controlled intersections are indicated in italics; ${ }^{* *}=$ delay greater than 120 seconds; Bold text $=$ deficient operation; Shaded cells = conditions with recommended improvements

## Future Conditions

Segment volumes for the horizon year of 2040 were obtained from the County's gravity demand model maintained by the Sonoma County Transportation Authority (SCTA) and translated to peak hour turning movement volumes at the study intersections using the "Furness" method. The Furness method is an iterative process that employs existing turn movement data, existing link volumes, and future link volumes to project likely future turning movement volumes at intersections.

Under the anticipated Future volumes, the intersections are expected to operate at LOS A or B overall during both peak hours, except that Todd Road/Standish Avenue-Ghilotti Avenue and Todd Road/Santa Rosa Avenue are expected to deteriorate to LOS F during both peak hours. It is noted that the LOS at Todd Road/Moorland Avenue is expected to improve during the a.m. peak hour under Future conditions as the model is projecting fewer southbound volumes in 2040; this is likely attributable to the anticipated overcrossing at Bellevue Avenue to the north. Future volumes are shown in Figure 5 and operating conditions are summarized in Table 6.





Table 6 - Future Peak Hour Intersection Levels of Service

| Study Intersection <br> Approach | AM Peak |  | PM Peak |  |  |
| :--- | :--- | :---: | :---: | :---: | :---: |
|  | Todd Rd/Standish Ave-Ghilotti Ave | Delay | LOS | Delay | LOS |
|  | Northbound (Ghilotti Ave) Approach | $* *$ | F | $* *$ | F |
|  | Southbound (Standish Ave) Approach | 18.2 | C | 17.9 | C |
|  | Install signal and restripe to add SB left-turn lane | 30.1 | C | 38.2 | F |
| 2. | Todd Rd/Moorland Ave | 3.8 | A | 14.3 | B |
|  | Southbound (Moorland Ave) Approach | 35.1 | $E$ | 91.4 | F |
| 3. | Todd Rd/US 101 South Ramps | 19.6 | B | 17.5 | B |
| 4. | Todd Rd/US 101 North Ramps | 7.6 | A | 7.4 | A |
| 5. | Todd Rd/Santa Rosa Ave | $\mathbf{6 3 . 8}$ | F | $\mathbf{7 7 . 2}$ | F |
|  | Restripe to provide 2 NB left-turn lanes | 24.1 | C | 40.8 | D |

Notes: Delay is measured in average seconds per vehicle; LOS = Level of Service; Results for minor approaches to two-way stop-controlled intersections are indicated in italics; ** $=$ delay greater than 120 seconds; Bold text = deficient operation; Shaded cells = conditions with recommended improvements; SB = Southbound; NB $=$ Northbound

As might be expected with no changes to the intersection's geometry or controls, the operation of Todd Road/ Standish Avenue-Ghilotti Avenue is anticipated to deteriorate significantly with the increase in traffic projected over the next 24 years. In fact, the delays estimated are well beyond what is reasonable, and indicate that the theoretical results are unreliable. As previously noted, it is recommended that the County install a traffic signal at the intersection and restripe the southbound approach to provide a left-turn lane in order to achieve acceptable levels of service during both peak hours under projected Future volumes.

Additionally, the northbound approach at Todd Road/Santa Rosa Avenue would need to be restriped to provide two left-turn lanes to accommodate the large increase in traffic anticipated for this movement. This improvement could be accomplished by restriping the western through lane into a second left-turn lane and the dedicated right-turn lane into a shared through/right lane. This configuration would result in two left-turn lanes, a single through lane, and a shared through/right lane. A conceptual striping plan for this improvement is contained in Appendix E. It should be noted that this improvement could also necessitate some modification to detection.

## Project Description

The proposed project would update the Ghilotti Construction Use Permit to reflect existing non-compliant uses. It is understood the property is zoned M3 (Limited Rural Industrial), and is currently being used to temporarily store contractor's equipment, stockpile rock rip-rap material, and process broken asphalt and concrete for recycling and reuse. The project site is located at 304 Todd Road and accessed via Ghilotti Avenue; the site plan is shown in Figure 6.

## Trip Generation

The anticipated trip generation potential for the proposed project was estimated using data from the Proposal Statement \& Project Description submitted by Ghilotti Construction to Sonoma County as well as information received directly from Ghilotti Construction. The majority of traffic associated with the proposed project would be due to the import and export of materials which would occur on an as-needed basis varying with the demand imposed by ongoing countywide construction projects.

Most trips would be made by semi-end dump trucks, semi-bottom dump trucks, and transfer trailers; daily traffic is estimated to range between zero and 50 trips per day. Though the actual volume on a typical daily basis is


SITE PLAN

## GHILOTTI PROPERTY

## APN 134-171-050

304 TODD ROAD, SANTA ROSA
ONOMA COUNTY, CALIFORNI
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expected to be substantially lower, to be conservative it was assumed that a maximum of 30 trips would be made during either the a.m. or p.m. peak hour ( 15 trips in and 15 trips out).

Additionally, to account for the fact the trips would be made by large trucks, which have a more significant impact on traffic variables such as headway, speed, density, etc. than standard passenger vehicles, a passenger car equivalent (PCE) factor was used in the analysis. The Highway Capacity Manual (HCM), $6^{\text {th }}$ Edition provides PCE factors based on terrain and recommends using 2.0 for level terrain and 3.0 for rolling terrain. Although the surrounding roadway network is flat, a ratio of three vehicles to one truck was used in the analysis to provide conservative results. After applying the PCE factor, it is estimated the proposed project would result in impacts similar to one that generates 90 passenger car trips during the peak hour, including 45 trips in and 45 trips out. The applied trip generation estimates are shown in Table 7.

Table 7 - Trip Generation Summary

| Land Use | Max Daily |  |  | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Trips | Trips | In | Out | Trips | In | Out |  |  |
| Construction Yard (Trucks) | 50 | 30 | 15 | 15 | 30 | 15 | 15 |  |  |
| Construction Yard (PCE) | 150 | 90 | 45 | 45 | 90 | 45 | 45 |  |  |

Note: $\quad$ PCE = Passenger Car Equivalent

## Trip Distribution

The pattern used to allocate new project trips to the street network was determined based on the likely origins/ destinations for site-generated traffic. Trips would be predominantly to and from construction projects located throughout the county and would occur via US 101. Maximum PCE trips are summarized in Table 8, and the applied distribution assumptions are shown in Figure 7.

Table 8 - Trip Distribution Assumptions

| Route | Percent | Daily Trips | AM Trips | PM Trips |
| :--- | :---: | :---: | :---: | :---: |
| US 101 (North) | $40 \%$ | 60 | 36 | 36 |
| US 101 (South) | $44 \%$ | 66 | 38 | 38 |
| Todd Rd (West of Standish Ave) | $4 \%$ | 6 | 4 | 4 |
| Moorland Ave (North of Todd Rd) | $4 \%$ | 6 | 4 | 4 |
| Santa Rosa Ave (North of Todd Rd) | $4 \%$ | 6 | 4 | 4 |
| Santa Rosa Ave (South of Todd Rd) | $\mathbf{4 \%}$ | 6 | 4 | 4 |
| TOTAL | $\mathbf{1 0 0 \%}$ | $\mathbf{1 5 0}$ | $\mathbf{9 0}$ | $\mathbf{9 0}$ |

Note: Trips do not correspond to exact percentages due to rounding

## Intersection Operation

## Existing plus Project Conditions

Upon the addition of project-related traffic to the Existing volumes, the study intersections are expected to continue operating acceptably during both peak hours, except for Todd Road/Standish Avenue-Ghilotti Avenue which would be expected to further deteriorate from LOS E to LOS F during the p.m. peak hour. The intersection is currently operating unacceptably under Existing Conditions so the project would not cause the intersection to

drop from acceptable operation to unacceptable operation; however, the project would increase the average delay by more than five seconds so the impact would be considered significant under the County's standard. These results are summarized in Table 9 and Existing plus Project traffic volumes are shown in Figure 8.

Table 9 - Existing and Existing plus Project Peak Hour Intersection Levels of Service

| Study Intersection <br> Approach | Existing Conditions |  |  |  | Existing plus Project |  |  |  |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AM Peak | PM Peak | AM Peak |  | PM Peak |  |  |  |
|  | Delay | LOS | Delay | LOS | Delay | LOS | Delay | LOS |  |
| 1. | Todd Rd/Standish Ave-Ghilotti Ave | 10.3 | B | $\mathbf{3 8 . 4}$ | E | 20.6 | C | $\mathbf{7 4 . 8}$ | F |
|  | Northbound (Ghilotti Ave) Approach | 13.6 | B | 12.7 | B | 12.2 | B | 12.5 | B |
|  | Southbound (Standish Ave) Approach | 52.1 | F | $* *$ | F | 114.7 | $F$ | $* *$ | F |
|  | With signal and SB left-turn lane | 16.9 | B | 18.2 | B | 20.0 | B | 21.1 | C |
| 2. | Todd Rd/Moorland Ave | 5.4 | A | 9.6 | A | 6.9 | A | 12.8 | B |
|  | Southbound (Moorland Ave) Approach | 44.3 | E | 78.2 | F | 59.0 | F | 109.3 | F |
| 3. | Todd Rd/US 101 South Ramps | 17.8 | B | 22.7 | C | 18.5 | B | 22.2 | C |
| 4. | Todd Rd/US 101 North Ramps | 7.4 | A | 6.3 | A | 6.9 | A | 7.1 | A |
| 5. | Todd Rd/Santa Rosa Ave | 10.9 | B | 18.6 | B | 12.1 | B | 19.6 | B |

Notes: Delay is measured in average seconds per vehicle; LOS = Level of Service; Results for minor approaches to two-way stop-controlled intersections are indicated in italics; ** $=$ delay greater than 120 seconds; Bold text $=$ deficient operation; Shaded cells = conditions with recommended improvements

It should be noted that with the addition of project-related traffic volumes, average delay on the northbound Ghilotti Avenue approach decreases during both peak hours. While this is counter-intuitive, this condition occurs when a project adds trips to movements that are currently underutilized or have delays that are below the approach average, resulting in a better balance between movements and lower average delay for that specific approach. The project adds traffic predominantly to the right-turn movement, which has an average delay that is lower than the average for the entire approach, resulting in a slight reduction in the average delay. This same reasoning also explains why delay decreases slightly at Todd Road/US 101 South Ramps during the evening peak hour.

Finding - The project would increase the overall average delay at Todd Road/Standish Avenue-Ghilotti Avenue by more than five seconds during the p.m. peak hour and therefore would have a significant impact per the County Standard.

Recommendation - It is understood that the County is planning on installing a traffic signal at Todd Road/ Standish Avenue-Ghilotti Avenue and will accept proportional share payments towards this project. To mitigate project impacts, is recommended that Ghilotti Construction pay a proportional share fee of 11.1 percent toward the installation of a traffic signal and southbound left-turn lane at Todd Road/Standish Avenue-Ghilotti Avenue. A copy of the Equitable Share Calculation spreadsheet is contained in Appendix D.

## Baseline plus Project Conditions

With project-related traffic added to Baseline volumes, the study intersections are expected to operate acceptably except for Todd Road/Standish Avenue-Ghilotti Avenue during the p.m. peak hour. Baseline plus Project volumes are provided in Figure 9, and the resulting levels of service are summarized in Table 10.





Table 10 - Baseline and Baseline plus Project Peak Hour Intersection Levels of Service

| Study Intersection <br> Approach | Baseline Conditions |  |  |  | Baseline plus Project |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AM Peak | PM Peak | AM Peak |  | PM Peak |  |  |

Notes: Delay is measured in average seconds per vehicle; LOS = Level of Service; Results for minor approaches to two-way stop-controlled intersections are indicated in italics; ${ }^{* *}=$ delay greater than 120 seconds; Bold text $=$ deficient operation; Shaded cells = conditions with recommended improvements

Finding - Consistent with Existing plus Project Conditions, the project would increase the overall average delay at Todd Road/Standish Avenue-Ghilotti Avenue by more than five seconds during the p.m. peak hour and therefore would have a significant impact per the County Standard.

Recommendation - As stated previously, the County is planning on installing a traffic signal at Todd Road/ Standish Avenue-Ghilotti Avenue and will accept proportional share payments towards this project. To mitigate its impacts, the project should pay its proportional share of 11.1 percent toward the cost of the improvements.

## Future plus Project Conditions

Upon the addition of project-related traffic to Future volumes, the study intersections that were operating acceptably would continue to operate acceptably and the intersections that were operating unacceptably would continue to operate unacceptably. Future plus Project volumes are shown in Figure 10, and the Future plus Project levels of service are summarized in Table 11.



Table 11 - Future and Future plus Project Peak Hour Intersection Levels of Service

| Study Intersection Approach | Future Conditions |  |  |  | Future plus Project |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AM Peak |  | PM Peak |  | AM Peak |  | PM Peak |  |
|  | Delay | LOS | Delay | LOS | Delay | LOS | Delay | LOS |
| 1. Todd Rd/Standish Ave-Ghilotti Ave | ** | F | ** | F | ** | F | ** | F |
| Northbound (Ghilotti Ave) Approach | 18.2 | C | 17.9 | C | 17.3 | C | 18.2 | C |
| Southbound (Standish Ave) Approach | ** | F | ** | F | ** | $F$ | ** | $F$ |
| With signal and SB left-turn lane | 30.1 | C | 38.2 | D | 36.6 | D | 44.1 | D |
| 2. Todd Rd/Moorland Ave | 3.8 | A | 14.3 | B | 4.2 | A | 17.5 | C |
| Southbound (Moorland Ave) Approach | 35.1 | E | 91.4 | F | 40.8 | E | 116.8 | $F$ |
| 3. Todd Rd/US 101 South Ramps | 19.6 | B | 18.9 | B | 21.4 | C | 16.4 | B |
| 4. Todd Rd/US 101 North Ramps | 7.6 | A | 7.4 | A | 7.5 | A | 7.4 | A |
| 5. Todd Rd/Santa Rosa Ave | 63.8 | F | 77.2 | F | 63.9 | F | 80.4 | F |
| With two NB Left-turn Lanes | 24.1 | C | 40.8 | D | 21.2 | C | 38.2 | D |

Notes: Delay is measured in average seconds per vehicle; LOS = Level of Service; Results for minor approaches to two-way stop-controlled intersections are indicated in italics; ** = delay greater than 120 seconds; Bold text = deficient operation; Shaded cells = conditions with recommended improvements; SB = Southbound; NB = Northbound

Finding - Installation of a traffic signal at Todd Road/Standish Avenue-Ghilotti Avenue will be necessary to achieve acceptable operation under the projected Future conditions with or without the proposed project. Although Todd Road/Santa Rosa Avenue is expected to deteriorate to LOS F under Future Conditions, the addition of project traffic would result in less than a five-second increase in delay at the intersection, so the impact would be less-than-significant impact under the County's criterion. As noted for Future conditions without the project, in order for the intersection to operate acceptably the northbound approach would need to be restriped to provide two left-turn lanes. This improvement could be accomplished by restriping the western through lane into a second left-turn lane and the dedicated right-turn lane into a shared through/right-turn lane. This configuration would result in two left-turn lanes, a single through lane, and a shared through/right-turn lane.

Recommendation - As stated previously, the County is planning on installing a traffic signal at Todd Road/ Standish Avenue-Ghilotti Avenue and will accept proportional share payments towards this project. To mitigate its impacts, the project should pay its proportional share of 11.1 percent toward the cost of the improvements.

## Queuing

Under each scenario, the projected $95^{\text {th }}$ percentile queues in the left-turn pockets at the study intersections were determined using the SimTraffic application of Synchro, and averaging the $95^{\text {th }}$ percentile queue for each of ten runs. All five intersections were evaluated with their existing controls and lane configurations for all scenarios; no improvements were assumed to be in place. These results are summarized in Table 12 and copies of the SimTraffic projections are contained in Appendix F.

Table 12-95 ${ }^{\text {th }}$ Percentile Left-turn Queues at Study Intersections

| Study Intersection Approach | Avail. Storage | 95 ${ }^{\text {th }}$ Percentile Queues |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AM Peak Hour |  |  |  |  |  | PM Peak Hour |  |  |  |  |  |
|  |  | E | E+P | B | B+P | F | F+P | E | E+P | B | B+P | F | F+P |
| Todd Rd/Standish Ave-Ghilotti Ave Southbound | - | 134 | 111 | 106 | 147 | 529 | 520 | 213 | 269 | 208 | 270 | 541 | 480 |
| Eastbound | 120 | 46 | 43 | 43 | 39 | 75 | 83 | 29 | 28 | 30 | 29 | 63 | 32 |
| Westbound | 150 | 11 | 28 | 11 | 30 | 18 | 28 | 9 | 24 | 14 | 25 | 14 | 10 |
| Todd Rd/Moorland Ave |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Southbound | 50 | 97 | 139 | 124 | 137 | 72 | 140 | 204 | 387 | 137 | 254 | 277 | 230 |
| Eastbound | 100 | 23 | 20 | 17 | 25 | 65 | 86 | 37 | 35 | 33 | 52 | 57 | 58 |
| Todd Rd/US 101 S Ramps |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Northbound | 160 | 298 | 290 | 278 | 307 | 300 | 296 | 304 | 292 | 263 | 293 | 230 | 238 |
| Westbound | 285 | 132 | 141 | 148 | 146 | 200 | 216 | 259 | 284 | 249 | 259 | 205 | 248 |
| Todd Rd/US 101 N Ramps |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Northbound | 100 | 133 | 137 | 111 | 139 | 158 | 153 | 110 | 118 | 117 | 130 | 154 | 156 |
| Westbound | 190 | 136 | 126 | 129 | 124 | 149 | 152 | 143 | 134 | 138 | 175 | 132 | 131 |
| Todd Rd/Santa Rosa Ave |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Northbound | 105 | 155 | 158 | 169 | 171 | 342 | 365 | 264 | 268 | 305 | 292 | 340 | 370 |
| Southbound | 200 | 25 | 20 | 17 | 22 | 11 | 19 | 39 | 60 | 39 | 48 | 19 | 13 |
| Eastbound | 300 | 85 | 82 | 92 | 99 | 54 | 54 | 116 | 136 | 123 | 141 | 45 | 46 |
| Westbound | 60 | 27 | 37 | 26 | 33 | 48 | 53 | 86 | 82 | 62 | 73 | 104 | 104 |

Notes: $\quad 95^{\text {th }}$ Percentile Queue based on the average of ten SimTraffic runs; all distances are measured in feet; $\mathrm{E}=$ Existing conditions; $\mathrm{E}+\mathrm{P}=$ Existing plus Project conditions; $\mathrm{B}=$ Baseline conditions; $\mathrm{B}+\mathrm{P}=$ Baseline plus Project conditions; $F=$ Future conditions; F+P = Future plus Project conditions; Bold = queue length exceeds available storage

At Todd Road/Standish Avenue-Ghilotti Avenue, no left-turn queues are expected to exceed available storage; however the southbound left-turn queue is projected to reach a maximum length of 541 feet during the evening peak hour under Future Conditions. Signalization of the intersection and the provision of a separate left-turn lane would be expected to reduce the southbound queue to a more reasonable length.

Southbound queues are expected to exceed available storage at Todd Road/Moorland Avenue during both peak hours and for all evaluated scenarios; however there is no potential to extend the existing left-turn lane without acquiring additional right-of-way. The County should consider installing a traffic signal at the intersection. In addition to reducing queuing, a traffic signal would also reduce the high delay projected for the southbound approach under Future Conditions.

Northbound queues are expected to exceed available storage at Todd Road/US 101 South ramps and Todd Road/US 101 North ramps during both peak hours and for all evaluated scenarios. There is no potential to extend the northbound left-turn lane at Todd Road/US 101 South ramps due to the proximity of the South Moorland Avenue/Overcrossing intersection; however there is room to extend the northbound left-turn lane at Todd Road/US 101 North ramps. As this is a tee intersection, there is no through traffic to be impacted by the excess queueing, though some modification to the signal timing could achieve relief and allow right-turning traffic to
pass by the queue of left-turning vehicles. Again, because there is no higher-speed through traffic, the normal safety concern associated with left-turn queues that extend beyond available storage does not apply.

At Todd Road/Santa Rosa Avenue, left-turn queues are expected to exceed available storage in the northbound direction during both peak hours and all evaluated scenarios; however because the left-turn lane connects to a two-way left-turn lane that extends approximately 2,500 feet to Mountain View Avenue there is no safety concern associated with the queuing. Field observations confirmed that the queue is currently extending into the twoway left-turn lane well beyond the end of the existing left-turn lane during the p.m. peak hour. The dual left-turn lanes identified as being needed to reduce the northbound approach delay under Future Conditions would also reduce queuing. Westbound left-turn queues are expected to exceed available storage under all evaluated scenarios during the evening peak hour; however the project would not add any trips to this movement.

Finding - The project would not cause any queues to exceed available storage that would not be expected to exceed available storage without the project.

## Alternative Modes

## Pedestrian Facilities

The proposed use of the site as a construction yard would not be expected to generate any pedestrian traffic so the existing lack of pedestrian facilities would have no impact.

Finding - Pedestrian facilities serving the project site are adequate for the demand given the rural setting.

## Bicycle Facilities

The planned bicycle facilities summarized in the 2010 Santa Rosa Bicycle and Pedestrian Master Plan would provide adequate access for the anticipated demand. Since the project site has limited frontage on Todd Road and it would make more sense to stripe an appreciable length of the roadway in both directions versus an isolated short segment in one direction only, the project should make an in-lieu payment towards the planned bicycle facility improvements to be completed at a later time.

Finding - Bicycle facilities serving the project site are expected to be adequate upon completion of the planned improvements.

Recommendation - Because the project site has frontage on Todd Road and Class II bike lanes are planned on the roadway, the project should make an in-lieu payment to the County towards the cost of striping a future Class II bike lane along the project frontage.

## Transit

Existing transit routes are adequate to accommodate project-generated transit trips and the stops on Todd Road east of the project site are within acceptable walking distance.

Finding - Transit facilities serving the project site are adequate.

## Access and Circulation

## Site Access

## Sight Distance

At unsignalized driveways and intersections, a substantially clear line of sight should be maintained between the driver of a vehicle waiting on the driveway and the driver of an approaching vehicle. Adequate time must be provided for the waiting vehicle to either cross, turn left, or turn right, without requiring the through traffic drivers to radically alter their speed.

Sight distances along Todd Road at Ghilotti Avenue were evaluated based on sight distance criteria contained in $A$ Policy on Geometric Design on Highways and Streets published by American Association of State Highway and Transportation Officials (AASHTO). These guidelines include recommended sight distances at intersections, including stopping sight distances for drivers traveling along the major approaches and for drivers of stopped vehicles at the minor street approaches and driveways. These recommendations are based upon approach travel speeds, and take into account which direction a vehicle would turn onto the major approach, with greater sight distance needed for the more time-consuming task of turning left as compared to turning right.

For the posted $35-\mathrm{mph}$ speed limit on Todd Road adjacent to the project site, the recommended corner sight distance is 390 feet for a left-turn and 335 feet for a right turn. Based on a review of the field conditions, sight distance extends 500 feet to both the east and west which is enough to satisfy speeds greater than 35 mph .

Radar speed samples were obtained on the westbound and eastbound approaches of Todd Road at Ghilotti Avenue and prevailing speeds were found to be at or below the posted $35-\mathrm{mph}$ speed limit in both directions. The $85^{\text {th }}$ percentile speed for westbound vehicles was 29 mph , with a peak observed speed of 30 mph ; in the eastbound direction, the $85^{\text {th }}$ percentile speed was 35 mph , with a peak observed speed of 41 mph . Based on these actual approach speeds, the available sight distance in each direction is adequate. A copy of the speed survey data is contained in Appendix G.

Finding - Sight distances along Todd Road at Ghilotti Avenue are adequate for the posted speed limit; however, it is noted that the bushes/trees along the roadway frontage west of Ghilotti Avenue have the potential to interrupt sight lines.

Recommendation - To ensure that adequate sight lines are maintained to the west from Ghilotti Avenue it is recommended that the bushes/trees along the roadway frontage be regularly maintained.

## Conclusions and Recommendations

## Conclusions

- The project is expected to generate a maximum of 50 new truck trips per day including a maximum of 30 trips during either the a.m. or p.m. peak hour.
- Under Existing Conditions the study intersections operate acceptably at LOS A or B overall during the a.m. peak hour; however, Todd Road/Standish Avenue-Ghilotti Avenue operates unacceptably at LOS E overall during the p.m. peak hour.
- Under Existing Conditions, p.m. peak hour volumes at the intersection of Todd Road/Standish Avenue-Ghilotti Avenue are sufficient to meet the Peak Hour Volume signal warrant.
- Upon the addition of project-generated traffic to Existing volumes, the study intersections are expected to continue operating acceptably during the a.m. peak hour, but Todd Road/Standish Avenue-Ghilotti Avenue is expected to deteriorate to LOS F during the p.m. peak hour with an increase in average delay that exceeds the five seconds allowed under County Standards.
- Under Baseline Conditions, which includes traffic associated with the Shamrock Materials facility, all study intersections would operate acceptably during both peak hours except that Todd Road/Standish AvenueGhilotti Avenue is expected to continue operating unacceptably at LOS E during the p.m. peak hour.
- Upon the addition of project-related traffic to Baseline volumes, the study intersections would be expected to continue operating acceptably except for Todd Road/Standish Avenue-Ghilotti Avenue which would deteriorate to LOS F during the p.m. peak hour with an increase in average delay that exceeds five seconds.
- Under the anticipated Future volumes, the intersections of Todd Road with the US 101 North and South ramps and Todd Road/Moorland Avenue are expected to continue operating acceptably overall during both peak hours; Todd Road/Standish Avenue-Ghilotti Avenue and Todd Road/Santa Rosa Avenue are expected to operate unacceptably at LOS F during both peak hours.
- Upon the addition of project-related traffic to Future volumes, the study intersections would all be expected to continue operating at the same levels of service as without it.
- The project would not cause any left-turn queues to exceed available storage that would not be expected to exceed available storage without the project.
- Pedestrian and transit facilities are adequate to serve the project site given the site location and anticipated demand. Bicycle facilities will be adequate upon completion of the planned Class II bike lanes on Todd Road.
- Sight distances along Todd Road at Ghilotti Avenue are adequate for the measured approach speeds and the posted speed limit.


## Recommendations

- It is understood that the County is planning on installing a traffic signal at Todd Road/Standish AvenueGhilotti Avenue and will accept proportional share payments towards this project. As part of these
improvements the Standish Avenue approach should be restriped to provide a southbound left-turn lane with at least 135 feet of storage length.
- The County should consider restriping the northbound approach at Santa Rosa Avenue/Todd Road to provide two northbound left-turn lanes to accommodate the anticipated growth under Future volumes.
- The project applicant should pay a proportional share fee of 11.1 percent toward the installation of a traffic signal and southbound left-turn lane at Todd Road/Standish Avenue-Ghilotti Avenue.
- The project applicant should make an in-lieu payment toward the cost of striping a Class II bike lane along the project frontage on Todd Road.
- The bushes/trees along the roadway frontage west of Ghilotti Avenue should be trimmed regularly to maintain adequate sight lines.


## Study Participants and References

## Study Participants

| Principal in Charge | Dalene J. Whitlock, PE, PTOE |
| :--- | :--- |
| Assistant Engineer | Cameron Nye, EIT |
| Graphics | Hannah Yung |
| Editing/Formatting | Angela McCoy |

## References

2010 Santa Rosa Bicycle and Pedestrian Master Plan, City of Santa Rosa, 2010
2013 Collision Data on California State Highways, California Department of Transportation, 2013
A Policy on Geometric Design of Highways and Streets, $6^{\text {th }}$ Edition, American Association of State Highway and Transportation Officials, 2011
California Manual on Uniform Traffic Control Devices for Streets and Highways, California Department of Transportation, 2014
Guide for the Preparation of Traffic Impact Studies, California Department of Transportation, 2002
Guidelines for Traffic Impact Studies, County of Sonoma, 2016
Highway Capacity Manual, Transportation Research Board, 2010
Highway Design Manual, 6 ${ }^{\text {th }}$ Edition, California Department of Transportation, 2012
Sonoma County General Plan 2020, County of Sonoma, 2013
Sonoma County Municipal Code, Municipal Code Corporation, 2016
Sonoma County Transit, http://sctransit.com/
Statewide Integrated Traffic Records System (SWITRS), California Highway Patrol, 2012-2016
SOX574


## Appendix A

## Collision Rate Calculations



## Intersection Collision Rate Calculaions

## Ghilotti Construction Yard TIS

Intersection \# 3: Todd Rd \& US 101 S Ramps
Date of Count: Wednesday, June 07, 2017

Number of Collisions: 12
Number of Injuries: 2
Number of Fatalities: 0
ADT: 17800
Start Date: January 1, 2012
End Date: December 31, 2016
Number of Years: 5
Intersection Type: Four-Legged
Control Type: Signals
Area: Suburban
collision rate $=\frac{\text { Number of Collisions } \times 1 \text { Million }}{\text { ADT } \times 365 \text { Days per Year } \times \text { Number of Years }}$


|  | Collision Rate |  | Fatality Rate |
| :---: | :---: | :---: | :---: |
|  | Injury Rate |  |  |
| Study Intersection | 0.37 | c/mve | $0.0 \%$ |
| $16.7 \%$ |  |  |  |
|  | Statewide Average* | $0.43 \quad \mathrm{c} / \mathrm{mve}$ | $0.4 \%$ |
| $37.9 \%$ |  |  |  |

ADT = average daily total vehicles entering intersection
$\mathrm{c} / \mathrm{mve}=$ collisions per million vehicles entering intersection

* 2013 Collision Data on California State Highways, Caltrans


## Intersection \# 4: Todd Rd \& US 101 N Ramps

Date of Count: Wednesday, June 07, 2017

Number of Collisions: 8
Number of Injuries: 2
Number of Fatalities: 0
ADT: 17400
Start Date: January 1, 2012
End Date: December 31, 2016
Number of Years: 5

Intersection Type: Tee
Control Type: Signals
Area: Suburban
collision rate $=\frac{\text { Number of Collisions } \times 1 \text { Million }}{\text { ADT } \times 365 \text { Days per Year } \times \text { Number of Years }}$

collision rate $=$|  | 8 | $x$ | $1,000,000$ |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | ---: | ---: | :---: | :---: | :---: | :---: |
|  | 17,400 | x |  | 365 | x |  |  |  |  |

|  | Collision Rate |  | Fatality Rate |
| :---: | :---: | :---: | :---: |
| Study Intersection | Injury Rate |  |  |
|  | 0.25 | c/mve | $0.0 \%$ |
| Statewide Average* | 0.27 | c/mve | $0.6 \%$ |

ADT = average daily total vehicles entering intersection
$\mathrm{c} / \mathrm{mve}=$ collisions per million vehicles entering intersection

* 2013 Collision Data on California State Highways, Caltrans



## Appendix B

Unsignalized Intersection Level of Service Calculations

Generated with PTV VISTRO
Version 5.00-00

| Intersection Level Of Service ReportIntersection 1: Todd Ral/Ghilotti Ave-Standish Ave |  |  |  |
| :---: | :---: | :---: | :---: |
| Control Type: | Two-way stop | Delay (sec / veh): | 54.5 |
| Analysis Method: | HCM 2010 | Level Of Service: | F |
| Analysis Period: | 15 minutes | Volume to Capacity (v/c) | 0.720 |


| Name | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |
| Lane Configuration | + |  |  | + |  |  | $71$ |  |  | $7 F$ |  |  |
| Turning Movement | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [f] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 |
| Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 120.00 | 100.00 | 100.00 | 150.00 | 100.00 | 100.00 |
| Speed [mph] | 10.00 |  |  | 30.00 |  |  | 35.00 |  |  | 35.00 |  |  |
| Grade [\%] | 0.00 |  |  | 0.00 |  |  | $\frac{0.00}{\text { No }}$ |  |  | $\frac{0.00}{\text { No }}$ |  |  |
| Crosswalk | No |  |  | No |  |  |  |  |  |  |  |  |

Volumes

| Name | Ghiotti Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 2 | 2 | 10 | 150 | 1 | 43 | 91 | 283 | 2 | 12 | 232 | 259 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [ven/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 2 | 2 | 10 | 150 | 1 | 43 | 91 | 283 | 2 | 12 | 232 | 259 |
| Peak Hour Factor | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 1 | 1 | 3 | 40 | 0 | 12 | 25 | 76 | 1 | 3 | 63 | 70 |
| Total Analysis Volume [veh/h] | 2 | 2 | 11 | 162 | 1 | 46 | 98 | 305 | 2 | 13 | 250 | 279 |
| Pedestrian Volume [ped/h] | 0 |  |  | 0 |  |  | - 0 |  |  | 0 |  |  |

## enerated with PTV VISTRC

ction Settings

| Priority Scheme | Stop | Stop | Free | Free |
| :---: | :---: | :---: | :---: | :---: |
| Flared Lane | No | Yes |  |  |
| Storage Area [veh] | 0 | 1 | 0 | 0 |
| Two-Stage Gap Acceptance | No | No |  |  |
| Number of Storage Spaces in Median | 0 | 0 | 0 | 0 |

Movement, Approach, \& Intersection Results

| V/C, Movement V/C Ratio | 0.01 | 0.01 | 0.01 | 0.72 | 0.00 | 0.07 | 0.09 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d_M, Delay for Movement [s/ven] | 22.63 | 23.15 | 10.20 | 54.46 | 53.26 | 43.92 | 8.83 | 0.00 | 0.00 | 7.90 | 0.00 | 0.00 |
| Movement LOS | c | c | B | F | F | E | A | A | A | A | A | A |
| 95th-Percentile Queue Length [veh] | 0.11 | 0.11 | 0.11 | 5.77 | 5.77 | 5.77 | 0.31 | 0.00 | 0.00 | 0.03 | 0.00 | 0.00 |
| 95 th-Percentile Queue Length [ft] | 2.68 | 2.68 | 2.68 | 144.16 | 144.16 | 144.16 | 7.80 | 0.00 | 0.00 | 0.79 | 0.00 | 0.00 |
| d_A, Approach Delay [s/ven] | 13.58 |  |  | 52.14 |  |  | 2.14 |  |  | 0.19 |  |  |
| Approach Los | B |  |  | F |  |  | A |  |  | A |  |  |
| d_I, Intersection Delay [s/ven] | 10.31 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS | F |  |  |  |  |  |  |  |  |  |  |  |

Ghilotti Construction Yard TIS

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PTV VISTRO

| Intersection Level Of Service Report Intersection 2: Todd Rd/Moorland Ave |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Control Type: | Two-way stop HCM 2010 |  | Delay (sec / veh): |  |  |  |
| Analysis Method: |  |  | Level Of Service: |  | F |  |
| Analysis Period: | 15 minutes |  |  | to Capa | 0.668 |  |
| Intersection Setup |  |  |  |  |  |  |
| Name | Moorland Ave |  | Todd Rd |  | Todd Rd |  |
| Approach | Southbound |  | Eastbound |  | Westbound |  |
| Lane Configuration | $7$ |  | $7$ |  | $F$ |  |
| Turning Movement | Left | Right | Left | Thru | Thru | Right |
| Lane Width [tt] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Pocket | 0 | 1 | 1 | 0 | 1 | 0 |
| Pocket Length [ft] | 100.00 | 50.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| Speed [mph] | 30.00 |  | 35.00 |  | 35.00 |  |
| Grade [\%] | 0.00 |  | 0.00 |  | 0.00 |  |
| Crosswalk | No |  | No |  | No |  |

Volumes

| Name | Moorland Ave |  | Todd Rd |  | Todd Rd |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 124 | 30 | 12 | 475 | 494 | 143 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 124 | 30 | 12 | 475 | 494 | 143 |
| Peak Hour Factor | 0.9000 | 0.9000 | 0.9000 | 0.9000 | 0.9000 | 0.9000 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 34 | 8 | 3 | 132 | 137 | 40 |
| Total Analysis Volume [veh/h] | 138 | 33 | 13 | 528 | 549 | 159 |
| Pedestrian Volume [pedh] |  | 0 |  |  |  | 0 |

Ghilotti Construction Yard TIS
AM Existing
(V) W-Trans

W-Trans

## Generated with PTV VISTRO

Version 5.00-00
Control Type:
Analysis Method:

| Intersection Level Of Service Report |  |  |
| :---: | :---: | :---: |
| Intersection 1: Todd Rd/Ghilotti Ave-Standish Ave |  |  |
| Devay (sec / veh): |  |  |
| Two-way stop | Level Of Service: | 138.5 |
| HCM 2010 | Volume to Capacity (v/c): | 1.050 |
| 15 minutes |  |  |

Intersection Setup

| Name | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |
| Lane Configuration | 中 |  |  | 中 |  |  | $7$ |  |  | $7 \mathrm{~F}$ |  |  |
| Turning Movement | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 |
| Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 120.00 | 100.00 | 100.00 | 150.00 | 100.00 | 100.00 |
| Speed [mph] | 10.00 |  |  | 30.00 |  |  | 35.00 |  |  | 35.00 |  |  |
| Grade [\%] | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  |
| Crosswalk | No |  |  | No |  |  | No |  |  | No |  |  |

Volumes

| Name | ti Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2 | 4 | 20 | 252 | 2 | 65 | 45 | 316 | 7 | 10 | 264 | 171 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [vehh/] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 2 | 4 | 20 | 252 | 2 | 65 | 45 | 316 | 7 | 10 | 264 | 171 |
| Peak Hour Factor | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 1 | 1 | 5 | 68 | 1 | 17 | 12 | 85 | 2 | 3 | 71 | 46 |
| Total Analysis Volume [veh/h] | 2 | 4 | 21 | 271 | 2 | 70 | 48 | 339 | 8 | 11 | 284 | 184 |
| Pedestrian Volume [ped/h] |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |

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| Priorsection Scheme | Stop | Stop | Free | Free |
| :---: | :---: | :---: | :---: | :---: |
| Flared Lane | No | Yes |  |  |
| Storage Area [veh] | 0 | 1 | 0 | 0 |
| Two-Stage Gap Acceptance | No | No |  |  |
| Number of Storage Spaces in Median | 0 | 0 | 0 | 0 |

Movement, Approach, \& Intersection Results

| V/C, Movement V/C Ratio | 0.01 | 0.02 | 0.03 | 1.05 | 0.01 | 0.10 | 0.04 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d_M, Delay for Movement [s/ven] | 20.98 | 19.62 | 10.56 | 138.50 | 137.17 | 129.92 | 8.44 | 0.00 | 0.00 | 8.00 | 0.00 | 0.00 |
| Movement LOS | c | c | B | F | F | F | A | A | A | A | A | A |
| 95th-Percentile Queue Length [veh] | 0.17 | 0.17 | 0.17 | 14.47 | 14.47 | 14.47 | 0.14 | 0.00 | 0.00 | 0.03 | 0.00 | 0.00 |
| 95 th-Percentile Queue Length [ft] | 4.31 | 4.31 | 4.31 | 361.75 | 361.75 | 361.75 | 3.44 | 0.00 | 0.00 | 0.69 | 0.00 | 0.00 |
| d_A, Approach Delay [s/ven] | 12.68 |  |  | 136.74 |  |  | 1.03 |  |  | 0.18 |  |  |
| Approach Los | B |  |  | F |  |  | A |  |  | A |  |  |
| d_I, Intersection Delay [s/ven] | 38.37 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS |  |  |  |  |  |  |  |  |  |  |  |  |

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Version $5.00-00$
PTV VISTRO

| Intersection Level Of Service Report Intersection 2: Todd Rd/Moorland Ave |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Control Type: | Two-way stop HCM 2010 |  | Delay (sec / veh): |  |  | $92.1$ |
| Analysis Method: |  |  |  | l Of Ser |  |  |
| Analysis Period: |  |  | Volume to Capacity (v/c): |  |  |  |
| Intersection Setup |  |  |  |  |  |  |
| Name | Moorland Ave |  | Todd Rd |  | Todd Rd |  |
| Approach | Southbound |  | Eastbound |  | Westbound |  |
| Lane Configuration | 75 |  | $7$ |  | $F$ |  |
| Turning Movement | Left | Right | Left | Thru | Thru | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Pocket | 0 | 1 | 1 | 0 | 1 | 0 |
| Pocket Length [ft] | 100.00 | 50.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| Speed [mph] | 30.00 |  | 35.00 |  | 35.00 |  |
| Grade [\%] | 0.00 |  | 0.00 |  | 0.00 |  |
| Crosswalk | No |  | No |  | No |  |

Volumes

| Name | Moorland Ave |  | Todd Rd |  | Todd Rd |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 142 | 30 | 40 | 606 | 428 | 189 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 142 | 30 | 40 | 606 | 428 | 189 |
| Peak Hour Factor | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 38 | 8 | 11 | 161 | 114 | 50 |
| Total Analysis Volume [veh/h] | 151 | 32 | 43 | 645 | 455 | 201 |
| Pedestrian Volume [pedh] |  |  |  |  |  |  |

## Generated with PTV VISTRO

Version $5.00-00$

| Priority Scheme | Stop | Free | Free |
| :---: | :---: | :---: | :---: |
| Flared Lane |  |  |  |
| Storage Area [veh] | 0 | 0 | 0 |
| Two-Stage Gap Acceptance | No |  |  |
| Number of Storage Spaces in Median | 0 | 0 | 0 |

Movement, Approach, \& Intersection Results

| V/C, Movement V/C Ratio | 0.87 | 0.06 | 0.05 | 0.01 | 0.00 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d_M, Delay for Movement [s/veh] | 92.14 | 12.21 | 9.05 | 0.00 | 0.00 | 0.00 |
| Movement LOS | F | B | A | A | A | A |
| 95 th-Percentile Queue Length [veh] | 6.28 | 0.19 | 0.15 | 0.00 | 0.00 | 0.00 |
| 95 th-Percentile Queue Length [ft] | 156.97 | 4.80 | 3.63 | 0.00 | 0.00 | 0.00 |
| d_A, Approach Delay [s/ven] | 78.17 |  | 0.57 |  | 0.00 |  |
| Approach LOS | F |  | A |  | A |  |
| d_I, Intersection Delay [s/veh] | 9.62 |  |  |  |  |  |
| Intersection LOS | F |  |  |  |  |  |

## Generated with PTV VISTRO

| Intersection Level Of Service Report Intersection 1: Todd Rd/Ghilotti Ave-Standish Ave |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Control Type: | Signalized HCM 2010 |  |  |  |  | Delay (sec / veh): |  |  |  | 16.9$B$ |  |  |
| Analysis Method: |  |  |  |  |  |  | Level Of | Service: |  |  |  |  |
| Analysis Period: | HCM 2010 15 minutes |  |  |  |  | Volume to Capacity (v/c): |  |  |  | 0.582 |  |  |
| Intersection Setup |  |  |  |  |  |  |  |  |  |  |  |  |
| Name | Ghiloti Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| Approach | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |
| Lane Configuration | 中 |  |  | $7 \mathrm{~F}$ |  |  | $7 \mathrm{~F}$ |  |  | $7 \mathrm{~F}$ |  |  |
| Turning Movement | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Pocket | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 |
| Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 120.00 | 100.00 | 100.00 | 150.00 | 100.00 | 100.00 |
| Speed [mph] |  | 10.00 |  |  | 30.00 |  |  | 35.00 |  |  | 35.00 |  |
| Grade [\%] |  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |
| Crosswalk |  | No |  |  | No |  |  | No |  |  | No |  |


| Name | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 2 | 2 | 10 | 150 | 1 | 43 | 91 | 283 | 2 | 12 | 232 | 259 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Right-Turn on Red Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 2 | 2 | 10 | 150 | 1 | 43 | 91 | 283 | 2 | 12 | 232 | 259 |
| Peak Hour Factor | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 1 | 1 | 3 | 40 | 0 | 12 | 25 | 76 | 1 | 3 | 63 | 70 |
| Total Analysis Volume [veh/h] | 2 | 2 | 11 | 162 | 1 | 46 | 98 | 305 | 2 | 13 | 250 | 279 |
| Presence of On-Street Parking | No |  | No | No |  | No | No |  | No | No |  | No |
| On-Stret Parking Maneuver Rate [/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Local Bus Stopping Rate [h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pedestrian Volume [ped/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |
| Bicycle Volume [bicycles/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |

Generated with PTV VISTRO

## Intersection Settings

| Located in CBD | No |
| :---: | :---: |
| Signal Coordination Group |  |
| Cycle Length [s] | 60 |
| Coordination Type | Time of Day Pattern Isolated |
| Actuation Type | Fully actuated |
| Offset $[s]$ | 0.0 |
| Offset Reference | LeadGreen |
| Permissive Mode | SingleBand |
| Lost time $[s]$ | 12.00 |

## Phasing \& Timing

| Control Type | Split | Split | Split | Split | Split | Split | Protecte | Permiss | Permiss | Protecte | Permiss | Permiss |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Signal group | 0 | 2 | 0 | 0 | 6 | 0 | 3 | 8 | 0 | 7 | 4 | 0 |
| Auxiliary Signal Groups |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead/Lag | - | - | - | - | - | - | Lead | - | . | Lead | . | . |
| Minimum Green [s] | 0 | 5 | 0 | 0 | 5 | 0 | 5 | 5 | 0 | 5 | 5 | 0 |
| Maximum Green [s] | 0 | 30 | 0 | 0 | 30 | 0 | 30 | 30 | 0 | 30 | 30 | 0 |
| Amber [s] | 0.0 | 3.0 | 0.0 | 0.0 | 3.0 | 0.0 | 3.0 | 3.0 | 0.0 | 3.0 | 3.0 | 0.0 |
| All red [s] | 0.0 | 1.0 | 0.0 | 0.0 | 1.0 | 0.0 | 1.0 | 1.0 | 0.0 | 1.0 | 1.0 | 0.0 |
| Split [s] | 0 | 21 | 0 | 0 | 9 | 0 | 10 | 9 | 0 | 21 | 20 | 0 |
| Vehicle Extension [s] | 0.0 | 3.0 | 0.0 | 0.0 | 3.0 | 0.0 | 3.0 | 3.0 | 0.0 | 3.0 | 3.0 | 0.0 |
| Walk [s] | 0 | 5 | 0 | 0 | 5 | 0 | 0 | 5 | 0 | 0 | 5 | 0 |
| Pedestrian Clearance [s] | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 10 | 0 |
| Rest In Walk |  | No |  |  | No |  |  | No |  |  | No |  |
| 11, Start-Up Lost Time [s] | 0.0 | 2.0 | 0.0 | 0.0 | 2.0 | 0.0 | 2.0 | 2.0 | 0.0 | 2.0 | 2.0 | 0.0 |
| 12, Clearance Lost Time [s] | 0.0 | 2.0 | 0.0 | 0.0 | 2.0 | 0.0 | 2.0 | 2.0 | 0.0 | 2.0 | 2.0 | 0.0 |
| Minimum Recall |  | No |  |  | No |  | No | No |  | No | No |  |
| Maximum Recall |  | No |  |  | No |  | No | No |  | No | No |  |
| Pedestrian Recall |  | No |  |  | No |  | No | No |  | No | No |  |
| Detector Location [ft] | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector Length [ft] | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | ${ }^{0.0}$ | ${ }^{0.0}$ |
| I, Upstream Filtering Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Exclusive Pedestrian Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Pedestrian Signal Group |  |  |  |  |  |  | 0 |  |  |  |  |  |
| Pedestrian Walk [s] |  |  |  |  |  |  | 0 |  |  |  |  |  |
| Pedestrian Clearance [s] |  |  |  |  |  |  | 0 |  |  |  |  |  |

## Generated with PTV VISTRO

Version 5.00-00

| Lane Group | c | L | c | L | c | L | c |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C, Cycle Length [s] | 60 | 60 | 60 | 60 | 60 | 60 | 60 |
| L, Total Lost Time per Cycle [s] | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 |
| 11_p, Permitted Start-Up Lost Time [s] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 12, Clearance Lost Time [s] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| g_i, Effective Green Time [s] | 1 | 8 | 8 | 4 | 34 | 1 | 31 |
| $\mathrm{g} / \mathrm{C}, \mathrm{Green}$ / Cycle | 0.02 | 0.13 | 0.13 | 0.07 | 0.57 | 0.02 | 0.52 |
| ( $\mathrm{V} / \mathrm{s}$ )_i Volume / Saturation Flow Rate | 0.01 | 0.09 | 0.03 | 0.06 | 0.17 | 0.01 | 0.31 |
| s , saturation flow rate [ [veh/h] | 1640 | 1774 | 1588 | 1774 | 1861 | 1774 | 1704 |
| c, Capacity [veh/h] | 34 | 224 | 200 | 132 | 1059 | 33 | 875 |
| d1, Uniform Delay [s] | 29.18 | 25.34 | 23.73 | 27.34 | 6.70 | 29.26 | 10.35 |
| k, delay calibration | 0.11 | 0.11 | 0.11 | 0.11 | 0.50 | 0.11 | 0.50 |
| I, Upstream Fillering Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| d2, Incremental Delay [s] | 8.70 | 4.41 | 0.59 | 7.93 | 0.69 | 7.54 | 3.09 |
| d3, Initial Queue Delay [s] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Rp, platoon ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| PF, progression factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |


| X, volume / capacity | 0.44 | 0.72 | 0.23 | 0.74 | 0.29 | 0.40 | 0.60 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d, Delay for Lane Group [s/veh] | 37.88 | 29.75 | 24.32 | 35.27 | 7.39 | 36.79 | 13.45 |
| Lane Group LOS | D | c | c | D | A | D | B |
| Critical Lane Group | Yes | Yes | No | Yes | No | No | Yes |
| 50th-Percentile Queue Length [veh] | 0.30 | 2.37 | 0.60 | 1.57 | 1.69 | 0.24 | 4.57 |
| 50th-Percentile Queue Length [t]] | 7.50 | 59.15 | 15.03 | 39.35 | 42.25 | 6.08 | 114.31 |
| 95th-Percentile Queue Length [veh] | 0.54 | 4.26 | 1.08 | 2.83 | 3.04 | 0.44 | 8.08 |
| 95th-Percentile Queue Length [tt] | 13.51 | 106.46 | 27.06 | 70.83 | 76.05 | 10.94 | 201.98 |

## Generated with PTV VISTRO

Version $5.00-00$
Movement, Approach, \& Intersection Results

| d_M, Delay for Movement [s/ven] | 37.88 | 37.88 | 37.88 | 29.75 | 24.32 | 24.32 | 35.27 | 7.39 | 7.39 | 36.79 | 13.45 | 13.45 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement LOS | D | D | D | c | c | c | D | A | A | D | B | B |
| d_A, Approach Delay [s/ven] | 37.88 |  |  | 28.53 |  |  | 14.14 |  |  | 14.01 |  |  |
| Approach Los | D |  |  | c |  |  | B |  |  | B |  |  |
| d_l, Intersection Delay [s/veh] | 16.95 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS | B |  |  |  |  |  |  |  |  |  |  |  |
| Intersection V/C | 0.582 |  |  |  |  |  |  |  |  |  |  |  |



## Generated with PTV VISTRO



| Name | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 2 | 4 | 20 | 252 | 2 | 65 | 45 | 316 | 7 | 10 | 264 | 171 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Right-Turn on Red Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 2 | 4 | 20 | 252 | 2 | 65 | 45 | 316 | 7 | 10 | 264 | 171 |
| Peak Hour Factor | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 1 | 1 | 5 | 68 | 1 | 17 | 12 | 85 | 2 | 3 | 71 | 46 |
| Total Analysis Volume [veh/h] | 2 | 4 | 21 | 271 | 2 | 70 | 48 | 339 | 8 | 11 | 284 | 184 |
| Presence of On-Street Parking | No |  | No | No |  | No | No |  | No | No |  | No |
| On-Stret Parking Maneuver Rate [/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Local Bus Stopping Rate [h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pedestrian Volume [ped/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |
| Bicycle Volume [bicycles/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |

Generated with PTV VISTRO

## Intersection Settings

| Located in CBD | No |
| :---: | :---: |
| Signal Coordination Group |  |
| Cycle Length [s] | 60 |
| Coordination Type | Time of Day Pattern Isolated |
| Actuation Type | Fully actuated |
| Offset $[s]$ | 0.0 |
| Offset Reference | LeadGreen |
| Permissive Mode | SingleBand |
| Lost time $[s]$ | 16.00 |

## Phasing \& Timing

| Control Type | Split | Split | Split | Split | Split | Split | Protecte | Permiss | Permiss | Protecte | Permiss | Permiss |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Signal group | 0 | 2 | 0 | 0 | 6 | 0 | 3 | 8 | 0 | 7 | 4 | 0 |
| Auxiliary Signal Groups |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead/Lag | - | - | - | - | - | - | Lead | - | - | Lead | . | . |
| Minimum Green [s] | 0 | 5 | 0 | 0 | 5 | 0 | 5 | 5 | 0 | 5 | 5 | 0 |
| Maximum Green [s] | 0 | 30 | 0 | 0 | 30 | 0 | 30 | 30 | 0 | 30 | 30 | 0 |
| Amber [s] | 0.0 | 3.0 | 0.0 | 0.0 | 3.0 | 0.0 | 3.0 | 3.0 | 0.0 | 3.0 | 3.0 | 0.0 |
| All red [s] | 0.0 | 1.0 | 0.0 | 0.0 | 1.0 | 0.0 | 1.0 | 1.0 | 0.0 | 1.0 | 1.0 | 0.0 |
| Split [s] | 0 | 9 | 0 | 0 | 26 | 0 | 9 | 16 | 0 | 9 | 16 | 0 |
| Vehicle Extension [s] | 0.0 | 3.0 | 0.0 | 0.0 | 3.0 | 0.0 | 3.0 | 3.0 | 0.0 | 3.0 | 3.0 | 0.0 |
| Walk [s] | 0 | 5 | 0 | 0 | 5 | 0 | 0 | 5 | 0 | 0 | 5 | 0 |
| Pedestrian Clearance [s] | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 10 | 0 |
| Rest In Walk |  | No |  |  | No |  |  | No |  |  | No |  |
| 11, Start-Up Lost Time [s] | 0.0 | 2.0 | 0.0 | 0.0 | 2.0 | 0.0 | 2.0 | 2.0 | 0.0 | 2.0 | 2.0 | 0.0 |
| 12, Clearance Lost Time [s] | 0.0 | 2.0 | 0.0 | 0.0 | 2.0 | 0.0 | 2.0 | 2.0 | 0.0 | 2.0 | 2.0 | 0.0 |
| Minimum Recall |  | No |  |  | No |  | No | No |  | No | No |  |
| Maximum Recall |  | No |  |  | No |  | No | No |  | No | No |  |
| Pedestrian Recall |  | No |  |  | No |  | No | No |  | No | No |  |
| Detector Location [ft] | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector Length [ft] | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | ${ }^{0.0}$ | ${ }^{0.0}$ |
| I, Upstream Filtering Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Exclusive Pedestrian Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Pedestrian Signal Group |  |  |  |  |  |  | 0 |  |  |  |  |  |
| Pedestrian Walk [s] |  |  |  |  |  |  | 0 |  |  |  |  |  |
| Pedestrian Clearance [s] |  |  |  |  |  |  | 0 |  |  |  |  |  |

## Generated with PTV VISTRO

Version 5.00-00

| Lane Group | c | L | c | L | c | L | c |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| c, Cycle Length [s] | 60 | 60 | 60 | 60 | 60 | 60 | 60 |
| L, Total Lost Time per Cycle [s] | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 |
| 11_p, Permitted Start-Up Lost Time [s] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 12, Clearance Lost Time [s] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| g_i, Effective Green Time [s] | 2 | 12 | 12 | 3 | 30 | 1 | 28 |
| $\mathrm{g} / \mathrm{C}, \mathrm{Green}$ / Cycle | 0.03 | 0.19 | 0.19 | 0.05 | 0.50 | 0.02 | 0.46 |
| ( $\mathrm{V} / \mathrm{s}$ ) i Volume / Saturation Flow Rate | 0.02 | 0.15 | 0.05 | 0.03 | 0.19 | 0.01 | 0.27 |
| s , saturation flow rate [ [veh/h] | 1633 | 1774 | 1590 | 1774 | 1855 | 1774 | 1742 |
| c, Capacity [veh/h] | 53 | 343 | 307 | 85 | 914 | 29 | 803 |
| d1, Uniform Delay [s] | 28.69 | 23.17 | 20.56 | 28.09 | 9.54 | 29.36 | 11.98 |
| k, delay calibration | 0.11 | 0.11 | 0.11 | 0.11 | 0.50 | 0.11 | 0.50 |
| I, Upstream Fillering Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| d2, Incremental Delay [s] | 7.24 | 4.12 | 0.39 | 5.78 | 1.20 | 8.14 | 3.08 |
| d3, Initial Queue Delay [s] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Rp, platoon ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| PF, progression factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |


| X, volume / capacity | 0.51 | 0.79 | 0.23 | 0.57 | 0.38 | 0.38 | . 58 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d, Delay for Lane Group [s/veh] | 35.93 | 27.29 | 20.95 | 33.87 | 10.74 | 37.50 | 15.06 |
| Lane Group LOS | D | c | c | C | B | D | B |
| Critical Lane Group | Yes | Yes | No | Yes | No | No | Yes |
| 50th-Percentile Queue Length [veh] | 0.50 | 3.79 | 0.83 | 0.77 | 2.58 | 0.21 | 4.43 |
| 50th-Percentile Queue Length [t]] | 12.43 | 94.69 | 20.84 | 19.21 | 64.39 | 5.32 | 110.80 |
| 95th-Percentile Queue Length [veh] | 0.89 | 6.82 | 1.50 | 1.38 | 4.64 | 0.38 | 7.88 |
| 95th-Percentile Queue Length [tt] | 22.37 | 170.45 | 37.52 | 34.58 | 115.90 | 9.57 | 197.12 |

## Generated with PTV VISTRO

$\frac{\text { Version } 5.00-00}{\text { Movement, Approach, \& Intersection Results }}$

| d_M, Delay for Movement [s/ven] | 35.93 | 35.93 | 35.93 | 27.29 | 20.95 | 20.95 | 33.87 | 10.74 | 10.74 | 37.50 | 15.06 | 15.06 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement LOS | D | D | D | c | c | c | c | в | B | D | B | B |
| d_A, Approach Delay [s/ven] | 35.93 |  |  | 25.96 |  |  | 13.55 |  |  | 15.57 |  |  |
| Approach Los | D |  |  | c |  |  | B |  |  | B |  |  |
| d_I, Intersection Delay [s/ven] | 18.24 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS | в |  |  |  |  |  |  |  |  |  |  |  |
| Intersection V/C | 0.634 |  |  |  |  |  |  |  |  |  |  |  |



Generated with PTV VISTRO
Version 5.00-00
PIV VISTRO


Volumes

| $\begin{gathered} \hline \text { Name } \\ \hline \text { Base Volume Input [veh/h] } \end{gathered}$ | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 3 | 2 | 17 | 150 | 1 | 43 | 91 | 283 | 3 | 19 | 232 | 259 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 3 | 2 | 17 | 150 | 1 | 43 | 91 | 283 | 3 | 19 | 232 | 259 |
| Peak Hour Factor | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 1 | 1 | 5 | 40 | 0 | 12 | 25 | 76 | 1 | 5 | 63 | 70 |
| Total Analysis Volume [veh/h] | 3 | 2 | 18 | 162 | 1 | 46 | 98 | 305 | 3 | 20 | 250 | 279 |
| Pedestrian Volume [ped/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |

Generated with PTV VISTRO
Version 5.00-00
Control Type:
Analysis Method:
Two-way stop
HCM 2010
15 minutes
Intersection Level Of Service Repor
Intersection 2: Todd Rd/Moorland
Analysis Method:
Analysis Period:
5 minutes

> Delay (sec / ven): Level Of Servic:

Volume to Capacity (v/c) 54.4
$F$
0.684

| Name | Moorland Ave |  | Todd Rd |  | Todd Rd |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Southbound |  | Eastbound |  | Westbound |  |
| Lane Configuration | $7$ |  | $7$ |  | $F$ |  |
| Turning Movement | Left | Right | Left | Thru | Thru | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Pocket | 0 | 1 | 1 | 0 | 1 | 0 |
| Pocket Length [ft] | 100.00 | 50.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| Speed [mph] | 30.00 |  | 35.00 |  | 35.00 |  |
| Grade [\%] | 0.00 |  | 0.00 |  | 0.00 |  |
| Crosswalk | No |  | No |  | No |  |

Volumes

| $\frac{\text { Name }}{\text { Base Volume Input [veh/h] }}$ | Moorland Ave |  | Todd Rd |  | Todd Rd |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 124 | 30 | 12 | 482 | 501 | 143 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 124 | 30 | 12 | 482 | 501 | 143 |
| Peak Hour Factor | 0.9000 | 0.9000 | 0.9000 | 0.9000 | 0.9000 | 0.9000 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 34 | 8 | 3 | 134 | 139 | 40 |
| Total Analysis Volume [veh/h] | 138 | 33 | 13 | 536 | 557 | 159 |
| Pedestrian Volume [ped/h] | 0 |  | 0 |  | 0 |  |

Generated with PTV VISTRO
Version $5.00-00$
Version $5.00-00$


Volumes

| $\begin{gathered} \hline \text { Name } \\ \hline \text { Base Volume Input [veh/h] } \end{gathered}$ | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2 | 4 | 25 | 252 | 2 | 65 | 45 | 316 | 7 | 15 | 264 | 171 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [vehh] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 2 | 4 | 25 | 252 | 2 | 65 | 45 | 316 | 7 | 15 | 264 | 171 |
| Peak Hour Factor | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 1 | 1 | 7 | 68 | 1 | 17 | 12 | 85 | 2 | 4 | 71 | 46 |
| Total Analysis Volume [veh/h] | 2 | 4 | 27 | 271 | 2 | 70 | 48 | 339 | 8 | 16 | 284 | 184 |
| Pedestrian Volume [ped/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |

Generated with PTV VISTRO
Version 5.00-00
Control Type:
Analysis Method:
Two-way stop
HCM 2010
15 minutes
Intersection Level Of Service Repor
Intersection 2: Todd Rd/Moorland
Delay (sec / veh):
Level Of Service:
96.0
$F$

Volume to Capacity (v/c): $\quad \underset{0.887}{\mathrm{~F}}$

| Name | Moorland Ave |  | Todd Rd |  | Todd Rd |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Southbound |  | Eastbound |  | Westbound |  |
| Lane Configuration | 75 |  | $7$ |  | $F$ |  |
| Turning Movement | Left | Right | Left | Thru | Thru | Right |
| Lane Width [f] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Pocket | 0 | 1 | 1 | 0 | 1 | 0 |
| Pocket Length [ft] | 100.00 | 50.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| Speed [mph] | 30.00 |  | 35.00 |  | 35.00 |  |
| Grade [\%] | 0.00 |  | 0.00 |  | 0.00 |  |
| Crosswalk | No |  | No |  | No |  |

Volumes

| Name | Moorland Ave |  | Todd Rd |  | Todd Rd |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 142 | 30 | 40 | 611 | 433 | 189 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 142 | 30 | 40 | 611 | 433 | 189 |
| Peak Hour Factor | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 38 | 8 | 11 | 163 | 115 | 50 |
| Total Analysis Volume [veh/h] | 151 | 32 | 43 | 650 | 461 | 201 |
| Pedestrian Volume [ped/h] | 0 |  | 0 |  | 0 |  |

Generated with PTV VISTRO


Volum

| $\begin{gathered} \hline \text { Name } \\ \hline \text { Base Volume Input [veh/h] } \end{gathered}$ | Ghiloti Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 3 | 2 | 17 | 150 | 1 | ${ }^{43}$ | 91 | 283 | 3 | 19 | 232 | 259 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [vehh] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Righ-Turn on Red Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 3 | 2 | 17 | 150 | 1 | 43 | 91 | 283 | 3 | 19 | 232 | 259 |
| Peak Hour Factor | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 1 | 1 | 5 | 40 | 0 | 12 | 25 | 76 | 1 | 5 | 63 | 70 |
| Total Analysis Volume [veh/h] | 3 | 2 | 18 | 162 | 1 | 46 | 98 | 305 | 3 | 20 | 250 | 279 |
| Presence of On-Street Parking | No |  | No | No |  | No | No |  | No | No |  | No |
| On-Street Parking Maneuver Rate [/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Local Bus Stopping Rate [h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pedestrian Volume [ped/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |
| Bicycle Volume [bicycles/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |

Generated with PTV VISTRO
Version 5.00-00

| Lane Group | c | L | c | L | c | L | c |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| c, Cycle Length [s] | 60 | 60 | 60 | 60 | 60 | 60 | 60 |
| L. Total Lost Time per Cycle [s] | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 |
| 11_p, Permitted Start-Up Lost Time [s] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 12, Clearance Lost Time [s] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| g_i, Effective Green Time [s] | 2 | 8 | 8 | 4 | 33 | 1 | 31 |
| $\mathrm{g} / \mathrm{C}, \mathrm{Green} / \mathrm{Cycle}$ | 0.03 | 0.12 | 0.12 | 0.07 | 0.56 | 0.02 | 0.51 |
| ( $\mathrm{V} / \mathrm{s}$ )_i Volume / Saturation Flow Rate | 0.01 | 0.09 | 0.03 | 0.06 | 0.17 | 0.01 | 0.31 |
| s , saturation flow rate [ [veh/h] | 1627 | 1774 | 1588 | 1774 | 1860 | 1774 | 1704 |
| c, Capacity [veh/h] | 47 | 223 | 200 | 132 | 1030 | 46 | 861 |
| d1, Uniform Delay [s] | 28.83 | 25.35 | 23.73 | 27.34 | 7.20 | 28.93 | 10.70 |
| k, delay calibration | 0.11 | 0.11 | 0.11 | 0.11 | 0.50 | 0.11 | 0.50 |
| 1, Upstream Filtering Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| d2, Incremental Delay [s] | 7.61 | 4.43 | 0.60 | 7.95 | 0.74 | 6.28 | 3.27 |
| d3, Initial Queue Delay [s] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Rp, platoon ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| PF, progression factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |


| X, volume / capacity | 0.49 | 0.72 | 0.23 | 0.74 | 0.30 | 0.43 | 0.61 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d, Delay for Lane Group [s/veh] | 36.44 | 29.77 | 24.33 | 35.29 | 7.94 | 35.21 | 13.97 |
| Lane Group LOS | D | c | c | D | A | D | B |
| Critical Lane Group | Yes | Yes | No | Yes | No | No | Yes |
| 50th-Percentile Queue Length [veh] | 0.43 | 2.37 | 0.60 | 1.57 | 1.80 | 0.35 | 4.71 |
| 50th-Percentile Queue Length [t] | 10.81 | 59.18 | 15.04 | 39.36 | 45.03 | 8.68 | 117.63 |
| 95th-Percentile Queue Length [veh] | 0.78 | 4.26 | 1.08 | 2.83 | 3.24 | 0.62 | 8.26 |
| 95th-Percentile Queue Length [t]] | 19.45 | 106.52 | 27.07 | 70.85 | 81.05 | 15.62 | 206.56 |

Generated with PTV VISTRO


Volum

| Name | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2 | 4 | 25 | 252 | 2 | 65 | 45 | 316 | 7 | 15 | 264 | 171 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Righ-Turn on Red Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 2 | 4 | 25 | 252 | 2 | 65 | 45 | 316 | 7 | 15 | 264 | 171 |
| Peak Hour Factor | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 1 | 1 | 7 | 68 | 1 | 17 | 12 | 85 | 2 | 4 | 71 | 46 |
| Total Analysis Volume [veh/h] | 2 | 4 | 27 | 271 | 2 | 70 | 48 | 339 | 8 | 16 | 284 | 184 |
| Presence of On-Street Parking | No |  | No | No |  | No | No |  | No | No |  | No |
| On-Street Parking Maneuver Rate [/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Local Bus Stopping Rate [h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pedestrian Volume [ped/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |
| Bicycle Volume [bicycles/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |

Generated with PTV VISTRO
Version 5.00-00

| Lane Group | c | L | c | L | c | L | c |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| c, Cycle Length [s] | 60 | 60 | 60 | 60 | 60 | 60 | 60 |
| L. Total Lost Time per Cycle [s] | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 |
| 11_p, Permitted Start-Up Lost Time [s] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 12, Clearance Lost Time [s] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| g_i, Effective Green Time [s] | 2 | 12 | 12 | 3 | 29 | 1 | 28 |
| $\mathrm{g} / \mathrm{C}, \mathrm{Green} / \mathrm{Cycle}$ | 0.04 | 0.19 | 0.19 | 0.05 | 0.48 | 0.02 | 0.46 |
| ( $\mathrm{V} / \mathrm{s}$ )_i Volume / Saturation Flow Rate | 0.02 | 0.15 | 0.05 | 0.03 | 0.19 | 0.01 | 0.27 |
| s , saturation flow rate [ [veh/h] | 1623 | 1774 | 1590 | 1774 | 1855 | 1774 | 1742 |
| c, Capacity [veh/h] | 61 | 342 | 307 | 85 | 894 | 39 | 794 |
| d1, Uniform Delay [s] | 28.49 | 23.17 | 20.57 | 28.09 | 9.95 | 29.11 | 12.20 |
| k, delay calibration | 0.11 | 0.11 | 0.11 | 0.11 | 0.50 | 0.11 | 0.50 |
| 1, Upstream Filtering Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| d2, Incremental Delay [s] | 7.15 | 4.13 | 0.39 | 5.78 | 1.27 | 6.87 | 3.19 |
| d3, Initial Queue Delay [s] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Rp, platoon ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| PF, progression factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |


| X, volume / capacity | 0.54 | 0.79 | 0.23 | 0.57 | 0.39 | 0.41 | 0.59 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d, Delay for Lane Group [s/veh] | 35.65 | 27.30 | 20.95 | 33.88 | 11.22 | 35.98 | 15.39 |
| Lane Group LOS | D | c | c | c | B | D | B |
| Critical Lane Group | Yes | Yes | No | Yes | No | No | Yes |
| 50th-Percentile Queue Length [ven] | 0.60 | 3.79 | 0.83 | 0.77 | 2.66 | 0.29 | 4.50 |
| 50th-Percentile Queue Length [ft] | 14.93 | 94.72 | 20.84 | 19.21 | 66.55 | 7.20 | 112.58 |
| 95th-Percentile Queue Length [veh] | 1.07 | 6.82 | 1.50 | 1.38 | 4.79 | 0.52 | 7.98 |
| 955 -Percentile Queue Length [ft] | 26.87 | 170.50 | 37.52 | 34.58 | 119.79 | 12.96 | 199.59 |

## Generated with PTV VISTRO

Version 5.00-00
Control Type:
Analysis Method:

- Intersectionection Level Of Service Report

| Control Type: | Two-way stop | Delay (sec / veh): | 51.5 |
| :---: | :---: | :---: | :---: |
| Analysis Method: | HCM 2010 | Level Of Service: | F |
| Analysis Period: | 15 minutes | Volume to Capacity (v/c): | 2.319 |


| Name | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |
| Lane Configuration | + |  |  | 中 |  |  | $7 F$ |  |  | $7 F$ |  |  |
| Turning Movement | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 |
| Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 120.00 | 100.00 | 100.00 | 150.00 | 100.00 | 100.00 |
| Speed [mph] | 10.00 |  |  | 30.00 |  |  | 35.00 |  |  | 35.00 |  |  |
| Grade [\%] | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  |
| Crosswalk | No |  |  | No |  |  | No |  |  | No |  |  |

Volumes

| Name | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 3 | 2 | 24 | 226 | 1 | 74 | 148 | 404 | 3 | 26 | 394 | 435 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 3 | 2 | 24 | 226 | 1 | 74 | 148 | 404 | 3 | 26 | 394 | 435 |
| Peak Hour Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 1 | 1 | 6 | 57 | 0 | 19 | 37 | 101 | 1 | 7 | 99 | 109 |
| Total Analysis Volume [veh/h] | 3 | 2 | 24 | 226 | 1 | 74 | 148 | 404 | 3 | 26 | 394 | 435 |
| Pedestrian Volume [ped/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |

## Generated with PTV VISTRO

Version 5.00-00
Intersection Settings

| Priority Scheme | Stop | Stop | Free | Free |
| :---: | :---: | :---: | :---: | :---: |
| Flared Lane | No | Yes |  |  |
| Storage Area [veh] | 0 | 1 | 0 | 0 |
| Two-Stage Gap Acceptance | No | No |  |  |
| Number of Storage Spaces in Median | 0 | 0 | 0 | 0 |

Movement, Approach, \& Intersection Results

| V/C, Movement V/C Ratio | 0.04 | 0.02 | 0.04 | 2.32 | 0.01 | 0.15 | 0.18 | 0.00 | 0.00 | 0.02 | 0.00 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d_M, Delay for Movement [s/veh] | 49.30 | 47.83 | 11.84 | 751.48 | 745.26 | 721.84 | 10.50 | 0.00 | 0.00 | 8.20 | 0.00 | 0 |
| Movement LOS | E | E | B | F | F | F | в | A | A | A | A | A |
| 95th-Percentile Queue Length [veh] | 0.32 | 0.32 | 0.32 | 26.65 | 26.65 | 26.65 | 0.67 | 0.00 | 0.00 | 0.07 | 0.00 | 0.00 |
| 95 th-Percentile Queue Length [ft] | 7.90 | 7.90 | 7.90 | 666.25 | 666.25 | 666.25 | 16.82 | 0.00 | 0.00 | 1.73 | 0.00 | 0.00 |
| d_A, Approach Delay [s/ven] | 18.20 |  |  | 744.17 |  |  | 2.80 |  |  | 0.25 |  |  |
| Approach Los | c |  |  | F |  |  | A |  |  | A |  |  |
| d_I, Intersection Delay [s/veh] | 130.05 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS |  |  |  |  |  |  |  |  |  |  |  |  |

Generated with PTV VISTRO
Version $5.00-00$
PTV VISTRO

| Intersection Level Of Service Report Intersection 2: Todd Rd/Moorland Ave |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Control Type: | Two-way stop HCM 2010 |  | Delay (sec/veh): |  |  |  |
| Analysis Method: |  |  | Level Of Service:Volume to Capacity (v/c): |  |  |  |
| Analysis Period: | 15 minutes |  |  |  |  |  |
| Intersection Setup |  |  |  |  |  |  |
| Name | Moorland Ave |  | Todd Rd |  | Todd Rd |  |
| Approach | Southbound |  | Eastbound |  | Westbound |  |
| Lane Configuration | $7$ |  | $7$ |  | $F$ |  |
| Turning Movement | Left | Right | Left | Thru | Thru | Right |
| Lane Width [f] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Pocket | 0 | 1 | 1 | 0 | 1 | 0 |
| Pocket Length [ft] | 100.00 | 50.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| Speed [mph] | 30.00 |  | 35.00 |  | 35.00 |  |
| Grade [\%] | 0.00 |  | 0.00 |  | 0.00 |  |
| Crosswalk | No |  | No |  | No |  |

Volumes

| Name | Moorland Ave |  | Todd Rd |  | Todd Rd |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 43 | 111 | 118 | 570 | 765 | 163 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 43 | 1111 | 118 | 570 | 765 | 163 |
| Peak Hour Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 11 | 28 | 30 | 143 | 191 | 41 |
| Total Analysis Volume [veh/h] | 43 | 111 | 118 | 570 | 765 | 163 |
| Pedestrian Volume [ped/h] |  |  |  |  |  |  |

## Generated with PTV VISTRO

Version $5.00-00$

| Priority Scheme | Stop | Free | Free |
| :---: | :---: | :---: | :---: |
| Flared Lane |  |  |  |
| Storage Area [veh] | 0 | 0 | 0 |
| Two-Stage Gap Acceptance | No |  |  |
| Number of Storage Spaces in Median | 0 | 0 | 0 |

Movement, Approach, \& Intersection Results

| V/C, Movement V/C Ratio | 0.47 | 0.31 | 0.16 | 0.01 | 0.01 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d_M, Delay for Movement [s/veh] | 75.94 | 19.28 | 10.82 | 0.00 | 0.00 | 0.00 |
| Movement LOS | F | c | B | A | A | A |
| 95 th-Percentile Queue Length [veh] | 2.01 | 1.27 | 0.57 | 0.00 | 0.00 | 0.00 |
| 95 th-Percentile Queue Length [ft] | 50.35 | 31.87 | 14.20 | 0.00 | 0.00 | 0.00 |
| d_A, Approach Delay [s/ven] | 35.10 |  | 1.85 |  | 0.0 |  |
| Approach LOS | E |  | A |  | A |  |
| d_L, Intersection Delay [s/ven] | 3.78 |  |  |  |  |  |
| Intersection LOS | F |  |  |  |  |  |

## Generated with PTV VISTRO

Version 5.00-00

| Intersection Level Of Service Report Intersection 1: Todd Rd/Ghilotti Ave-Standish Ave |  |  |  |
| :---: | :---: | :---: | :---: |
| Control Type: | Two-way stop | Delay (sec / veh): | 1,426. |
| Analysis Method: | HCM 2010 | Level Of Service: | F |
| Analysis Period: | 15 minutes | Volume to Capacity | . 609 |


| Name | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |
| Lane Configuration | $\uparrow$ |  |  | 中 |  |  | $7 F$ |  |  | $7 \%$ |  |  |
| Turning Movement | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 |
| Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 120.00 | 100.00 | 100.00 | 150.00 | 100.00 | 100.00 |
| Speed [mph] | 10.00 |  |  | 30.00 |  |  | 35.00 |  |  | 35.00 |  |  |
| Grade [\%] | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  |
| Crosswalk | No |  |  | No |  |  | No |  |  | No |  |  |

Volumes

| Name | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 3 | 4 | 34 | 438 | 2 | 199 | 108 | 350 | 8 | 24 | 443 | 355 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [ven/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 3 | 4 | 34 | 438 | 2 | 199 | 108 | 350 | 8 | 24 | 443 | 355 |
| Peak Hour Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 1 | 1 | 9 | 110 | 1 | 50 | 27 | 88 | 2 | 6 | 111 | 89 |
| Total Analysis Volume [veh/h] | 3 | 4 | 34 | 438 | 2 | 199 | 108 | 350 | 8 | 24 | 443 | 355 |
| Pedestrian Volume [pedh] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |

## Generated with PTV VISTRO

Version 5.00-00

| Intersection Settings | Stop | Stop | Free | Free |
| :---: | :---: | :---: | :---: | :---: |
| Priority Scheme | No | Yes |  |  |
| Flared Lane | 0 | 1 | 0 | 0 |
| Storage Area [veh] | No | No |  |  |
| Two-Stage Gap Acceptance | 0 | 0 | 0 | 0 |
| Number of Storage Spaces in Median | 0 |  |  |  |

Movement, Approach, \& Intersection Results

| V/C, Movement V/C Ratio | 0.04 | 0.03 | 0.05 | 3.61 | 0.01 | 0.41 | 0.13 | 0.00 | 0.00 | 0.02 | 0.00 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d_M, Delay for Movement [s/ven] | 60.03 | 37.45 | 11.86 | 1426.63 | 1421.18 | 1404.35 | 10.02 | 0.00 | 0.00 | 8.06 | 0.00 | 0.00 |
| Movement LOS | F | E | B | F | F | F | B | A | A | A | A | A |
| 95th-Percentile Queue Length [veh] | 0.43 | 0.43 | 0.43 | 63.80 | 63.80 | 63.80 | 0.45 | 0.00 | 0.00 | 0.06 | 0.00 | 0.00 |
| 95 th-Percentile Queue Length [ft] | 10.87 | 10.87 | 10.87 | 1594.98 | 1594.98 | 1594.98 | 11.25 | 0.00 | 0.00 | 1.53 | 0.00 | 0.00 |
| d_A, Approach Delay [s/ven] | 17.88 |  |  | 1419.67 |  |  | 2.32 |  |  | 0.24 |  |  |
| Approach Los | c |  |  | F |  |  | A |  |  | A |  |  |
| d_I, Intersection Delay [s/ven] | 461.98 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS | F |  |  |  |  |  |  |  |  |  |  |  |

Generated with PTV VISTRO
Version 5.00-00
PTV VISTRO

| Intersection Level Of Service Report Intersection 2: Todd Rd/Moorland Ave |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Control Type: | Two-way stop HCM 2010 |  | Delay (sec / veh): |  |  |  |
| Analysis Method: |  |  |  | Of Se |  |  |
| Analysis Period: | 15 minutes |  | Volume to Capacity (v/c): |  |  |  |
| Intersection Setup |  |  |  |  |  |  |
| Name | Moorland Ave |  | Todd Rd |  | Todd Rd |  |
| Approach | Southbound |  | Eastbound |  | Westbound |  |
| Lane Configuration | 75 |  | $7$ |  | $F$ |  |
| Turning Movement | Left | Right | Left | Thru | Thru | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Pocket | 0 | 1 | 1 | 0 | 1 | 0 |
| Pocket Length [ft] | 100.00 | 50.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| Speed [mph] | 30.00 |  | 35.00 |  | 35.00 |  |
| Grade [\%] | 0.00 |  | 0.00 |  | 0.00 |  |
| Crosswalk | No |  | No |  | No |  |

Volumes

| Name | Moorland Ave |  | Todd Rd |  | Todd Rd |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 96 | 186 | 139 | 739 | 647 | 89 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 96 | 186 | 139 | 739 | 647 | 89 |
| Peak Hour Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 24 | 47 | 35 | 185 | 162 | 22 |
| Total Analysis Volume [veh/h] | 96 | 186 | 139 | 739 | 647 | 89 |
| Pedestrian Volume [pedh] |  |  |  |  |  |  |

## Generated with PTV VISTRO

| Intersection Level Of Service Report Intersection 1: Todd Rd/Ghilotti Ave-Standish Ave |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Control Type: | Signalized HCM 2010 |  |  |  |  | Delay (sec / veh): |  |  |  | 30.1$c$ |  |  |
| Analysis Method: |  |  |  |  |  |  | Level Of | Service: |  |  |  |  |
| Analysis Period: | HCM 2010 15 minutes |  |  |  |  | Volume to Capacity (v/c): |  |  |  | 0.825 |  |  |
| Intersection Setup |  |  |  |  |  |  |  |  |  |  |  |  |
| Name | Ghiloti Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| Approach | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |
| Lane Configuration | 中 |  |  | $7 \mathrm{~F}$ |  |  | $7 \mathrm{~F}$ |  |  | $7 \mathrm{~F}$ |  |  |
| Turning Movement | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Pocket | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 |
| Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 120.00 | 100.00 | 100.00 | 150.00 | 100.00 | 100.00 |
| Speed [mph] |  | 10.00 |  |  | 30.00 |  |  | 35.00 |  |  | 35.00 |  |
| Grade [\%] |  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |
| Crosswalk |  | No |  |  | No |  |  | No |  |  | No |  |


| Name | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 3 | 2 | 24 | 226 | 1 | 74 | 148 | 404 | 3 | 26 | 394 | 435 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Right-Turn on Red Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 3 | 2 | 24 | 226 | 1 | 74 | 148 | 404 | 3 | 26 | 394 | 435 |
| Peak Hour Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 1 | 1 | 6 | 57 | 0 | 19 | 37 | 101 | 1 | 7 | 99 | 109 |
| Total Analysis Volume [veh/h] | 3 | 2 | 24 | 226 | 1 | 74 | 148 | 404 | 3 | 26 | 394 | 435 |
| Presence of On-Street Parking | No |  | No | No |  | No | No |  | No | No |  | No |
| On-Street Parking Maneuver Rate [/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Local Bus Stopping Rate [h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pedestrian Volume [ped/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |
| Bicycle Volume [bicyclesh] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |

Generated with PTV VISTRO

## Intersection Settings

| Located in CBD | No |
| :---: | :---: |
| Signal Coordination Group |  |
| Cycle Length [s] | 90 |
| Coordination Type | Time of Day Pattern Isolated |
| Actuation Type | Fully actuated |
| Offset $[s]$ | 0.0 |
| Offset Reference | LeadGreen |
| Permissive Mode | SingleBand |
| Lost time $[s]$ | 12.00 |

Phasing \& Timing


Ghilotti Construction Yard TIS
AM Future (Signal)

## Generated with PTV VISTRO

Version 5.00-00

| Lane Group | c | L | c | L | c | L | c |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| c, Cycle Length [s] | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| L, Total Lost Time per Cycle [s] | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 |
| 11_p, Permitted Start-Up Lost Time [s] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 12, Clearance Lost Time [s] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| g_i, Effective Green Time [s] | 3 | 13 | 13 | 9 | 56 | 2 | 49 |
| $\mathrm{g} / \mathrm{C}, \mathrm{Green}$ / Cycle | 0.03 | 0.15 | 0.15 | 0.10 | 0.62 | 0.03 | 0.55 |
| ( $\mathrm{V} / \mathrm{s}$ ) i Volume / Saturation Flow Rate | 0.02 | 0.13 | 0.05 | 0.08 | 0.22 | 0.01 | 0.49 |
| s , saturation flow rate [ [veh/h] | 1618 | 1774 | 1587 | 1774 | 1860 | 1774 | 1705 |
| c, Capacity [veh/h] | 47 | 259 | 231 | 180 | 1155 | 47 | 931 |
| d1, Uniform Delay [s] | 43.23 | 37.64 | 34.47 | 39.63 | 8.28 | 43.27 | 18.06 |
| k, delay calibration | 0.11 | 0.11 | 0.11 | 0.11 | 0.50 | 0.11 | 0.50 |
| I, Upstream Fillering Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| d2, Incremental Delay [s] | 12.73 | 8.98 | 0.80 | 8.91 | 0.85 | 9.50 | 12.55 |
| d3, Initial Queue Delay [s] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Rp, platoon ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| PF, progression factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |


| X, volume / capacity | 0.62 | 0.87 | 0.32 | 0.82 | 0.35 | 0.55 | 0.89 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d, Delay for Lane Group [s/veh] | 55.96 | 46.61 | 35.27 | 48.54 | 9.13 | 52.77 | 30.60 |
| Lane Group LOS | E | D | D | D | A | D | c |
| Critical Lane Group | Yes | Yes | No | Yes | No | No | Yes |
| 50th-Percentile Queue Length [veh] | 0.82 | 5.43 | 1.50 | 3.57 | 3.60 | 0.69 | 16.56 |
| 50th-Percentile Queue Length [tt] | 20.59 | 135.63 | 37.62 | 89.28 | 89.88 | 17.13 | 414.01 |
| 95th-Percentile Queue Length [veh] | 1.48 | 9.25 | 2.71 | 6.43 | 6.47 | 1.23 | 23.23 |
|  | 37.06 | 231.13 | 67.71 | 160.70 | 161.79 | 30.84 | 580.85 |

## Generated with PTV VISTRO

$\frac{\text { Version } 5.00-00}{\text { Movement, Approach, \& Intersection Results }}$

| d_M, Delay for Movement [s/ven] | 55.96 | 55.96 | 55.96 | 46.61 | 35.27 | 35.27 | 48.54 | 9.13 | 9.13 | 52.77 | 30.60 | 30.60 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement LOS | E | E | E | D | D | D | D | A | A | D | c | c |
| d_A, Approach Delay [s/ven] | 55.96 |  |  | 43.79 |  |  | 19.64 |  |  | 31.28 |  |  |
| Approach Los | E |  |  | D |  |  | B |  |  | c |  |  |
| d_l, Intersection Delay [s/ven] | 30.14 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS | c |  |  |  |  |  |  |  |  |  |  |  |
| Intersection V/C | 0.825 |  |  |  |  |  |  |  |  |  |  |  |

Sequence


## Generated with PTV VISTRO

| Intersection Level Of Service Report Intersection 1: Todd Rd/Ghilotti Ave-Standish Ave |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Control Type: | Signalized HCM 2010 |  |  |  |  | Delay (sec / veh): |  |  |  | 38.2D |  |  |
| Analysis Method: |  |  |  |  |  |  | Level Of | Service: |  |  |  |  |
| Analysis Period: | HCM 2010 15 minutes |  |  |  |  | Volume to Capacity (v/c): |  |  |  | 0.908 |  |  |
| Intersection Setup |  |  |  |  |  |  |  |  |  |  |  |  |
| Name | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| Approach | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |
| Lane Configuration | 中 |  |  | $7 \mathrm{~F}$ |  |  | $7 \mathrm{~F}$ |  |  | $7 \mathrm{~F}$ |  |  |
| Turning Movement | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Pocket | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 |
| Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 120.00 | 100.00 | 100.00 | 150.00 | 100.00 | 100.00 |
| Speed [mph] |  | 10.00 |  |  | 30.00 |  |  | 35.00 |  |  | 35.00 |  |
| Grade [\%] |  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |
| Crosswalk |  | No |  |  | No |  |  | No |  |  | No |  |

Volum

| Name | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 3 | 4 | 34 | 438 | 2 | 199 | 108 | 350 | 8 | 24 | 443 | 355 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Right-Turn on Red Volume [veh/h] | 0 | 0 | 11 | 0 | 0 | 66 | 0 | 0 | 3 | 0 | 0 | 66 |
| Total Hourly Volume [veh/h] | 3 | 4 | ${ }^{23}$ | 438 | 2 | 133 | 108 | 350 | 5 | 24 | 443 | 289 |
| Peak Hour Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 1 | 1 | 6 | 110 | 1 | 33 | 27 | 88 | 1 | 6 | 111 | 72 |
| Total Analysis Volume [veh/h] | 3 | 4 | 23 | 438 | 2 | ${ }^{133}$ | 108 | 350 | 5 | 24 | 443 | 289 |
| Presence of On-Street Parking | No |  | No | No |  | No | No |  | No | No |  | No |
| On-Street Parking Maneuver Rate [/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Local Bus Stopping Rate [h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pedestrian Volume [ped/h] |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Bicycle Volume [bicycles/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |

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Version $5.00-00$

| Lane Group | c | L | c | L | c | L | c |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| c, Cycle Length [s] | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| L, Total Lost Time per Cycle [s] | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 |
| 11_p, Permitted Start-Up Lost Time [s] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 12, Clearance Lost Time [s] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| g_i, Effective Green Time [s] | 3 | 24 | 24 | 6 | 45 | 2 | 41 |
| $\mathrm{g} / \mathrm{C}, \mathrm{Green}$ / Cycle | 0.03 | 0.27 | 0.27 | 0.07 | 0.50 | 0.03 | 0.45 |
| ( $\mathrm{V} / \mathrm{s}$ ) i Volume / Saturation Flow Rate | 0.02 | 0.25 | 0.09 | 0.06 | 0.19 | 0.01 | 0.42 |
| s , saturation flow rate [ [veh/h] | 1634 | 1774 | 1587 | 1774 | 1858 | 1774 | 1741 |
| c, Capacity [veh/h] | 48 | 472 | 423 | 129 | 932 | 45 | 790 |
| d1, Uniform Delay [s] | 43.19 | 32.17 | 26.48 | 41.18 | 13.82 | 43.36 | 23.18 |
| k, delay calibration | 0.11 | 0.26 | 0.11 | 0.11 | 0.50 | 0.11 | 0.50 |
| I, Upstream Fillering Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| d2, Incremental Delay [s] | 12.60 | 16.74 | 0.43 | 12.89 | 1.18 | 9.73 | 18.46 |
| d3, Initial Queue Delay [s] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Rp, platoon ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| PF, progression factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |


| X, volume / capacity | 0.63 | 0.93 | 0.32 | 0.83 | 0.38 | 0.54 | 0.93 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d, Delay for Lane Group [s/veh] | 55.79 | 48.91 | 26.91 | 54.07 | 15.01 | 53.09 | 41.63 |
| Lane Group LOS | E | D | c | D | B | D | D |
| Critical Lane Group | Yes | Yes | No | Yes | No | No | Yes |
| 50th-Percentile Queue Length [veh] | 0.85 | 11.19 | 2.33 | 2.77 | 4.41 | 0.64 | 17.35 |
| 50th-Percentile Queue Length [ft] | 21.22 | 279.64 | 58.28 | 69.35 | 110.30 | 15.94 | 433.63 |
| 95th-Percentile Queue Length [veh] | 1.53 | 16.67 | 4.20 | 4.99 | 7.86 | 1.15 | 24.18 |
|  | 38.20 | 416.77 | 104.90 | 124.83 | 196.42 | 28.70 | 604.39 |

## Generated with PTV VISTRO

Version $5.00-00$
Movement, Approach, \& Intersection Results

| d_M, Delay for Movement [s/veh] | 55.79 | 55.79 | 55.79 | 48.91 | 26.91 | 26.91 | 54.07 | 15.01 | 15.01 | 53.09 | 41.63 | 41.63 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement LOS | E | E | E | D | c | c | D | в | в | D | D | D |
| d_A, Approach Delay [s/veh] | 55.79 |  |  | 43.73 |  |  | 24.12 |  |  | 42.00 |  |  |
| Approach LOS | E |  |  | D |  |  | c |  |  | D |  |  |
| d_L, Intersection Delay [s/veh] | 38.23 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS | D |  |  |  |  |  |  |  |  |  |  |  |
| Intersection V/C | 0.908 |  |  |  |  |  |  |  |  |  |  |  |



## Generated with PTV VISTRO

Version 5.00-00
Control Type:
Analysis Method:

| Intersection Level Of Service Report |  |  |
| :---: | :---: | :---: |
| Intersection 1: Todd Rd/Ghilotti Ave-Standish Ave |  |  |
| Delay (sec / ven): |  |  |
| Two-way stop | Level f Service: | 116.9 |
| HCM 2010 | Volume to Capacity (V/c): | F |
| 15 minutes |  | 0.947 |

Intersection Setup

| Name | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |
| Lane Configuration | 中 |  |  | 中 |  |  | $7$ |  |  | $7 \mathrm{~F}$ |  |  |
| Turning Movement | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 |
| Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 120.00 | 100.00 | 100.00 | 150.00 | 100.00 | 100.00 |
| Speed [mph] | 10.00 |  |  | 30.00 |  |  | 35.00 |  |  | 35.00 |  |  |
| Grade [\%] | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  |
| Crosswalk | No |  |  | No |  |  | No |  |  | No |  |  |

Volumes

| Name | ti Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2 | 2 | 10 | 150 | 1 | 43 | 91 | 283 | 2 | 12 | 232 | 259 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 2 | 0 | 43 | 0 | 0 | 0 | 0 | 0 | 2 | 42 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 4 | 2 | 53 | 150 | 1 | 43 | 91 | 283 | 4 | 54 | 232 | 259 |
| Peak Hour Factor | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 1 | 1 | 14 | 40 | 0 | 12 | 25 | 76 | 1 | 15 | 63 | 70 |
| Total Analysis Volume [veh/h] | 4 | 2 | 57 | 162 | 1 | 46 | 98 | 305 | 4 | 58 | 250 | 279 |
| Pedestrian Volume [ped/h] |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |

## Generated with PTV VISTRO

Version 5.00-00

| Intersection Settings | Stop | Stop | Free | Free |
| :---: | :---: | :---: | :---: | :---: |
| Priority Scheme | No | Yes |  |  |
| Flared Lane | 0 | 1 | 0 | 0 |
| Storage Area [ven] | No | No |  |  |
| Two-Stage Gap Acceptance | 0 | 0 | 0 | 0 |
| Number of Storage Spaces in Median | 0 |  | 0 |  |

Movement, Approach, \& Intersection Results

| V/C, Movement V/C Ratio | 0.02 | 0.01 | 0.08 | 0.95 | 0.00 | 0.07 | 0.09 | 0.00 | 0.00 | 0.05 | 0.00 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d_M, Delay for Movement [s/veh] | 26.37 | 26.79 | 10.72 | 116.91 | 113.27 | 101.34 | 8.83 | 0.00 | 0.00 | 8.02 | 0.00 | 0.00 |
| Movement LOS | D | D | в | F | F | F | A | A | A | A | A | A |
| 95th-Percentile Queue Length [veh] | 0.38 | 0.38 | 0.38 | 8.97 | 8.97 | 8.97 | 0.31 | 0.00 | 0.00 | 0.15 | 0.00 | 0.00 |
| 95th-Percentile Queue Length [ft] | 9.43 | 9.43 | 9.43 | 224.25 | 224.25 | 224.25 | 7.80 | 0.00 | 0.00 | 3.64 | 0.00 | 0.00 |
| d_A, Approach Delay [s/ven] | 12.22 |  |  | 113.47 |  |  | 2.13 |  |  | 0.79 |  |  |
| Approach Los | B |  |  | F |  |  | A |  |  | A |  |  |
| d_I, Intersection Delay [s/veh] | 20.39 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS |  |  |  |  |  |  |  |  |  |  |  |  |

Generated with PTV VISTRO
Version 5.00-00
PTV VISTRO

| Intersection Level Of Service Report Intersection 2: Todd Rd/Moorland Ave |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Control Type: | Two-way stop HCM 2010 |  | Delay (sec/ veh): |  |  |  |
| Analysis Method: |  |  | Level Of Service:Volume to Capacity (v/c): |  |  |  |
| Analysis Period: | 15 minutes |  |  |  |  |  |
| Intersection Setup |  |  |  |  |  |  |
| Name | Moorland Ave |  | Todd Rd |  | Todd Rd |  |
| Approach | Southbound |  | Eastbound |  | Westbound |  |
| Lane Configuration | 75 |  | $7$ |  | $F$ |  |
| Turning Movement | Left | Right | Left | Thru | Thru | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Pocket | 0 | 1 | 1 | 0 | 1 | 0 |
| Pocket Length [ft] | 100.00 | 50.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| Speed [mph] | 30.00 |  | 35.00 |  | 35.00 |  |
| Grade [\%] | 0.00 |  | 0.00 |  | 0.00 |  |
| Crosswalk | No |  | No |  | No |  |

## Volume

| Name | Moorland Ave |  | Todd Rd |  | Todd Rd |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 124 | 30 | 12 | 475 | 494 | 143 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 2 | 2 | 41 | 40 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 124 | 32 | 14 | 516 | 534 | 143 |
| Peak Hour Factor | 0.9000 | 0.9000 | 0.9000 | 0.9000 | 0.9000 | 0.9000 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 34 | 9 | 4 | 143 | 148 | 40 |
| Total Analysis Volume [veh/h] | 138 | 36 | 16 | 573 | 593 | 159 |
| Pedestrian Volume [pedh] |  |  |  |  |  |  |

## Generated with PTV VISTRO

Intersection Settings

| Priority Scheme | Stop | Free | Free |
| :---: | :---: | :---: | :---: |
| Flared Lane |  |  |  |
| Storage Area [veh] | 0 | 0 | 0 |
| Two-Stage Gap Acceptance | No |  |  |
| Number of Storage Spaces in Median | 0 | 0 | 0 |

Movement, Approach, \& Intersection Results

| V/C, Movement V/C Ratio | 0.77 | 0.08 | 0.02 | 0.01 | 0.01 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d_M, Delay for Movement [s/veh] | 70.62 | 13.58 | 9.28 | 0.00 | 0.00 | 0.00 |
| Movement LOS | F | B | A | A | A | A |
| 95 th-Percentile Queue Length [veh] | 5.03 | 0.26 | 0.06 | 0.00 | 0.00 | 0.00 |
| 95 th-Percentile Queue Length [ft] | 125.66 | 6.41 | 1.43 | 0.00 | 0.00 | 0.00 |
| d_A, Approach Delay [s/ven] | 58.82 |  | 0.25 |  | 0.00 |  |
| Approach LOS | F |  | A |  | A |  |
| d_I, Intersection Delay [s/veh] | 6.85 |  |  |  |  |  |
| Intersection LOS | F |  |  |  |  |  |

## Generated with PTV VISTRO

Version 5.00-00
Control Type:
Analysis Method

$$
\begin{aligned}
& \text { Analysis Method: } \\
& \text { Analysis Period: }
\end{aligned}
$$

\[

\]

| Name | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |
| Lane Configuration | $+$ |  |  | 中 |  |  | $7 \mathrm{~F}$ |  |  | $7$ |  |  |
| Turning Movement | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 |
| Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 120.00 | 100.00 | 100.00 | 150.00 | 100.00 | 100.00 |
| Speed [mph] | 10.00 |  |  | 30.00 |  |  | 35.00 |  |  | 35.00 |  |  |
| Grade [\%] | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  |
| Crosswalk | No |  |  | No |  |  | No |  |  | No |  |  |

Volumes

| Name | Ghiotti Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 2 | 4 | 20 | 252 | 2 | 65 | 45 | 316 | 7 | 10 | 264 | 171 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [ven/h] | 2 | 0 | 43 | 0 | 0 | 0 | 0 | 0 | 2 | 42 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 4 | 4 | 63 | 252 | 2 | 65 | 45 | 316 | 9 | 52 | 264 | 171 |
| Peak Hour Factor | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 1 | 1 | 17 | 68 | 1 | 17 | 12 | 85 | 2 | 14 | 71 | 46 |
| Total Analysis Volume [veh/h] | 4 | 4 | 68 | 271 | , | 70 | 48 | 339 | 10 | 56 | 284 | 184 |
| Pedestrian Volume [ped/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |

## Generated with PTV VISTRO

Version 5.00-00
Intersection Settings

| Priority Scheme | Stop | Stop | Free | Free |
| :---: | :---: | :---: | :---: | :---: |
| Flared Lane | No | Yes |  |  |
| Storage Area [veh] | 0 | 1 | 0 | 0 |
| Two-Stage Gap Acceptance | No | No |  |  |
| Number of Storage Spaces in Median | 0 | 0 | 0 | 0 |

Movement, Approach, \& Intersection Results

| V/C, Movement V/C Ratio | 0.02 | 0.02 | 0.10 | 1.39 | 0.01 | 0.10 | 0.04 | 0.00 | 0.00 | 0.05 | 0.00 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d_M, Delay for Movement [s/veh] | 24.49 | 22.70 | 11.17 | 287.60 | 283.96 | 274.49 | 8.44 | 0.00 | 0.00 | 8.12 | 0.00 | , 0 |
| Movement LOS | c | c | B | F | F | F | A | A | A | A | A | A |
| 95th-Percentile Queue Length [veh] | 0.47 | 0.47 | 0.47 | 20.52 | 20.52 | 20.52 | 0.14 | 0.00 | 0.00 | 0.15 | 0.00 | 0.00 |
| 95 th-Percentile Queue Length [ft] | 11.75 | 11.75 | 11.75 | 512.96 | 512.96 | 512.96 | 3.44 | 0.00 | 0.00 | 3.64 | 0.00 | 0.00 |
| d_A, Approach Delay [s/ven] | 12.48 |  |  | 284.90 |  |  | 1.02 |  |  | 0.87 |  |  |
| Approach Los | B |  |  | F |  |  | A |  |  | A |  |  |
| d_I, Intersection Delay [s/veh] | 74.28 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS |  |  |  |  |  |  |  |  |  |  |  |  |

hilotti Construction Ya

PM Existing + Project

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## Volume

| Name | Moorland Ave |  | Todd Rd |  | Todd Rd |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 142 | 30 | 40 | 606 | 428 | 189 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 2 | 2 | 41 | 40 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 142 | 32 | 42 | 647 | 468 | 189 |
| Peak Hour Factor | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 38 | 9 | 11 | 172 | 124 | 50 |
| Total Analysis Volume [veh/h] | 151 | 34 | 45 | 688 | 498 | 201 |
| Pedestrian Volume [ped/h] |  | 0 |  |  |  | 0 |

## Generated with PTV VISTRO

Intersection Settings

| Priority Scheme | Stop | Free | Free |
| :---: | :---: | :---: | :---: |
| Flared Lane |  |  |  |
| Storage Area [veh] | 0 | 0 | 0 |
| Two-Stage Gap Acceptance | No | 0 |  |
| Number of Storage Spaces in Median | 0 | 0 | 0 |

Movement, Approach, \& Intersection Results

| V/C, Movement V/C Ratio | 0.99 | 0.07 | 0.05 | 0.01 | 0.00 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d_M, Delay for Movement [s/veh] | 130.49 | 12.69 | 9.22 | 0.00 | 0.00 | 00 |
| Movement LOS | F | B | A | A | A | A |
| 95 th-Percentile Queue Length [veh] | 7.47 | 0.22 | 0.16 | 0.00 | 0.00 | 0.00 |
| 95 th-Percentile Queue Length [ft] | 186.82 | 5.43 | 3.95 | 0.00 | 0.00 | 0.00 |
| d_A, Approach Delay [s/ven] | 108.84 |  | 0.57 |  | 0.00 |  |
| Approach Los | F |  | A |  | A |  |
| d_I, Intersection Delay [s/veh] | 12.71 |  |  |  |  |  |
| Intersection LOS | F |  |  |  |  |  |

## Generated with PTV VISTRO

| Intersection Level Of Service Report Intersection 1: Todd Rd/Ghilotti Ave-Standish Ave |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Control Type: | Signalized HCM 2010 |  |  |  |  | Delay (sec / veh): |  |  |  | 20.0$B$ |  |  |
| Analysis Method: |  |  |  |  |  |  | Level Of | Service: |  |  |  |  |
| Analysis Period: | HCM 2010 15 minutes |  |  |  |  | Volume to Capacity (v/c): |  |  |  | 0.620 |  |  |
| Intersection Setup |  |  |  |  |  |  |  |  |  |  |  |  |
| Name | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| Approach | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |
| Lane Configuration | 中 |  |  | $7 \mathrm{~F}$ |  |  | $7 \mathrm{~F}$ |  |  | $7 \mathrm{~F}$ |  |  |
| Turning Movement | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Pocket | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 |
| Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 120.00 | 100.00 | 100.00 | 150.00 | 100.00 | 100.00 |
| Speed [mph] |  | 10.00 |  |  | 30.00 |  |  | 35.00 |  |  | 35.00 |  |
| Grade [\%] |  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |
| Crosswalk |  | No |  |  | No |  |  | No |  |  | No |  |


| Name | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 2 | 2 | 10 | 150 | 1 | 43 | 91 | 283 | 2 | 12 | 232 | 259 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| in-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [ven/h] | 2 | 0 | 43 | 0 | 0 | 0 | 0 | 0 | 2 | 42 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Right-Turn on Red Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 4 | 2 | 53 | 150 | 1 | 43 | 91 | 283 | 4 | 54 | 232 | 259 |
| Peak Hour Factor | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 1 | 1 | 14 | 40 | 0 | 12 | 25 | 76 | 1 | 15 | 63 | 70 |
| Total Analysis Volume [veh/h] | 4 | 2 | 57 | 162 | 1 | 46 | 98 | 305 | 4 | 58 | 250 | 279 |
| Presence of On-Street Parking | No |  | No | No |  | No | No |  | No | No |  | No |
| On-Street Parking Maneuver Rate [/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Local Bus Stopping Rate [ h$]$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pedestrian Volume [ped/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |
| Bicycle Volume [bicycles/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |

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Version 5.00-00

| Lane Group | c | L | c | L | c | L | c |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| c, Cycle Length [s] | 60 | 60 | 60 | 60 | 60 | 60 | 60 |
| L, Total Lost Time per Cycle [s] | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 |
| 11_p, Permitted Start-Up Lost Time [s] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 12, Clearance Lost Time [s] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| g_i, Effective Green Time [s] | 3 | 7 | 7 | 4 | 30 | 3 | 29 |
| $\mathrm{g} / \mathrm{C}, \mathrm{Green}$ / Cycle | 0.06 | 0.12 | 0.12 | 0.07 | 0.50 | 0.05 | 0.48 |
| ( $\mathrm{V} / \mathrm{s}$ )_i Volume / Saturation Flow Rate | 0.04 | 0.09 | 0.03 | 0.06 | 0.17 | 0.03 | 0.31 |
| s , saturation flow rate [ [veh/h] | 1602 | 1774 | 1588 | 1774 | 1858 | 1774 | 1704 |
| c, Capacity [veh/h] | 91 | 223 | 199 | 132 | 926 | 96 | 815 |
| d1, Uniform Delay [s] | 27.93 | 25.37 | 23.76 | 27.35 | 9.10 | 27.89 | 11.90 |
| k, delay calibration | 0.11 | 0.11 | 0.11 | 0.11 | 0.50 | 0.11 | 0.50 |
| I, Upstream Fillering Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| d2, Incremental Delay [s] | 9.12 | 4.50 | 0.60 | 8.02 | 0.97 | 5.99 | 3.99 |
| d3, Initial Queue Delay [s] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Rp, platoon ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| PF, progression factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |


| X, volume / capacity | 0.69 | 0.73 | 0.24 | 0.74 | 0.33 | 0.60 | 0.65 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d, Delay for Lane Group [s/veh] | 37.05 | 29.87 | 24.36 | 35.36 | 10.07 | 33.87 | 15.89 |
| Lane Group LOS | D | C | c | D | B | C | B |
| Critical Lane Group | Yes | Yes | No | Yes | No | No | Yes |
| 50th-Percentile Queue Length [veh] | 1.13 | 2.37 | 0.60 | 1.58 | 2.19 | 0.92 | 5.17 |
| 50th-Percentile Queue Length [ft] | 28.37 | 59.29 | 15.05 | 39.42 | 54.67 | 23.05 | ${ }^{129.34}$ |
| 95th-Percentile Queue Length [veh] | 2.04 | 4.27 | 1.08 | 2.84 | 3.94 | 1.66 | 8.90 |
| 95th-Percentile Queue Length [ft] | 51.06 | 106.72 | 27.09 | 70.95 | 98.41 | 41.48 | 222.59 |

## Generated with PTV VISTRO



| Name | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 2 | 4 | 20 | 252 | 2 | 65 | 45 | 316 | 7 | 10 | 264 | 171 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 2 | 0 | 43 | 0 | 0 | 0 | 0 | 0 | 2 | 42 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Right-Turn on Red Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 4 | 4 | 63 | 252 | 2 | 65 | 45 | 316 | 9 | 52 | 264 | 171 |
| Peak Hour Factor | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 1 | 1 | 17 | 68 | 1 | 17 | 12 | 85 | 2 | 14 | 71 | 46 |
| Total Analysis Volume [veh/h] | 4 | 4 | 68 | 271 | 2 | 70 | 48 | 339 | 10 | 56 | 284 | 184 |
| Presence of On-Street Parking | No |  | No | No |  | No | No |  | No | No |  | No |
| On-Stret Parking Maneuver Rate [/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Local Bus Stopping Rate [h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pedestrian Volume [ped/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |
| Bicycle Volume [bicycles/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |

Generated with PTV VISTRO

## Intersection Settings

| Located in CBD | No |
| :---: | :---: |
| Signal Coordination Group |  |
| Cycle Length [s] | 60 |
| Coordination Type | Time of Day Pattern Isolated |
| Actuation Type | Fully actuated |
| Offset $[s]$ | 0.0 |
| Offset Reference | LeadGreen |
| Permissive Mode | SingleBand |
| Lost time $[s]$ | 16.00 |

## Phasing \& Timing

| Control Type | Split | Split | Split | Split | Split | Split | Protecte | Permiss | Permiss | Protecte | Permiss | Permiss |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Signal group | 0 | 2 | 0 | 0 | 6 | 0 | 3 | 8 | 0 | 7 | 4 | 0 |
| Auxiliary Signal Groups |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead/Lag | - | - | - | - | - | - | Lead | - | - | Lead | . | . |
| Minimum Green [s] | 0 | 5 | 0 | 0 | 5 | 0 | 5 | 5 | 0 | 5 | 5 | 0 |
| Maximum Green [s] | 0 | 30 | 0 | 0 | 30 | 0 | 30 | 30 | 0 | 30 | 30 | 0 |
| Amber [s] | 0.0 | 3.0 | 0.0 | 0.0 | 3.0 | 0.0 | 3.0 | 3.0 | 0.0 | 3.0 | 3.0 | 0.0 |
| All red [s] | 0.0 | 1.0 | 0.0 | 0.0 | 1.0 | 0.0 | 1.0 | 1.0 | 0.0 | 1.0 | 1.0 | 0.0 |
| Split [s] | 0 | 9 | 0 | 0 | 26 | 0 | 9 | 16 | 0 | 9 | 16 | 0 |
| Vehicle Extension [s] | 0.0 | 3.0 | 0.0 | 0.0 | 3.0 | 0.0 | 3.0 | 3.0 | 0.0 | 3.0 | 3.0 | 0.0 |
| Walk [s] | 0 | 5 | 0 | 0 | 5 | 0 | 0 | 5 | 0 | 0 | 5 | 0 |
| Pedestrian Clearance [s] | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 10 | 0 |
| Rest In Walk |  | No |  |  | No |  |  | No |  |  | No |  |
| 11, Start-Up Lost Time [s] | 0.0 | 2.0 | 0.0 | 0.0 | 2.0 | 0.0 | 2.0 | 2.0 | 0.0 | 2.0 | 2.0 | 0.0 |
| 12, Clearance Lost Time [s] | 0.0 | 2.0 | 0.0 | 0.0 | 2.0 | 0.0 | 2.0 | 2.0 | 0.0 | 2.0 | 2.0 | 0.0 |
| Minimum Recall |  | No |  |  | No |  | No | No |  | No | No |  |
| Maximum Recall |  | No |  |  | No |  | No | No |  | No | No |  |
| Pedestrian Recall |  | No |  |  | No |  | No | No |  | No | No |  |
| Detector Location [ft] | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector Length [ft] | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | ${ }^{0.0}$ | ${ }^{0.0}$ |
| I, Upstream Filtering Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Exclusive Pedestrian Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Pedestrian Signal Group |  |  |  |  |  |  | 0 |  |  |  |  |  |
| Pedestrian Walk [s] |  |  |  |  |  |  | 0 |  |  |  |  |  |
| Pedestrian Clearance [s] |  |  |  |  |  |  | 0 |  |  |  |  |  |

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Version 5.00-00

| Lane Group | c | L | c | L | c | L | c |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| c, Cycle Length [s] | 60 | 60 | 60 | 60 | 60 | 60 | 60 |
| L, Total Lost Time per Cycle [s] | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 |
| 11_p, Permitted Start-Up Lost Time [s] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 12, Clearance Lost Time [s] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| g_i, Effective Green Time [s] | 4 | 11 | 11 | 3 | 26 | 3 | 26 |
| $\mathrm{g} / \mathrm{C}, \mathrm{Green}$ / Cycle | 0.06 | 0.19 | 0.19 | 0.05 | 0.43 | 0.05 | 0.44 |
| ( $\mathrm{V} / \mathrm{s}$ ) i Volume / Saturation Flow Rate | 0.05 | 0.15 | 0.05 | 0.03 | 0.19 | 0.03 | 0.27 |
| s , saturation flow rate [ [veh/h] | 1605 | 1774 | 1590 | 1774 | 1853 | 1774 | 1742 |
| c, Capacity [veh/h] | 98 | 340 | 304 | 83 | 796 | 92 | 757 |
| d1, Uniform Delay [s] | 27.82 | 23.21 | 20.59 | 28.08 | 12.06 | 27.92 | 13.15 |
| k, delay calibration | 0.11 | 0.11 | 0.11 | 0.11 | 0.50 | 0.11 | 0.50 |
| I, Upstream Fillering Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| d2, Incremental Delay [s] | 12.10 | 4.31 | 0.40 | 6.17 | 1.75 | 6.34 | 3.77 |
| d3, Initial Queue Delay [s] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Rp, platoon ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| PF, progression factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |


| X, volume / capacity | 0.77 | 0.80 | 0.24 | 0.58 | 0.44 | 0.61 | 0.62 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d, Delay for Lane Group [s/veh] | 39.92 | 27.52 | 20.99 | 34.25 | 13.82 | 34.25 | 16.93 |
| Lane Group LOS | D | c | c | c | B | c | B |
| Critical Lane Group | Yes | Yes | No | Yes | No | No | Yes |
| 50th-Percentile Queue Length [veh] | 1.42 | 3.80 | 0.83 | 0.77 | 3.13 | 0.90 | 4.83 |
| 50th-Percentile Queue Length [t]] | 35.56 | 95.08 | 20.85 | 19.36 | 78.32 | 22.44 | 120.68 |
| 95th-Percentile Queue Length [veh] | 2.56 | 6.85 | 1.50 | 1.39 | 5.64 | 1.62 | 8.43 |
| 95th-Percentile Queue Length [tt] | 64.01 | 171.15 | 37.54 | 34.84 | 140.98 | 40.39 | 210.77 |

Generated with PTV VISTRO
Version 5.00-00
Tiv VISTRO

| Intersection Level Of Service Report |  |  |  |
| :---: | :---: | :---: | :---: |
| Control Type: | Intersection 1: Todd Rel/Ghilotti Ave-Standish Ave |  |  |
| Analysis Method: | Two-way sec / veh): | 135.9 |  |
| Analysis Period: | HCM 2010 | Level Of Service: | F |
|  | 15 minutes | Volume to Capacity (v/c): | 0.998 |

Intersection Setup

| Name | Ghiloti Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |
| Lane Configuration | + |  |  | + |  |  | $7 \mathrm{~F}$ |  |  | $7 \mathrm{~F}$ |  |  |
| Turning Movement | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [t] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 |
| Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 120.00 | 100.00 | 100.00 | 150.00 | 100.00 | 100.00 |
| Speed [mph] | 10.00 |  |  | 30.00 |  |  | 35.00 |  |  | 35.00 |  |  |
| Grade [\%] | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  |
| Crosswalk | No |  |  | No |  |  | No |  |  | No |  |  |

Volumes

| $\begin{gathered} \hline \text { Name } \\ \hline \text { Base Volume Input [veh/h] } \end{gathered}$ | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 3 | 2 | 17 | 150 | 1 | 43 | 91 | 283 | 3 | 19 | 232 | 259 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 2 | 0 | 43 | 0 | 0 | 0 | 0 | 0 | 2 | 43 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 5 | 2 | 60 | 150 | 1 | 43 | 91 | 283 | 5 | 62 | 232 | 259 |
| Peak Hour Factor | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 1 | 1 | 16 | 40 | 0 | 12 | 25 | 76 | 1 | 17 | 63 | 70 |
| Total Analysis Volume [veh/h] | 5 | 2 | 65 | 162 | 1 | 46 | 98 | 305 | 5 | 67 | 250 | 279 |
| Pedestrian Volume [ped/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |

Generated with PTV VISTRO
Version 5.00-00
Control Type:
Analysis Method:
Two-way stop
HCM 2010
15 minutes
Intersecion Level Of Service Repor
Intersection 2: Todd Rd/Moorland
Delay (sec / veh):
Level Of Service:
74.8
$F$

Analysis Method:
Analysis Period:
5 minutes
Volume to Capacity (v/c)
0.784

| Name | Moorland Ave |  | Todd Rd |  | Todd Rd |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Southbound |  | Eastbound |  | Westbound |  |
| Lane Configuration | 75 |  | $7$ |  | $F$ |  |
| Turning Movement | Left | Right | Left | Thru | Thru | Right |
| Lane Width [f] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Pocket | 0 | 1 | 1 | 0 | 1 | 0 |
| Pocket Length [ft] | 100.00 | 50.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| Speed [mph] | 30.00 |  | 35.00 |  | 35.00 |  |
| Grade [\%] | 0.00 |  | 0.00 |  | 0.00 |  |
| Crosswalk | No |  | No |  | No |  |

Volumes

| $\begin{gathered} \hline \text { Name } \\ \hline \text { Base Volume Input [veh/h] } \end{gathered}$ | Moorland Ave |  | Todd Rd |  | Todd Rd |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 124 | 30 | 12 | 482 | 501 | 143 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 2 | 2 | 41 | 41 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [vehh/] | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 124 | 32 | 14 | 523 | 542 | 143 |
| Peak Hour Factor | 0.9000 | 0.9000 | 0.9000 | 0.9000 | 0.9000 | 0.9000 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 34 | 9 | 4 | 145 | 151 | 40 |
| Total Analysis Volume [veh/h] | 138 | 36 | 16 | 581 | 602 | 159 |
| Pedestrian Volume [ped/h] | 0 |  | 0 |  | 0 |  |

Generated with PTV VISTRO
Version $5.00-00$
Version $5.00-00$


Volumes

| $\begin{gathered} \hline \text { Name } \\ \hline \text { Base Volume Input [veh/h] } \end{gathered}$ | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2 | 4 | 25 | 252 | 2 | 65 | 45 | 316 | 7 | 15 | 264 | 171 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 2 | 0 | 43 | 0 | 0 | 0 | 0 | 0 | 2 | 43 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 4 | 4 | 68 | 252 | 2 | 65 | 45 | 316 | 9 | 58 | 264 | 171 |
| Peak Hour Factor | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 1 | 1 | 18 | 68 | 1 | 17 | 12 | 85 | 2 | 16 | 71 | 46 |
| Total Analysis Volume [veh/h] | 4 | 4 | 73 | 271 | 2 | 70 | 48 | 339 | 10 | 62 | 284 | 184 |
| Pedestrian Volume [ped/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |

Generated with PTV VISTRO
Version 5.00-00
Control Type:
Analysis Method:
Two-way stop
HCM 2010
15 minutes
Intersection Level Of Service Repor
Intersection 2: Todd Rd/Moorland
Delay (sec / veh):
Level Of Service:
136.6
$F$
1.6

Volume to Capacity (v/c): $\quad$| F |
| :---: |
|  |
| 1.012 |

| Name | Moorland Ave |  | Todd Rd |  | Todd Rd |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Southbound |  | Eastbound |  | Westbound |  |
| Lane Configuration | 75 |  | $7$ |  | $F$ |  |
| Turning Movement | Left | Right | Left | Thru | Thru | Right |
| Lane Width [f] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Pocket | 0 | 1 | 1 | 0 | 1 | 0 |
| Pocket Length [ft] | 100.00 | 50.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| Speed [mph] | 30.00 |  | 35.00 |  | 35.00 |  |
| Grade [\%] | 0.00 |  | 0.00 |  | 0.00 |  |
| Crosswalk | No |  | No |  | No |  |

volumes

| Name | Moorland Ave |  | Todd Rd |  | Todd Rd |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 142 | 30 | 40 | 611 | 433 | 189 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 2 | 2 | 41 | 41 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 142 | 32 | 42 | 652 | 474 | 189 |
| Peak Hour Factor | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 38 | 9 | 11 | 173 | 126 | 50 |
| Total Analysis Volume [veh/h] | 151 | 34 | 45 | 694 | 504 | 201 |
| Pedestrian Volume [ped/h] | 0 |  | 0 |  | 0 |  |

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Volume

| Name | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 3 | 2 | 17 | 150 | 1 | 43 | 91 | 283 | 3 | 19 | 232 | 259 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 2 | 0 | 43 | 0 | 0 | 0 | 0 | 0 | 2 | 43 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Righ-Turn on Red Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 5 | 2 | 60 | 150 | 1 | 43 | 91 | 283 | 5 | 62 | 232 | 259 |
| Peak Hour Factor | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 | 0.9280 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 1 | 1 | 16 | 40 | 0 | 12 | 25 | 76 | 1 | 17 | 63 | 70 |
| Total Analysis Volume [veh/h] | 5 | 2 | 65 | 162 | 1 | 46 | 98 | 305 | 5 | 67 | 250 | 279 |
| Presence of On-Street Parking | No |  | No | No |  | No | No |  | No | No |  | No |
| On-Street Parking Maneuver Rate [/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Local Bus Stopping Rate [h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pedestrian Volume [ped/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |
| Bicycle Volume [bicycles/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |

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Version 5.00-00

| Lane Group | c | L | c | L | c | L | c |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| c, Cycle Length [s] | 60 | 60 | 60 | 60 | 60 | 60 | 60 |
| L. Total Lost Time per Cycle [s] | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 |
| 11_p, Permitted Start-Up Lost Time [s] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 12, Clearance Lost Time [s] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| g_i, Effective Green Time [s] | 4 | 7 | 7 | 4 | 30 | 3 | 29 |
| $\mathrm{g} / \mathrm{C}, \mathrm{Green} / \mathrm{Cycle}$ | 0.06 | 0.12 | 0.12 | 0.07 | 0.49 | 0.06 | 0.48 |
| ( $\mathrm{V} / \mathrm{s}$ )_i Volume / Saturation Flow Rate | 0.04 | 0.09 | 0.03 | 0.06 | 0.17 | 0.04 | 0.31 |
| s , saturation flow rate [ [veh/h] | 1602 | 1774 | 1588 | 1774 | 1857 | 1774 | 1704 |
| c, Capacity [veh/h] | 97 | 223 | 199 | 132 | 910 | 104 | 808 |
| d1, Uniform Delay [s] | 27.85 | 25.38 | 23.76 | 27.35 | 9.42 | 27.77 | 12.09 |
| k, delay calibration | 0.11 | 0.11 | 0.11 | 0.11 | 0.50 | 0.11 | 0.50 |
| 1, Upstream Filtering Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| d2, Incremental Delay [s] | 10.41 | 4.51 | 0.60 | 8.03 | 1.02 | 6.56 | 4.11 |
| d3, Initial Queue Delay [s] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Rp, platoon ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| PF, progression factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |


| X, volume / capacity | 0.74 | 0.73 | 0.24 | 0.74 | 0.34 | 0.65 | 0.65 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d, Delay for Lane Group [s/veh] | 38.26 | 29.88 | 24.36 | 35.38 | 10.43 | 34.33 | 16.20 |
| Lane Group LOS | D | c | c | D | B | C | B |
| Critical Lane Group | Yes | Yes | No | Yes | No | No | Yes |
| 50th-Percentile Queue Length [veh] | 1.32 | 2.37 | 0.60 | 1.58 | 2.25 | 1.07 | 5.25 |
| 50th-Percentile Queue Length [t] | 32.91 | 59.31 | 15.05 | 39.43 | 56.37 | 26.73 | 131.15 |
| 95th-Percentile Queue Length [veh] | 2.37 | 4.27 | 1.08 | 2.84 | 4.06 | 1.92 | 9.00 |
| 95th-Percentile Queue Length [t]] | 59.25 | 106.75 | 27.09 | 70.97 | 101.47 | 48.11 | 225.05 |

## Generated with PTV VISTRO

Version $5.00-00$
Movement, Approach, \& Intersection Results

| d_M, Delay for Movement [s/ven] | 38.26 | 38.26 | 38.26 | 29.88 | 24.36 | 24.36 | 35.38 | 10.43 | 10.43 | 34.33 | 16.20 | 16.20 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement LOS | D | D | D | c | c | c | D | в | в | c | в | в |
| d_A, Approach Delay [s/ven] | 38.26 |  |  | 28.64 |  |  | 16.42 |  |  | 18.24 |  |  |
| Approach LOS | D |  |  | c |  |  | B |  |  | B |  |  |
| d_L, Intersection Delay [s/veh] | 20.48 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS | c |  |  |  |  |  |  |  |  |  |  |  |
| Intersection V/C | 0.627 |  |  |  |  |  |  |  |  |  |  |  |



Generated with PTV VISTRO


Volum

| Name | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2 | 4 | 25 | 252 | 2 | 65 | 45 | 316 | 7 | 15 | 264 | 171 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 2 | 0 | 43 | 0 | 0 | 0 | 0 | 0 | 2 | 43 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Right-Turn on Red Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | , | 0 | , |
| Total Hourly Volume [veh/h] | 4 | 4 | 68 | 252 | 2 | 65 | 45 | 316 | 9 | 58 | 264 | 171 |
| Peak Hour Factor | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 | 0.9310 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 1 | 1 | 18 | 68 | 1 | 17 | 12 | 85 | 2 | 16 | 71 | 46 |
| Total Analysis Volume [veh/h] | 4 | 4 | 73 | 271 | 2 | 70 | 48 | 339 | 10 | 62 | 284 | 184 |
| Presence of On-Street Parking | No |  | No | No |  | No | No |  | No | No |  | No |
| On-Street Parking Maneuver Rate [/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Local Bus Stopping Rate [/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pedestrian Volume [ped/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |
| Bicycle Volume [bicycles/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |

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Version 5.00-00

| Lane Group | c | L | c | L | c | L | c |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| c, Cycle Length [s] | 60 | 60 | 60 | 60 | 60 | 60 | 60 |
| L, Total Lost Time per Cycle [s] | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 |
| 11_p, Permitted Start-Up Lost Time [s] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 12, Clearance Lost Time [s] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| g_i, Effective Green Time [s] | 4 | 11 | 11 | 3 | 26 | 3 | 26 |
| $\mathrm{g} / \mathrm{C}, \mathrm{Green} / \mathrm{Cycle}$ | 0.06 | 0.19 | 0.19 | 0.05 | 0.43 | 0.05 | 0.43 |
| ( $\mathrm{V} / \mathrm{s}$ )_i Volume / Saturation Flow Rate | 0.05 | 0.15 | 0.05 | 0.03 | 0.19 | 0.03 | 0.27 |
| s , saturation flow rate [ [veh/h] | 1604 | 1774 | 1590 | 1774 | 1853 | 1774 | 1742 |
| c, Capacity [veh/h] | 101 | 340 | 304 | 83 | 786 | 98 | 753 |
| d1, Uniform Delay [s] | 27.79 | 23.21 | 20.60 | 28.08 | 12.28 | 27.83 | 13.25 |
| k, delay calibration | 0.11 | 0.11 | 0.11 | 0.11 | 0.50 | 0.11 | 0.50 |
| 1, Upstream Filtering Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| d2, Incremental Delay [s] | 13.24 | 4.32 | 0.40 | 6.17 | 1.81 | 6.68 | 3.84 |
| d3, Initial Queue Delay [s] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Rp, platoon ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| PF, progression factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |


| X, volume / capacity | 0.80 | 0.80 | 0.24 | 0.58 | 0.44 | 0.64 | 0.62 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d, Delay for Lane Group [s/veh] | 41.04 | 27.53 | 20.99 | 34.25 | 14.09 | 34.51 | 17.08 |
| Lane Group LOS | D | c | c | C | B | C | B |
| Critical Lane Group | Yes | Yes | No | Yes | No | No | Yes |
| 50th-Percentile Queue Length [veh] | 1.54 | 3.80 | 0.83 | 0.77 | 3.18 | 0.99 | 4.86 |
| 50th-Percentile Queue Length [t] | 38.46 | 95.10 | 20.86 | 19.36 | 79.44 | 24.87 | 121.43 |
| 95th-Percentile Queue Length [veh] | 2.77 | 6.85 | 1.50 | 1.39 | 5.72 | 1.79 | 8.47 |
| 95th-Percentile Queue Length [t]] | 69.23 | 171.18 | 37.54 | 34.84 | 142.98 | 44.77 | 211.79 |

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Movement, Approach, \& Intersection Results

| d_M, Delay for Movement [s/ven] | 41.04 | 41.04 | 41.04 | 27.53 | 20.99 | 20.99 | 34.25 | 14.09 | 14.09 | 34.51 | 17.08 | 17.08 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement LOS | D | D | D | c | c | c | c | в | B | c | B | B |
| d_A, Approach Delay [s/ven] | 41.04 |  |  | 26.16 |  |  | 16.53 |  |  | 19.12 |  |  |
| Approach Los | D |  |  | c |  |  | B |  |  | B |  |  |
| d_I, Intersection Delay [s/ven] | 21.46 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS | c |  |  |  |  |  |  |  |  |  |  |  |
| Intersection V/C | 0.680 |  |  |  |  |  |  |  |  |  |  |  |



## Generated with PTV VISTRO

Version 5.00-00
Control Type:
Analysis Method

| Intersection Level Of Service ReportIntersection 1: Todd Rd/Ghiloti Ave-Standish |  |  |
| :---: | :---: | :---: |
| Two-way stop | Delay (see / veh): | 1,098.3 |
| HCM 2010 | Level Of Service: | F |
| 15 minutes | Volume to Capacity (v/c): | 04 |


| Name | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |
| Lane Configuration | + |  |  | + |  |  | $71$ |  |  | $7 F$ |  |  |
| Turning Movement | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [f] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 |
| Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 120.00 | 100.00 | 100.00 | 150.00 | 100.00 | 100.00 |
| Speed [mph] | 10.00 |  |  | 30.00 |  |  | 35.00 |  |  | 35.00 |  |  |
| Grade [\%] | 0.00 |  |  | 0.00 |  |  | $\frac{0.00}{\text { No }}$ |  |  | $\frac{0.00}{\text { No }}$ |  |  |
| Crosswalk | No |  |  | No |  |  |  |  |  |  |  |  |

Volumes

| Name | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 3 | 2 | 24 | 226 | 1 | 74 | 148 | 404 | 3 | 26 | 394 | 435 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| in-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 2 | 0 | 43 | 0 | 0 | 0 | 0 | 0 | 2 | 42 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [vehh/] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 5 | 2 | 67 | 226 | 1 | 74 | 148 | 404 | 5 | 68 | 394 | 435 |
| Peak Hour Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 1 | 1 | 17 | 57 | 0 | 19 | 37 | 101 | 1 | 17 | 99 | 109 |
| Total Analysis Volume [veh/h] | 5 | 2 | 67 | 226 | 1 | 74 | 148 | 404 | 5 | 68 | 394 | 435 |
| Pedestrian Volume [ped/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |

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Version 5.00-00

| Intersection Settings | Stop | Stop | Free | Free |
| :---: | :---: | :---: | :---: | :---: |
| Priority Scheme | No | Yes |  |  |
| Flared Lane | 0 | 1 | 0 | 0 |
| Storage Area [ven] | No | No |  |  |
| Two-Stage Gap Acceptance | 0 | 0 | 0 | 0 |
| Number of Storage Spaces in Median | 0 |  | 0 |  |

Movement, Approach, \& Intersection Results

| V/C, Movement V/C Ratio | 0.07 | 0.03 | 0.10 | 3.05 | 0.01 | 0.15 | 0.18 | 0.00 | 0.00 | 0.06 | 0.00 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d_M, Delay for Movement [s/ven] | 58.21 | 56.15 | 13.04 | 1098.33 | 1085.78 | 1057.10 | 10.50 | 0.00 | 0.00 | 8.33 | 0.00 | 0.00 |
| Movement LOS | F | F | B | F | F | F | B | A | A | A | A | A |
| 95th-Percentile Queue Length [veh] | 0.74 | 0.74 | 0.74 | 29.69 | 29.69 | 29.69 | 0.67 | 0.00 | 0.00 | 0.19 | 0.00 | 0.00 |
| 95 th-Percentile Queue Length [ft] | 18.55 | 18.55 | 18.55 | 742.13 | 742.13 | 742.13 | 16.82 | 0.00 | 0.00 | 4.71 | 0.00 | 0.00 |
| d_A, Approach Delay [s/ven] | 17.26 |  |  | 1088.15 |  |  | 2.79 |  |  | 0.63 |  |  |
| Approach Los | c |  |  | F |  |  | A |  |  | A |  |  |
| d_I, Intersection Delay [s/ven] | 180.94 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS |  |  |  |  |  |  |  |  |  |  |  |  |

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Version $5.00-00$
PTV VISTRO

| Intersection Level Of Service Report Intersection 2: Todd Rd/Moorland Ave |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Control Type: | Two-way stop HCM 2010 |  | Delay (sec/veh): |  |  |  |
| Analysis Method: |  |  | Level Of Service:Volume to Capacity (v/c): |  |  |  |
| Analysis Period: | 15 minutes |  |  |  |  |  |
| Intersection Setup |  |  |  |  |  |  |
| Name | Moorland Ave |  | Todd Rd |  | Todd Rd |  |
| Approach | Southbound |  | Eastbound |  | Westbound |  |
| Lane Configuration | $7$ |  | $7$ |  | $F$ |  |
| Turning Movement | Left | Right | Left | Thru | Thru | Right |
| Lane Width [f] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Pocket | 0 | 1 | 1 | 0 | 1 | 0 |
| Pocket Length [ft] | 100.00 | 50.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| Speed [mph] | 30.00 |  | 35.00 |  | 35.00 |  |
| Grade [\%] | 0.00 |  | 0.00 |  | 0.00 |  |
| Crosswalk | No |  | No |  | No |  |

Volumes

| Name | Moorland Ave |  | Todd Rd |  | Todd Rd |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 43 | 111 | 118 | 570 | 765 | 163 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 2 | 2 | 41 | 40 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 43 | 113 | 120 | 611 | 805 | 163 |
| Peak Hour Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 11 | 28 | 30 | 153 | 201 | 41 |
| Total Analysis Volume [veh/h] | 43 | 113 | 120 | 611 | 805 | 163 |
| Pedestrian Volume [ped/h] |  |  |  |  |  |  |

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Intersection Settings

| Priority Scheme | Stop | Free | Free |
| :---: | :---: | :---: | :---: |
| Flared Lane |  |  |  |
| Storage Area [veh] | 0 | 0 | 0 |
| Two-Stage Gap Acceptance | No |  |  |
| Number of Storage Spaces in Median | 0 | 0 | 0 |

Movement, Approach, \& Intersection Results

| V/C, Movement V/C Ratio | 0.54 | 0.33 | 0.17 | 0.01 | 0.01 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d_M, Delay for Movement [s/veh] | 93.76 | 20.55 | 11.08 | 0.00 | 0.00 | 0.00 |
| Movement LOS | F | c | B | A | A | A |
| 95th-Percentile Queue Length [veh] | 2.33 | 1.40 | 0.60 | 0.00 | 0.00 | 0.00 |
| 95 th-Percentile Queue Length [ft] | 58.22 | 35.09 | 15.09 | 0.00 | 0.00 | 0.00 |
| d_A, Approach Delay [s/ven] | 40.73 |  | 1.82 |  | 0.00 |  |
| Approach Los | E |  | A |  | A |  |
| d_I, Intersection Delay [s/veh] | 4.14 |  |  |  |  |  |
| Intersection LOS | F |  |  |  |  |  |

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Version 5.00-00

| Intersection Level Of Service Report |  |  |  |
| :---: | :---: | :---: | :---: |
| Intersection 1: Todd Rd/Ghilotti Ave-Standish Ave |  |  |  |
| Control Type: | Two-way stop | Delay (sec / veh): | 943.5 |
| Analysis Method: | HCM 2010 | Level Of Service: | F |
| Analysis Period: | 15 minutes | Volume to Capacity (v/c): | 4.721 |


| Name | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |
| Lane Configuration | + |  |  | + |  |  | $71$ |  |  | $7 F$ |  |  |
| Turning Movement | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [f] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 |
| Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 120.00 | 100.00 | 100.00 | 150.00 | 100.00 | 100.00 |
| Speed [mph] | 10.00 |  |  | 30.00 |  |  | 35.00 |  |  | 35.00 |  |  |
| Grade [\%] | 0.00 |  |  | 0.00 |  |  | $\frac{0.00}{\text { No }}$ |  |  | $\frac{0.00}{\text { No }}$ |  |  |
| Crosswalk | No |  |  | No |  |  |  |  |  |  |  |  |

Volumes

| Name | ti Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 3 | 4 | 34 | 438 | 2 | 199 | 108 | 350 | 8 | 24 | 443 | 355 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 2 | 0 | 43 | 0 | 0 | 0 | 0 | 0 | 2 | 42 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [vehh/] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 5 | 4 | 77 | 438 | 2 | 199 | 108 | 350 | 10 | 66 | 443 | 355 |
| Peak Hour Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 1 | 1 | 19 | 110 | 1 | 50 | 27 | 88 | 3 | 17 | 111 | 89 |
| Total Analysis Volume [veh/h] | 5 | 4 | 77 | 438 | 2 | 199 | 108 | 350 | 10 | 66 | 443 | 355 |
| Pedestrian Volume [ped/h] |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |

## Generated with PTV VISTRO

Intersection Settings

| Priority Scheme | Stop | Stop | Free | Free |
| :---: | :---: | :---: | :---: | :---: |
| Flared Lane | No | Yes |  |  |
| Storage Area [ven] | 0 | 1 | 0 | 0 |
| Two-Stage Gap Acceptance | No | No |  |  |
| Number of Storage Spaces in Median | 0 | 0 | 0 | 0 |

Movement, Approach, \& Intersection Results

| V/C, Movement V/C Ratio | 0.09 | 0.04 | 0.11 | 4.72 | 0.02 | 0.41 | 0.13 | 0.00 | 0.00 | 0.06 | 0.00 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d_M, Delay for Movement [s/veh] | 71.04 | 44.10 | 13.34 | 1943.47 | 1932.95 | 1912.05 | 10.02 | 0.00 | 0.00 | 8.18 | 0.00 | . 00 |
| Movement LOS | F | E | в | F | F | F | в | A | A | A | A | A |
| 95th-Percentile Queue Length [veh] | 0.92 | 0.92 | 0.92 | 67.87 | 67.87 | 67.87 | 0.45 | 0.00 | 0.00 | 0.17 | 0.00 | 0.00 |
| 95 th-Percentile Queue Length [ft] | 22.96 | 22.96 | 22.96 | 1696.87 | 1696.87 | 1696.87 | 11.25 | 0.00 | 0.00 | 4.36 | 0.00 | 0.00 |
| d_A, Approach Delay [s/ven] | 18.13 |  |  | 1933.65 |  |  | 2.31 |  |  | 0.62 |  |  |
| Approach Los | C |  |  | F |  |  | A |  |  | A |  |  |
| d_I, Intersection Delay [s/veh] | 602.23 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS |  |  |  |  |  |  |  |  |  |  |  |  |

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Version $5.00-00$
PTV VISTRO

| Intersection Level Of Service Report Intersection 2: Todd Rd/Moorland Ave |  |  |  |
| :---: | :---: | :---: | :---: |
| Control Type: | Two-way stop | Delay (sec / veh): | 304.7 |
| Analysis Method: | HCM 2010 | Level Of Service: | F |
| Analysis Period: | 15 minutes | Volume to Capacity (v/c): | 1.303 |


| Name | Moorland Ave |  | Todd Rd |  | Todd Rd |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Southbound |  | Eastbound |  | Westbound |  |
| Lane Configuration | $7$ |  | $7$ |  | $F$ |  |
| Turning Movement | Left | Right | Left | Thru | Thru | Right |
| Lane Width [t] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Pocket | 0 | 1 | 1 | 0 | 1 | 0 |
| Pocket Length [ft] | 100.00 | 50.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| Speed [mph] | 30.00 |  | 35.00 |  | 35.00 |  |
| Grade [\%] | 0.00 |  | 0.00 |  | 0.00 |  |
| Crosswalk | No |  | No |  | No |  |

Volumes

| Name | Moorland Ave |  | Todd Rd |  | Todd Rd |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 96 | 186 | 139 | 739 | 647 | 89 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 2 | 2 | 41 | 40 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [vehh] | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 96 | 188 | 141 | 780 | 687 | 89 |
| Peak Hour Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 24 | 47 | 35 | 195 | 172 | 22 |
| Total Analysis Volume [veh/h] | 96 | 188 | 141 | 780 | 687 | 89 |
| Pedestrian Volume [ped/h] |  |  |  |  |  |  |

## Generated with PTV VISTRO

Version $5.00-00$
Intersection Settings

| Priority Scheme | Stop | Free | Free |
| :---: | :---: | :---: | :---: |
| Flared Lane |  |  |  |
| Storage Area [veh] | 0 | 0 | 0 |
| Two-Stage Gap Acceptance | No |  |  |
| Number of Storage Spaces in Median | 0 | 0 | 0 |

Movement, Approach, \& Intersection Results

| V/C, Movement V/C Ratio | 1.30 | 0.45 | 0.17 | 0.01 | 0.01 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d_M, Delay for Movement [s/ven] | 304.70 | 20.24 | 10.15 | 0.00 | 0.00 | 0.00 |
| Movement LOS | F | C | B | A | A | A |
| 955 h-Percentile Queue Length [veh] | 7.56 | 2.24 | 0.60 | 0.00 | 0.00 | 0.00 |
| 95th-Percentile Queue Length [ft] | 188.93 | 56.09 | 15.02 | 0.00 | 0.00 | 0.00 |
| d_A, Approach Delay [s/ven] | 116.40 |  | 1.55 |  | 0.00 |  |
| Approach Los | F |  | A |  | A |  |
| d_L, Intersection Delay [s/ven] | 17.41 |  |  |  |  |  |
| Intersection LOS | F |  |  |  |  |  |

Ghilotti Construction Yard TIS
PM Future + Project
(W-Trans
W-Trans

## Generated with PTV VISTRO



| Name | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 3 | 2 | 24 | 226 | 1 | 74 | 148 | 404 | 3 | 26 | 394 | 435 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [ven/h] | 2 | 0 | 43 | 0 | 0 | 0 | 0 | 0 | 2 | 42 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [vehh/] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Right-Turn on Red Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 5 | 2 | 67 | 226 | 1 | 74 | 148 | 404 | 5 | 68 | 394 | 435 |
| Peak Hour Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 1 | 1 | 17 | 57 | 0 | 19 | 37 | 101 | 1 | 17 | 99 | 109 |
| Total Analysis Volume [veh/h] | 5 | 2 | 67 | 226 | 1 | 74 | 148 | 404 | 5 | 68 | 394 | 435 |
| Presence of On-Street Parking | No |  | No | No |  | No | No |  | No | No |  | No |
| On-Street Parking Maneuver Rate [ h$]$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Local Bus Stopping Rate [/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pedestrian Volume [ped/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |
| Bicycle Volume [bicycles/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |

## Generated with PTV VISTRO

Version 5.00-00

| Lane Group | c | L | c | L | c | L | c |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| c, Cycle Length [s] | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| L, Total Lost Time per Cycle [s] | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 |
| 11_p, Permitted Start-Up Lost Time [s] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 12, Clearance Lost Time [s] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| g_i, Effective Green Time [s] | 5 | 11 | 11 | 9 | 54 | 5 | 49 |
| $\mathrm{g} / \mathrm{C}, \mathrm{Green}$ / Cycle | 0.06 | 0.12 | 0.12 | 0.10 | 0.59 | 0.05 | 0.54 |
| ( $\mathrm{V} / \mathrm{s}$ ) i Volume / Saturation Flow Rate | 0.05 | 0.13 | 0.05 | 0.08 | 0.22 | 0.04 | 0.49 |
| s , saturation flow rate [ [veh/h] | 1601 | 1774 | 1587 | 1774 | 1859 | 1774 | 1705 |
| c, Capacity [veh/h] | 89 | 214 | 192 | 180 | 1107 | 89 | 928 |
| d1, Uniform Delay [s] | 42.08 | 39.57 | 36.52 | 39.64 | 9.44 | 42.21 | 18.20 |
| k, delay calibration | 0.11 | 0.11 | 0.11 | 0.11 | 0.50 | 0.11 | 0.50 |
| I, Upstream Fillering Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| d2, Incremental Delay [s] | 17.35 | 44.01 | 1.30 | 8.96 | 0.95 | 12.49 | ${ }^{12.83}$ |
| d3, Initial Queue Delay [s] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Rp, platoon ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| PF, progression factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |


| X, volume / capacity | 0.83 | 1.05 | 0.39 | 0.82 | 0.37 | 0.76 | 0.89 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d, Delay for Lane Group [s/veh] | 59.43 | 83.58 | 37.82 | 48.60 | 10.39 | 54.70 | 31.03 |
| Lane Group LOS | E | F | D | D | B | D | c |
| Critical Lane Group | Yes | Yes | No | Yes | No | No | Yes |
| 50th-Percentile Queue Length [veh] | 2.11 | 7.27 | 1.57 | 3.57 | 3.97 | 1.77 | 16.69 |
| 50th-Percentile Queue Length [tt] | 52.69 | 181.82 | 39.28 | 89.35 | 99.29 | 44.22 | 417.34 |
| 95th-Percentile Queue Length [veh] | 3.79 | 11.95 | 2.83 | 6.43 | 7.15 | 3.18 | 23.39 |
| 95 th-Percentile Queue Length [ft] | 94.85 | 298.70 | 70.71 | 160.82 | 178.72 | 79.60 | 584.86 |

## Generated with PTV VISTRO

| Intersection Level Of Service Report Intersection 1: Todd Rd/Ghilotti Ave-Standish Ave |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Control Type: | Signalized HCM 2010 |  |  |  |  | Delay (sec / veh): |  |  |  | 44.1 |  |  |
| Analysis Method: |  |  |  |  |  |  | Level Of | Service: |  |  |  |  |
| Analysis Period: | HCM 2010 15 minutes |  |  |  |  | Volume to Capacity (v/c): |  |  |  | 0.942 |  |  |
| Intersection Setup |  |  |  |  |  |  |  |  |  |  |  |  |
| Name | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| Approach | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |
| Lane Configuration | 中 |  |  | $7 \mathrm{~F}$ |  |  | $7 \mathrm{~F}$ |  |  | $7 \mathrm{~F}$ |  |  |
| Turning Movement | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Pocket | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 |
| Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 120.00 | 100.00 | 100.00 | 150.00 | 100.00 | 100.00 |
| Speed [mph] |  | 10.00 |  |  | 30.00 |  |  | 35.00 |  |  | 35.00 |  |
| Grade [\%] |  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |
| Crosswalk |  | No |  |  | No |  |  | No |  |  | No |  |

Volum

| Name | Ghilotit Ave |  |  | Standish Ave |  |  | Todd Rd |  |  | Todd Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 3 | 4 | 34 | 438 | 2 | 199 | 108 | 350 | 8 | 24 | 443 | 355 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Rate | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 2 | 0 | 43 | 0 | 0 | 0 | 0 | 0 | 2 | 42 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Right-Turn on Red Volume [veh/h] | 0 | 0 | 11 | 0 | 0 | 66 | 0 | 0 | 3 | 0 | 0 | 66 |
| Total Hourly Volume [veh/h] | 5 | 4 | 66 | 438 | 2 | 133 | 108 | 350 | 7 | 66 | 443 | 289 |
| Peak Hour Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 1 | 1 | 17 | 110 | 1 | 33 | 27 | 88 | 2 | 17 | 111 | 72 |
| Total Analysis Volume [veh/h] | 5 | 4 | 66 | 438 | 2 | ${ }^{133}$ | 108 | 350 | 7 | 66 | 443 | 289 |
| Presence of On-Street Parking | No |  | No | No |  | No | No |  | No | No |  | No |
| On-Street Parking Maneuver Rate [/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Local Bus Stopping Rate [h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pedestrian Volume [ped/h] | 0 |  |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Bicycle Volume [bicycles/h] |  |  |  | 0 |  |  | 0 |  |  | 0 |  |  |

## Generated with PTV VISTRO

Version 5.00-00

| Lane Group | c | L | c | L | c | L | c |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| c, Cycle Length [s] | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| L. Total Lost Time per Cycle [s] | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 |
| 11_p, Permitted Start-Up Lost Time [s] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 12, Clearance Lost Time [s] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| g_i, Effective Green Time [s] | 5 | 23 | 23 | 5 | 42 | 4 | 41 |
| g/ C, Green / Cycle | 0.06 | 0.26 | 0.26 | 0.06 | 0.46 | 0.05 | 0.45 |
| ( $\mathrm{V} / \mathrm{s}$ )_i Volume / Saturation Flow Rate | 0.05 | 0.25 | 0.09 | 0.06 | 0.19 | 0.04 | 0.42 |
| s , saturation flow rate [ [veh/h] | 1608 | 1774 | 1587 | 1774 | 1856 | 1774 | 1741 |
| c, Capacity [veh/h] | 89 | 453 | 405 | 102 | 859 | 87 | 790 |
| d1, Uniform Delay [s] | 42.10 | 33.14 | 27.28 | 42.41 | 16.09 | 42.29 | 23.16 |
| k, delay calibration | 0.11 | 0.26 | 0.11 | 0.11 | 0.50 | 0.11 | 0.50 |
| I, Upstream Fillering Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| d2, Incremental Delay [s] | 18.20 | 23.56 | 0.48 | 57.16 | 1.48 | 12.87 | 18.40 |
| d3, Initial Queue Delay [s] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Rp, platoon ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| PF, progression factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |


| X, volume / capacity | 0.84 | 0.97 | 0.33 | 1.06 | 0.42 | 0.76 | b. 93 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d, Delay for Lane Group [s/veh] | 60.30 | 56.71 | 27.76 | 99.57 | 17.57 | 55.16 | ${ }^{41.56}$ |
| Lane Group LOS | E | E | c | F | B | E | D |
| Critical Lane Group | Yes | Yes | No | Yes | No | No | Yes |
| 50th-Percentile Queue Length [veh] | 2.15 | 12.11 | 2.38 | 3.84 | 4.92 | 1.73 | 17.33 |
| 50th-Percentile Queue Length [t]] | 53.82 | 302.82 | 59.38 | 96.07 | 122.96 | 43.16 | 433.30 |
| 95th-Percentile Queue Length [veh] | 3.88 | 17.82 | 4.28 | 6.92 | 8.56 | 3.11 | 24.16 |
| 95th-Percentile Queue Length [tt] | 96.88 | 445.51 | 106.88 | 172.93 | 213.89 | 77.69 | 603.99 |

## Appendix C

Signalized Intersection Level of Service Calculations

SimTraffic Performance Report

## AM Existing

11/13/2017
3: S Moorland Ave \& Todd Rd/US 101 South Ramps Performance by approach


4: Todd Rd Overcrossing \& US 101 North Off-ramp/Todd Rd Performance by approach

|  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Approach | EB | WB | NB | All |
| Denied Del/Veh (s) | 3.3 | 0.0 | 0.0 | 0.7 |
| Total DelVeh (s) | 5.4 | 8.4 | 7.5 | 7.4 |

5: Santa Rosa Ave \& Todd Rd Performance by approach


Total Zone Performance

|  |  |
| :--- | ---: |
| Denied Del/Veh (s) | 1.9 |
| Total Del/Veh (s) | 240.3 |

SimTraffic Performance Report
PM Existing
3: S Moorland Ave \& Todd Rd/US 101 South Ramps Performance by approach

| Approach | EB | WB | NB | All |
| :--- | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.0 | 0.0 |
| Total DelVeh (s) | 14.6 | 31.5 | 25.5 | 22.7 |

$\begin{array}{lllll}\text { Total Del/Veh (s) } & 14.6 & 31.5 & 25.5 & 22.7\end{array}$
4: Todd Rd Overcrossing \& US 101 North Off-ramp/Todd Rd Performance by approach

| Approach | EB | WB | NB | All |
| :--- | :---: | :---: | :---: | :---: |
| Denied DelVeh (s) | 3.1 | 0.0 | 0.0 | 0.5 |
| Total DelVeh (s) | 6.9 | 6.9 | 5.6 | 6.3 |

5: Santa Rosa Ave \& Todd Rd Performance by approach

| Approach | EB | WB | NB | SB | All |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Denied DelVeh (s) | 0.0 | 1.3 | 1.0 | 1.3 | 0.9 |

$\begin{array}{lrrrrr} & 0.0 & 1.3 & 1.0 & 1.3 & 0.9\end{array}$
Total Zone Performance

|  | 1.3 |
| :--- | ---: |
| Denied Delveh (s) | 277.6 |
| Total DelVeh $(\mathrm{s})$ |  |

Total Del/Veh (s)
277.6

SimTraffic Performance Report

## AM Baseline

11/13/20017
3: S Moorland Ave \& Todd Rd/US 101 South Ramps Performance by approach


4: Todd Rd Overcrossing \& US 101 North Off-ramp/Todd Rd Performance by approach

| Approach | EB | WB | NB | All |
| :--- | :---: | :---: | :---: | :---: |
| Denied Delveh (s) | 3.4 | 0.0 | 0.0 | 0.8 |
| Total DelVeh (s) | 5.7 | 8.2 | 6.9 | 7.1 |

5: Santa Rosa Ave \& Todd Rd Performance by approach


Total Zone Performance

|  | 1.8 |
| :--- | ---: |
| Denied Del/Veh (s) | 244.4 |

SimTraffic Performance Report
PM Baseline
3: S Moorland Ave \& Todd Rd/US 101 South Ramps Performance by approach


4: Todd Rd Overcrossing \& US 101 North Off-ramp/Todd Rd Performance by approach

| Approach | EB | WB | NB | All |
| :--- | :---: | :---: | :---: | :---: |
| Denied DelVeh (s) | 3.1 | 0.0 | 0.0 | 0.5 |
| Total DelVeh (s) | 7.5 | 8.3 | 6.2 | 7.2 |

5: Santa Rosa Ave \& Todd Rd Performance by approach

| Approach | EB | WB | NB | SB | All |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Denied DelVeh (s) | 0.0 | 1.3 | 1.1 | 1.2 | 0.9 |

$\begin{array}{lrrrrr}\text { Denied } & & 1.0 & 1.3 & 1.1 & 1.2 \\ \text { Total DelVeh }(s) & 14.9 & 30.4 & 2.4 & 180 & \end{array}$

Total Zone Performance

|  | 1.4 |
| :--- | ---: |
| Denied DelVeh $(\mathrm{s})$ | 277.5 |
| Total DelVeh (s) |  |

SimTraffic Performance Report
AM Future
11/13/20017
3: S Moorland Ave \& Todd Rd/US 101 South Ramps Performance by approach


4: Todd Rd Overcrossing \& US 101 North Off-ramp/Todd Rd Performance by approach

| Approach | EB | WB | NB | All |
| :--- | :--- | :--- | :--- | :--- |
| Denied Del/Veh $(\mathrm{s})$ | 3.5 | 0.0 | 0.0 | 0.8 |
| Total Delveh |  | 5.5 | 7.9 | 8.5 |
| 7.6 |  |  |  |  |

5: Santa Rosa Ave \& Todd Rd Performance by approach


Total Zone Performance

|  |  |
| :--- | ---: |
| Denied Del/Veh (s) | 1.5 |
| Total Del/Veh (s) | 291.8 |

SimTraffic Performance Report
PM Future
3: S Moorland Ave \& Todd Rd/US 101 South Ramps Performance by approach


4: Todd Rd Overcrossing \& US 101 North Off-ramp/Todd Rd Performance by approach

| Approach | EB | WB | NB | All |
| :--- | :---: | :---: | :---: | :---: |
| Denied DelVeh (s) | 3.7 | 0.0 | 0.0 | 0.4 |
| Total DelVeh (s) | 6.4 | 6.8 | 7.9 | 7.4 |

5: Santa Rosa Ave \& Todd Rd Performance by approach

| Approach | EB | WB | NB | SB | All |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Denied DelVeh (s) | 1.9 | 2.7 | 2.5 | 0.4 | 1.9 |

$\begin{array}{lllrrr} & & 2.9 & 2.5 & 0.4 & 1.9\end{array}$
Total Zone Performance

|  | 2.2 |
| :--- | ---: |
| Denied DelVeh (s) | 328.6 |
| Total DelVeh (s) |  |

SimTraffic Performance Report
AM Future plus Mitigation
0912812017
5: Santa Rosa Ave \& Todd Rd Performance by approach


SimTraffic Performance Report PM Future plus Mitigation
5: Santa Rosa Ave \& Todd Rd Performance by approach

| Approach | EB | WB | NB | SB | All |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 1.2 | 3.0 | 0.7 | 0.4 | 0.8 |
| Total DelVeh (s) | 20.0 | 54.8 | 42.3 | 45.5 | 40.8 |

$\begin{array}{llllll}\text { Total Deliveh (s) } & 20.0 & 54.8 & 42.3 & 45.5 & 40.8\end{array}$

SimTraffic Performance Report
AM Existing plus Project
11/13/2017
3: S Moorland Ave \& Todd Rd/US 101 South Ramps Performance by approach


4: Todd Rd Overcrossing \& US 101 North Off-ramp/Todd Rd Performance by approach

| Approach | EB | WB | NB | All |
| :--- | :---: | :---: | :---: | :---: |
| Denied DelVeh (s) | 3.2 | 0.0 | 0.0 | 0.8 |
| Total DelVeh $(\mathrm{s})$ | 6.0 | 7.5 | 6.8 | 6.9 |

5: Santa Rosa Ave \& Todd Rd Performance by approach


Total Zone Performance

|  |  |
| :--- | ---: |
| Denied Del/Veh (s) | 1.9 |
| Total DelVeh (s) | 271.3 |

SimTraffic Performance Repor
PM Existing plus Project
3: S Moorland Ave \& Todd Rd/US 101 South Ramps Performance by approach


4: Todd Rd Overcrossing \& US 101 North Off-ramp/Todd Rd Performance by approach

| Approach | EB | WB | NB | All |
| :--- | :---: | :---: | :---: | :---: |
| Denied Del/Veh (s) | 3.0 | 0.0 | 0.0 | 0.5 |
| Total DelVeh (s) | 7.0 | 8.3 | 6.2 | 7.1 |

5: Santa Rosa Ave \& Todd Rd Performance by approach

| Approach | EB | WB | NB | SB | All |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Denied DelVeh (s) | 0.0 | 1.3 | 0.9 | 1.3 | 0.8 |

$\begin{array}{lllllll}\text { Total Delveh (s) } & 155 & 1.3 & 0.9 & 1.3 & 0.8\end{array}$
Total Zone Performance

|  | 1.3 |
| :--- | ---: |
| Denied Del/Veh (s) | 289.3 |

Total DelVeh (s)
289.3

[^7]PM Existing + Project

## SimTraffic Performance Report

AM Baseline + Project
11/13/20017
3: S Moorland Ave \& Todd Rd/US 101 South Ramps Performance by approach


4: Todd Rd Overcrossing \& US 101 North Off-ramp/Todd Rd Performance by approach

| Approach | EB | WB | NB | All |
| :--- | :--- | :--- | :--- | :--- |
| Denied Del/Veh $(s)$ | 3.3 | 0.0 | 0.1 | 0.8 |
| Total Delveh $(\mathrm{s})$ | 6.1 | 8.1 | 7.6 | 7.4 |

5: Santa Rosa Ave \& Todd Rd Performance by approach


Total Zone Performance

|  | 1.9 |
| :--- | ---: |
| Denied Del/Veh (s) | 257.7 |
| Total Del/Veh (s) |  |

SimTraffic Performance Report
PM Baseline + Project
11/13/2017
3: S Moorland Ave \& Todd Rd/US 101 South Ramps Performance by approach


4: Todd Rd Overcrossing \& US 101 North Off-ramp/Todd Rd Performance by approach

| Approach | EB | WB | NB | All |
| :--- | :---: | :---: | :---: | :---: |
| Denied DelVeh (s) | 3.2 | 0.0 | 0.1 | 0.6 |
| Total DelVeh (s) | 7.0 | 8.8 | 6.3 | 7.4 |

5: Santa Rosa Ave \& Todd Rd Performance by approach

| Approach | EB | WB | NB | SB | All |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Denied DelVeh (s) | 0.0 | 1.3 | 1.1 | 1.3 | 0.9 |

$\begin{array}{lrrrrr}\text { Donied } & & 1.3 & 1.1 & 1.3 & 0.9\end{array}$
Total Zone Performance

|  | 1.5 |
| :--- | ---: |
| Denied DelVeh (s) | 299.4 |
| Total DelVeh (s) |  |

Total DelVeh (s)
299.4

## Ghilotii Construction Yard TIS

PM Baseline + Project

## SimTraffic Performance Report

## AM Future plus Project

3: S Moorland Ave \& Todd Rd/US 101 South Ramps Performance by approach


4: Todd Rd Overcrossing \& US 101 North Off-ramp/Todd Rd Performance by approach

| Approach | EB | WB | NB | All |
| :--- | :---: | :---: | :---: | :---: |
| Denied DelVeh (s) | 3.5 | 0.0 | 0.0 | 0.8 |

5: Santa Rosa Ave \& Todd Rd Performance by approach


Total Zone Performance

|  |  |
| :--- | ---: |
| Denied Del/Veh (s) | 30.1 |
| Total DelVeh (s) | 305.3 | 3.1

305.3

SimTraffic Performance Repor
PM Future plus Project
3: S Moorland Ave \& Todd Rd/US 101 South Ramps Performance by approach


4: Todd Rd Overcrossing \& US 101 North Off-ramp/Todd Rd Performance by approach

| Approach | EB | WB | NB | All |
| :--- | :---: | :---: | :---: | :---: |
| Denied DelVeh $(\mathrm{s})$ | 3.9 | 0.0 | 0.0 | 0.4 |
| Total DelVeh $(\mathrm{s})$ | 5.5 | 6.8 | 8.2 | 7.4 |

5: Santa Rosa Ave \& Todd Rd Performance by approach

| Approach | EB | WB | NB | SB | All |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Denied DelVeh (s) | 0.4 | 3.1 | 2.2 | 0.5 | 1.5 |

$\begin{array}{llrrrr}\text { lol } & 18.2 & 3.2 & 0.5 & 1.5\end{array}$
Total Zone Performance

|  | 1.9 |
| :--- | ---: |
| Denied DelVeh (s) | 314.2 |

SimTraffic Performance Report
AM Future plus Project and Mitigation

5: Santa Rosa Ave \& Todd Rd Performance by approach


0912812017

SimTraffic Performance Report
PM Future plus Project and Mitigation
1: Ghillotti Ave/Standish Ave \& Todd Rd Performance by approach

| Approach | EB | WB | NB | SB | All |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Denied Delveh (s) | 1.3 | 0.0 | 0.1 | 10.5 | 3.9 |
| Total Del/Veh (s) | 30.7 | 30.7 | 15.5 | 55.1 | 38.2 |

$\begin{array}{llllll}\text { Total DelVeh (s) } & 30.7 & 30.7 & 15.5 & 55.1 & 38.2\end{array}$

## Appendix D

Signal Warrants Analysis \& Equitable Share Calculations

# Warrant 3: Peak-Hour Volumes and Delay 

Sonoma County
304 Todd Road CUP
Todd Rd \& Standish-Ghilotti Ave

|  | Major Street |  |
| :--- | :---: | :---: |
| Street Name | Todd Rd | Minor Street |
| Direction | E-W | Standish-Ghilotti Ave |
| Number of Lanes | 1 | N-S |
| Approach Speed | 35 | 1 |
|  |  | 30 |

Population less than 10,000? No
Date of Count: Tuesday, October 04, 2016
Scenario:

PM Existing

| Warrant 3 Met?: Met when either Condition A or B is met |  |
| :--- | :--- |
| Condition A: Met when conditions A1, A2, and A3 are met |  |
| Condition A1 | Yes |
| The total delay experienced by traffic on one minor street approach (one direction only) |  |
| controlled by a STOP sign equals or exceeds four vehicle-hours for a one lane approach, <br> or five vehicle-hours for a two-lane approach <br> Minor Approach Delay: |  |

Condition A2
The volume on the same minor street approach (one direction only) equals or exceeds 100 vph for one moving lane of traffic of 150 vph for two moving lanes

$$
\text { Minor Approach Volume: } \quad 319 \text { vph }
$$

Condition A3
The total entering volume serviced during the hour equals or exceeds 800 vph for intersections with four or more appraches or 650 vph for intersections with three approaches

Total Entering Volume: 1158 vph
Condition B
Met

$$
5
$$

$\xrightarrow{\text { Met }}$
.
$\qquad$

# Equitable Share Calculations <br> 304 Todd Road CUP Traffic Study 

|  |  | Total Volume Entering <br> the Intersection of |  |
| :--- | :---: | :---: | :---: |
|  | PM | Todd Rd/Standish Ave-Ghilotti Ave |  |

Install a traffic signal and restripe southbound approach to provide a left-turn lane.

## Calculation of Project Share

$P=T /(T B-T E)$
where:
$\mathrm{P}=$ Equitable Share
T = Project trips during the affected peak hour
TB = Build-out volumes
TE = Existing volumes

| T | 90 | * Trips are PCE (1 truck = |
| :--- | ---: | :--- |
| TB | 1968 | 3 passenger cars) |
| TE | 1158 |  |
| P | $\mathbf{1 1 . 1 \%}$ |  |

Equitable Share (per Caltrans "Guide for the Preparation of Traffic Impact Studies")

## Appendix E

## Concept Striping Plan



## Appendix F

## Queuing Calculations

Intersection: 1: Ghillotti Ave/Standish Ave \& Todd Rd

| Movement | EB | WB | WB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | L | TR | LTR | LT | R |
| Maximum Queue (ft) | 38 | 8 | 7 | 24 | 98 | 55 |
| Average Queue (ft) | 20 | 2 | 1 | 11 | 67 | 39 |
| 95th Queue (ft) | 46 | 11 | 12 | 34 | 134 | 71 |
| Link Distance (ft) |  |  | 1164 | 265 | 442 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  | 40 |
| Storage Bay Dist (ft) | 120 | 150 |  |  | 26 | 3 |
| Storage Blk Time (\%) |  |  |  |  | 11 | 4 |

Intersection: 2: Todd Rd \& Moorland Ave

| Movement | EB | EB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | TR | L | TR |
| Maximum Queue (ft) | 17 | 2 | 3 | 84 | 56 |
| Average Queue (ft) | 6 | 0 | 1 | 53 | 31 |
| 95th Queue (ft) | 23 | 5 | 7 | 97 | 67 |
| Link Distance (ft) |  | 1164 | 151 | 516 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  | 50 |
| Storage Bay Dist (ft) | 100 |  |  | 16 | 1 |
| Storage Blk Time (\%) |  |  |  | 5 | 1 |

Intersection: 3: S Moorland Ave \& Todd Rd/US 101 South Ramps

| Movement | EB | EB | WB | WB | NB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | R | L | TR | L | R | R |
| Maximum Queue (ft) | 129 | 68 | 125 | 143 | 255 | 140 | 17 |
| Average Queue (ft) | 94 | 49 | 76 | 94 | 205 | 54 | 5 |
| 95th Queue (ft) | 148 | 73 | 132 | 157 | 298 | 173 | 25 |
| Link Distance (ft) | 151 | 151 |  | 318 | 251 | 251 |  |
| Upstream Blk Time (\%) | 1 |  |  |  | 6 | 1 |  |
| Queuing Penalty (veh) | 3 |  |  |  | 17 | 4 |  |
| Storage Bay Dist (ft) |  |  | 260 |  |  |  | 150 |
| Storage Blk Time (\%) | 57 |  |  |  |  |  |  |

Intersection: 4: Todd Rd Overcrossing \& US 101 North Off-ramp/Todd Rd

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | T | R | L | LT | T | L | $R$ | $R$ |
| Maximum Queue (ft) | 35 | 34 | 83 | 120 | 87 | 72 | 112 | 68 | 79 |
| Average Queue (ft) | 16 | 17 | 55 | 79 | 46 | 46 | 78 | 30 | 45 |
| 95th Queue (ft) | 43 | 46 | 89 | 136 | 106 | 82 | 133 | 79 | 93 |
| Link Distance (ft) | 566 |  |  | 211 | 211 | 211 |  | 264 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  | 100 | 100 |  |
| Storage Bay Dist (ft) |  | 180 | 180 |  |  |  | 4 |  | 0 |
| Storage Blk Time (\%) |  |  |  |  |  |  | 16 |  | 0 |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | EB | EB | EB | WB | WB | NB | NB | NB | NB | SB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | LT | R | L | TR | L | T | T | R | L | T | T |
| Maximum Queue ( ft$)$ | 77 | 81 | 63 | 23 | 59 | 136 | 104 | 54 | 14 | 21 | 75 | 43 |
| Average Queue $(\mathrm{tt})$ | 49 | 55 | 41 | 8 | 24 | 102 | 53 | 28 | 5 | 6 | 54 | 25 |
| 95th Queue (ft) | 85 | 87 | 72 | 27 | 61 | 155 | 114 | 60 | 17 | 25 | 90 | 58 |
| Link Distance (ft) | 211 | 211 | 211 |  | 701 |  | 573 | 573 |  |  | 1108 | 1108 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  | 65 |  | 280 |  |  | 200 | 205 |  |  |
| Storage Bay Dist (ft) |  |  |  |  | 2 |  |  |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  | 0 |  |  |  |  |  |  |  |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | SB |
| :--- | ---: |
| Directions Served | R |
| Maximum Queue (ft) | 70 |
| Average Queue (ft) | 46 |
| 95th Queue (ft) | 76 |
| Link Distance (ft) |  |
| Upstream Blk Time (\%) |  |
| Queuing Penalty (veh) |  |
| Storage Bay Dist (ft) | 205 |
| Storage Blk Time (\%) |  |

Zone Summary
Zone wide Queuing Penalty: 62

Intersection: 1: Ghillotti Ave/Standish Ave \& Todd Rd

| Movement | EB | WB | WB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | L | TR | LTR | LT | R |
| Maximum Queue (ft) | 24 | 6 | 1 | 39 | 180 | 60 |
| Average Queue (ft) | 9 | 1 | 0 | 19 | 115 | 44 |
| 95th Queue (ft) | 29 | 9 | 1 | 47 | 213 | 78 |
| Link Distance (ft) |  |  | 1164 | 265 | 442 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  | 40 |
| Storage Bay Dist (ft) | 120 | 150 |  |  | 47 | 3 |
| Storage Blk Time (\%) |  |  |  |  | 31 | 9 |

Intersection: 2: Todd Rd \& Moorland Ave

| Movement | EB | EB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | TR | L | TR |
| Maximum Queue (ft) | 31 | 80 | 7 | 148 | 62 |
| Average Queue (ft) | 13 | 20 | 2 | 108 | 30 |
| 95th Queue (ft) | 37 | 103 | 16 | 204 | 82 |
| Link Distance (ft) |  | 1164 | 151 | 516 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  | 50 |
| Storage Bay Dist (ft) | 100 | 1 | 0 | 54 | 1 |
| Storage BIk Time (\%) |  | 1 | 0 | 16 | 1 |

Intersection: 3: S Moorland Ave \& Todd Rd/US 101 South Ramps

| Movement | EB | EB | WB | WB | NB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | R | L | TR | L | R | R |
| Maximum Queue (ft) | 142 | 119 | 212 | 126 | 251 | 68 | 15 |
| Average Queue (ft) | 105 | 84 | 153 | 70 | 211 | 34 | 3 |
| 95th Queue (ft) | 169 | 145 | 259 | 144 | 304 | 94 | 18 |
| Link Distance (ft) | 151 | 151 |  | 318 | 251 | 251 |  |
| Upstream Blk Time (\%) | 4 | 2 | 0 |  | 9 | 0 |  |
| Queuing Penalty (veh) | 14 | 8 | 0 |  | 24 | 1 |  |
| Storage Bay Dist (ft) |  |  | 260 |  |  |  | 150 |
| Storage Blk Time (\%) | 57 |  | 1 | 0 |  |  |  |
| Queuing Penalty (veh) | 0 |  | 1 | 0 |  |  |  |

Intersection: 4: Todd Rd Overcrossing \& US 101 North Off-ramp/Todd Rd

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | T | R | L | LT | T | L | $R$ | R |
| Maximum Queue (ft) | 47 | 32 | 59 | 127 | 86 | 77 | 95 | 44 | 81 |
| Average Queue (ft) | 28 | 17 | 43 | 82 | 49 | 50 | 65 | 30 | 54 |
| 95th Queue (ft) | 60 | 43 | 67 | 143 | 102 | 88 | 110 | 55 | 96 |
| Link Distance (ft) | 566 |  |  | 211 | 211 | 211 |  | 264 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  | 100 |  | 100 |
| Storage Bay Dist (ft) |  | 180 | 180 |  |  |  | 2 | 0 |  |
| Storage Blk Time (\%) |  |  |  |  |  |  | 14 |  | 2 |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | EB | EB | EB | WB | WB | NB | NB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | LT | R | L | TR | L | T | T | R | L | T | T |
| Maximum Queue (ft) | 108 | 121 | 89 | 76 | 131 | 231 | 201 | 159 | 20 | 35 | 164 | 119 |
| Average Queue (ft) | 71 | 88 | 55 | 38 | 75 | 161 | 134 | 109 | 11 | 14 | 117 | 70 |
| 95th Queue (ft) | 116 | 132 | 105 | 86 | 157 | 264 | 246 | 193 | 26 | 39 | 174 | 135 |
| Link Distance (ft) | 211 | 211 | 211 |  | 701 |  | 573 | 573 |  |  | 1108 | 1108 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  | 65 |  | 280 |  |  | 200 | 205 |  |  |
| Storage Blk Time (\%) |  |  |  | 2 | 17 | 2 | 0 | 0 |  |  |  |  |
| Queuing Penalty (veh) |  |  |  | 3 | 8 | 7 | 0 | 0 |  |  |  |  |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | SB |
| :--- | ---: |
| Directions Served | R |
| Maximum Queue (ft) | 83 |
| Average Queue (ft) | 54 |
| 95th Queue (ft) | 93 |
| Link Distance (ft) |  |
| Upstream Blk Time (\%) |  |
| Queuing Penalty (veh) |  |
| Storage Bay Dist (ft) | 205 |
| Storage Blk Time (\%) |  |

Zone Summary
Zone wide Queuing Penalty: 141

Queuing and Blocking Report
AM Existing plus Mitigation
Intersection: 1: Ghillotti Ave/Standish Ave \& Todd Rd

| Movement | EB | EB | WB | WB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | TR | LTR | L | TR |
| Maximum Queue (ft) | 62 | 92 | 21 | 193 | 20 | 99 | 56 |
| Average Queue (ft) | 36 | 49 | 8 | 123 | 10 | 65 | 28 |
| 95th Queue (ft) | 74 | 100 | 27 | 223 | 33 | 112 | 73 |
| Link Distance (ft) |  | 590 |  | 1159 | 265 |  | 442 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  | 100 |  |
| Storage Bay Dist (ft) | 120 |  | 150 |  |  | 3 |  |
| Storage Blk Time (\%) | 0 | 0 |  | 4 |  | 1 |  |
| Queuing Penalty (veh) | 0 | 0 |  | 1 |  | 1 |  |

Intersection: 1: Ghillotti Ave/Standish Ave \& Todd Rd

| Movement | EB | EB | WB | WB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | TR | LTR | L | TR |
| Maximum Queue (ft) | 49 | 108 | 53 | 170 | 33 | 115 | 104 |
| Average Queue (ft) | 23 | 65 | 13 | 108 | 15 | 91 | 38 |
| 95th Queue (ft) | 56 | 126 | 79 | 192 | 42 | 132 | 119 |
| Link Distance (ft) |  | 590 |  | 1159 | 265 |  | 442 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  | 100 |
| Storage Bay Dist (ft) | 120 |  | 150 |  | 3 | 6 |  |
| Storage Blk Time (\%) |  | 1 |  | 3 |  | 4 |  |
| Queuing Penalty (veh) |  | 0 |  | 0 |  | 4 |  |

Intersection: 1: Ghillotti Ave/Standish Ave \& Todd Rd

| Movement | EB | WB | WB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | L | TR | LTR | LT | R |
| Maximum Queue (ft) | 34 | 8 | 7 | 38 | 95 | 54 |
| Average Queue (ft) | 21 | 2 | 2 | 14 | 59 | 35 |
| 95th Queue (ft) | 43 | 11 | 9 | 44 | 106 | 70 |
| Link Distance (ft) |  |  | 1164 | 265 | 442 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  | 40 |
| Storage Bay Dist (ft) | 120 | 150 |  |  | 20 | 2 |
| Storage Blk Time (\%) |  |  |  |  | 9 | 4 |

Intersection: 2: Todd Rd \& Moorland Ave

| Movement | EB | EB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | TR | L | TR |
| Maximum Queue (ft) | 15 | 25 | 5 | 99 | 51 |
| Average Queue (ft) | 3 | 6 | 1 | 59 | 27 |
| 95th Queue (ft) | 17 | 35 | 13 | 124 | 69 |
| Link Distance (ft) |  | 1164 | 151 | 516 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  | 50 |
| Storage Bay Dist (ft) | 100 |  | 0 | 20 | 0 |
| Storage Blk Time (\%) |  |  | 0 | 6 | 1 |

Intersection: 3: S Moorland Ave \& Todd Rd/US 101 South Ramps

| Movement | EB | EB | WB | WB | NB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | R | L | TR | L | R | R |
| Maximum Queue (ft) | 152 | 71 | 125 | 142 | 243 | 69 | 16 |
| Average Queue (ft) | 108 | 51 | 84 | 96 | 193 | 35 | 3 |
| 95th Queue (ft) | 168 | 77 | 148 | 163 | 278 | 93 | 21 |
| Link Distance (ft) | 151 | 151 |  | 318 | 251 | 251 |  |
| Upstream Blk Time (\%) | 2 |  |  |  | 3 | 0 |  |
| Queuing Penalty (veh) | 7 |  |  |  | 8 | 0 |  |
| Storage Bay Dist (ft) |  |  |  |  |  |  |  |
| Storage Blk Time (\%) | 55 |  |  |  |  |  |  |

Intersection: 4: Todd Rd Overcrossing \& US 101 North Off-ramp/Todd Rd

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | T | R | L | LT | T | L | $R$ | R |
| Maximum Queue (ft) | 34 | 46 | 70 | 119 | 68 | 57 | 99 | 45 | 67 |
| Average Queue (ft) | 14 | 22 | 49 | 76 | 36 | 38 | 69 | 26 | 44 |
| 95th Queue (ft) | 43 | 55 | 79 | 129 | 83 | 68 | 111 | 52 | 79 |
| Link Distance (ft) | 566 |  |  | 211 | 211 | 211 |  | 264 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  | 100 |  |
| Storage Bay Dist (ft) |  | 180 |  |  |  |  | 2 | 100 |  |
| Storage Blk Time (\%) |  |  |  |  |  |  | 9 | 0 |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  | 0 |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | EB | EB | EB | WB | WB | NB | NB | NB | NB | SB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | LT | R | L | TR | L | T | T | R | L | T | T |
| Maximum Queue (ft) | 85 | 98 | 70 | 22 | 35 | 155 | 88 | 59 | 12 | 14 | 72 | 45 |
| Average Queue (ft) | 54 | 64 | 40 | 7 | 21 | 92 | 45 | 30 | 3 | 5 | 52 | 23 |
| 95th Queue (ft) | 92 | 109 | 77 | 26 | 42 | 169 | 90 | 65 | 14 | 17 | 89 | 54 |
| Link Distance (ft) | 211 | 211 | 211 |  | 701 |  | 573 | 573 |  |  | 1108 | 1108 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  | 65 |  | 280 |  |  | 200 | 205 |  |  |
| Storage Bay Dist (ft) |  |  |  |  | 0 |  |  |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  | 0 |  |  |  |  |  |  |  |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | SB |
| :--- | ---: |
| Directions Served | R |
| Maximum Queue (ft) | 65 |
| Average Queue (ft) | 44 |
| 95th Queue (ft) | 72 |
| Link Distance (ft) |  |
| Upstream Blk Time (\%) |  |
| Queuing Penalty (veh) |  |
| Storage Bay Dist (ft) | 205 |
| Storage Blk Time (\%) |  |

Zone Summary
Zone wide Queuing Penalty: 43

Intersection: 1: Ghillotti Ave/Standish Ave \& Todd Rd

| Movement | EB | WB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | L | LTR | LT | $R$ |
| Maximum Queue (ft) | 23 | 9 | 36 | 196 | 59 |
| Average Queue (ft) | 11 | 3 | 18 | 122 | 48 |
| 95th Queue (ft) | 30 | 14 | 45 | 208 | 78 |
| Link Distance (ft) |  |  | 265 | 442 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  | 40 |
| Storage Bay Dist (ft) | 120 | 150 |  | 52 | 4 |
| Storage Blk Time (\%) |  |  |  | 34 | 10 |

Intersection: 2: Todd Rd \& Moorland Ave

| Movement | EB | EB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | TR | L | TR |
| Maximum Queue (ft) | 25 | 4 | 6 | 111 | 65 |
| Average Queue (ft) | 13 | 1 | 1 | 79 | 32 |
| 95th Queue (ft) | 33 | 10 | 9 | 137 | 77 |
| Link Distance (ft) |  | 1164 | 151 | 516 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  | 50 |
| Storage Bay Dist (ft) | 100 |  |  | 36 | 1 |
| Storage Blk Time (\%) |  |  |  | 11 | 1 |

Intersection: 3: S Moorland Ave \& Todd Rd/US 101 South Ramps

| Movement | EB | EB | WB | WB | NB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | R | L | TR | L | R | R |
| Maximum Queue (ft) | 132 | 113 | 217 | 120 | 226 | 39 | 21 |
| Average Queue (ft) | 97 | 78 | 145 | 53 | 175 | 29 | 6 |
| 95th Queue (ft) | 152 | 122 | 249 | 147 | 263 | 51 | 25 |
| Link Distance (ft) | 151 | 151 |  | 318 | 251 | 251 |  |
| Upstream Blk Time (\%) | 1 | 0 | 0 | 0 | 4 |  |  |
| Queuing Penalty (veh) | 3 | 0 | 0 | 0 | 11 |  | 150 |
| Storage Bay Dist (ft) |  |  | 260 |  |  |  |  |
| Storage Blk Time (\%) | 52 |  | 1 | 0 |  |  |  |
| Queuing Penalty (veh) | 0 |  | 2 | 1 |  |  |  |

Intersection: 4: Todd Rd Overcrossing \& US 101 North Off-ramp/Todd Rd

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | T | R | L | LT | T | L | $R$ | $R$ |
| Maximum Queue (ft) | 48 | 51 | 59 | 119 | 86 | 87 | 106 | 45 | 78 |
| Average Queue (ft) | 28 | 32 | 43 | 84 | 54 | 55 | 70 | 29 | 52 |
| 95th Queue (ft) | 59 | 64 | 66 | 138 | 98 | 91 | 117 | 55 | 90 |
| Link Distance (ft) | 566 |  |  | 211 | 211 | 211 |  | 264 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  | 100 |  | 100 |
| Storage Bay Dist (ft) |  | 180 | 180 |  |  |  | 3 | 0 |  |
| Storage Blk Time (\%) |  |  |  |  |  |  | 16 |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  | 1 |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | EB | EB | EB | WB | WB | NB | NB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SB |  |  |  |  |  |  |  |  |  |  |  |
| Directions Served | L | LT | R | L | TR | L | T | T | R | L | T |
| Maximum Queue (ft) | 109 | 130 | 91 | 54 | 103 | 239 | 295 | 260 | 48 | 34 | 147 |
| Average Queue (ft) | 74 | 91 | 59 | 29 | 62 | 173 | 171 | 145 | 16 | 14 | 110 |
| 95th Queue (ft) | 123 | 145 | 104 | 62 | 119 | 305 | 366 | 306 | 75 | 39 | 166 |
| Link Distance (ft) | 211 | 211 | 211 |  | 701 |  | 573 | 573 |  | 142 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  | 1 |  |  |  | 1108 |
| Queuing Penalty (veh) |  |  |  |  |  |  | 0 |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  | 65 |  | 280 |  |  | 200 | 205 |  |
| Storage Blk Time (\%) |  |  |  | 0 | 11 | 5 | 0 | 2 |  |  |  |
| Queuing Penalty (veh) |  |  |  | 0 | 5 | 22 | 1 | 1 |  |  | 0 |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | SB |
| :--- | ---: |
| Directions Served | R |
| Maximum Queue (ft) | 67 |
| Average Queue (ft) | 47 |
| 95th Queue (ft) | 75 |
| Link Distance (ft) |  |
| Upstream Blk Time (\%) |  |
| Queuing Penalty (veh) |  |
| Storage Bay Dist (ft) | 205 |
| Storage Blk Time (\%) |  |

Zone Summary
Zone wide Queuing Penalty: 117

Intersection: 1: Ghillotti Ave/Standish Ave \& Todd Rd

| Movement | EB | EB | WB | WB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | TR | LTR | L | TR |
| Maximum Queue (ft) | 63 | 100 | 28 | 178 | 30 | 92 | 54 |
| Average Queue (ft) | 38 | 56 | 11 | 117 | 15 | 63 | 26 |
| 95th Queue (ft) | 72 | 108 | 34 | 194 | 39 | 108 | 66 |
| Link Distance (ft) |  | 590 |  | 1159 | 265 |  | 442 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  | 150 |  |  | 100 |  |
| Storage Bay Dist (ft) | 120 |  | 150 | 3 |  | 2 |  |
| Storage Blk Time (\%) | 0 | 0 |  | 3 |  | 1 |  |
| Queuing Penalty (veh) | 0 | 0 |  | 1 |  |  |  |

Intersection: 1: Ghillotti Ave/Standish Ave \& Todd Rd

| Movement | EB | EB | WB | WB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | TR | LTR | L | TR |
| Maximum Queue (ft) | 55 | 135 | 17 | 180 | 43 | 113 | 81 |
| Average Queue (ft) | 29 | 78 | 6 | 117 | 20 | 85 | 38 |
| 95th Queue (ft) | 62 | 157 | 21 | 202 | 52 | 121 | 103 |
| Link Distance (ft) |  | 590 |  | 1159 | 265 |  | 442 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  | 150 |  |  | 100 |  |
| Storage Bay Dist (ft) | 120 |  | 150 | 3 |  | 5 |  |
| Storage Blk Time (\%) |  | 1 |  | 3 |  | 3 |  |
| Queuing Penalty (veh) |  | 1 |  | 0 |  |  |  |

Intersection: 1: Ghillotti Ave/Standish Ave \& Todd Rd

| Movement | EB | WB | WB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | L | TR | LTR | LT | R |
| Maximum Queue (ft) | 64 | 13 | 17 | 36 | 433 | 60 |
| Average Queue (ft) | 42 | 4 | 4 | 19 | 315 | 44 |
| 95th Queue (ft) | 75 | 18 | 20 | 45 | 529 | 86 |
| Link Distance (ft) |  |  | 1164 | 265 | 442 |  |
| Upstream Blk Time (\%) |  |  |  |  | 23 |  |
| Queuing Penalty (veh) |  |  |  |  | 0 |  |
| Storage Bay Dist (ft) | 120 | 150 |  |  | 91 | 40 |
| Storage Blk Time (\%) |  |  |  |  | 67 | 6 |

Intersection: 2: Todd Rd \& Moorland Ave

| Movement | EB | EB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | TR | L | TR |
| Maximum Queue (ft) | 61 | 38 | 10 | 59 | 66 |
| Average Queue (ft) | 35 | 8 | 2 | 37 | 45 |
| 95th Queue (ft) | 65 | 56 | 15 | 72 | 76 |
| Link Distance (ft) |  | 1164 | 151 | 516 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  | 50 |
| Storage Bay Dist (ft) | 100 |  |  |  | 50 |
| Storage Blk Time (\%) | 0 | 0 | 0 | 5 | 7 |
| Queuing Penalty (veh) | 0 | 0 | 0 | 6 | 3 |

Intersection: 3: S Moorland Ave \& Todd Rd/US 101 South Ramps

| Movement | EB | EB | WB | WB | NB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | R | L | TR | L | R | R |
| Maximum Queue (ft) | 145 | 67 | 179 | 182 | 267 | 113 | 30 |
| Average Queue (ft) | 108 | 48 | 120 | 118 | 213 | 52 | 8 |
| 95th Queue (ft) | 169 | 72 | 200 | 203 | 300 | 155 | 32 |
| Link Distance (ft) | 151 | 151 |  | 318 | 251 | 251 |  |
| Upstream Blk Time (\%) | 3 |  |  |  | 8 | 1 |  |
| Queuing Penalty (veh) | 8 |  |  |  | 30 | 5 |  |
| Storage Bay Dist (ft) |  |  | 260 |  |  |  | 150 |
| Storage Blk Time (\%) | 59 |  | 0 | 0 |  |  |  |
| Queuing Penalty (veh) | 0 |  | 0 | 0 |  |  |  |

Intersection: 4: Todd Rd Overcrossing \& US 101 North Off-ramp/Todd Rd

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | T | R | L | LT | T | L | $R$ | R |
| Maximum Queue (ft) | 21 | 54 | 75 | 133 | 85 | 88 | 145 | 73 | 85 |
| Average Queue (ft) | 6 | 32 | 54 | 95 | 55 | 60 | 95 | 26 | 50 |
| 95th Queue (ft) | 28 | 64 | 83 | 149 | 100 | 103 | 158 | 122 | 98 |
| Link Distance (ft) | 566 |  |  | 211 | 211 | 211 |  | 264 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  | 0 |  |
| Queuing Penalty (veh) |  |  |  |  |  |  | 100 | 0 | 100 |
| Storage Bay Dist (ft) |  | 180 | 180 |  |  |  | 7 |  | 1 |
| Storage Blk Time (\%) |  |  |  |  |  |  | 24 |  | 2 |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | EB | EB | EB | WB | WB | NB | NB | NB | NB | SB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | LT | R | L | TR | L | T | T | R | L | T | T |
| Maximum Queue (ft) | 48 | 41 | 160 | 40 | 47 | 340 | 606 | 534 | 23 | 8 | 176 | 148 |
| Average Queue (ft) | 26 | 24 | 109 | 22 | 20 | 340 | 587 | 345 | 9 | 2 | 134 | 94 |
| 95th Queue (ft) | 54 | 55 | 183 | 48 | 53 | 342 | 636 | 685 | 27 | 11 | 207 | 171 |
| Link Distance (ft) | 211 | 211 | 211 |  | 701 |  | 573 | 573 |  |  | 1108 | 1108 |
| Upstream Blk Time (\%) |  |  | 0 |  |  |  | 83 | 0 |  |  |  |  |
| Queuing Penalty (veh) |  |  | 0 |  |  |  | 0 | 0 |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  | 65 |  | 280 |  |  | 200 | 205 |  |  |
| Storage Blk Time (\%) |  |  |  | 1 | 2 | 81 |  | 0 |  |  | 0 | 0 |
| Queuing Penalty (veh) |  |  |  | 0 | 1 | 269 |  | 0 |  |  | 0 | 0 |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | SB |
| :--- | ---: |
| Directions Served | R |
| Maximum Queue (ft) | 61 |
| Average Queue (ft) | 38 |
| 95th Queue (ft) | 68 |
| Link Distance (ft) |  |
| Upstream Blk Time (\%) |  |
| Queuing Penalty (veh) |  |
| Storage Bay Dist (ft) | 205 |
| Storage Blk Time (\%) |  |

Zone Summary
Zone wide Queuing Penalty: 422

Intersection: 1: Ghillotti Ave/Standish Ave \& Todd Rd

| Movement | EB | WB | WB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | L | TR | LTR | LT | R |
| Maximum Queue (ft) | 53 | 11 | 16 | 50 | 469 | 60 |
| Average Queue (ft) | 31 | 3 | 4 | 30 | 441 | 54 |
| 95th Queue (ft) | 63 | 14 | 23 | 61 | 541 | 84 |
| Link Distance (ft) |  |  | 1164 | 265 | 442 |  |
| Upstream Blk Time (\%) |  |  |  |  | 74 |  |
| Queuing Penalty (veh) |  |  |  |  | 0 |  |
| Storage Bay Dist (ft) | 120 | 150 |  |  | 94 | 40 |
| Storage Blk Time (\%) |  |  |  |  | 187 | 34 |

Intersection: 2: Todd Rd \& Moorland Ave

| Movement | EB | EB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | TR | L | TR |
| Maximum Queue (ft) | 47 | 8 | 4 | 188 | 75 |
| Average Queue (ft) | 29 | 2 | 1 | 113 | 63 |
| 95th Queue (ft) | 57 | 17 | 7 | 277 | 91 |
| Link Distance (ft) |  | 1164 | 151 | 516 |  |
| Upstream Blk Time (\%) |  |  |  | 0 |  |
| Queuing Penalty (veh) |  |  |  | 0 |  |
| Storage Bay Dist (ft) | 100 |  |  |  | 50 |
| Storage Blk Time (\%) |  |  |  | 33 | 12 |
| Queuing Penalty (veh) |  |  |  | 62 | 11 |

Intersection: 3: S Moorland Ave \& Todd Rd/US 101 South Ramps

| Movement | EB | EB | WB | WB | NB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | R | L | TR | L | R | R |
| Maximum Queue (ft) | 123 | 116 | 192 | 136 | 199 | 35 | 3 |
| Average Queue (ft) | 81 | 71 | 133 | 70 | 145 | 22 | 1 |
| 95th Queue (ft) | 137 | 123 | 205 | 158 | 230 | 47 | 8 |
| Link Distance (ft) | 151 | 151 |  | 318 | 251 | 251 |  |
| Upstream Blk Time (\%) | 1 | 1 |  |  | 0 |  |  |
| Queuing Penalty (veh) | 3 | 4 |  |  | 1 |  |  |
| Storage Bay Dist (ft) |  |  | 260 |  |  |  | 150 |
| Storage Blk Time (\%) | 48 |  | 0 | 0 |  |  |  |
| Queuing Penalty (veh) | 0 |  | 0 | 1 |  |  |  |

Intersection: 4: Todd Rd Overcrossing \& US 101 North Off-ramp/Todd Rd

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | T | T | R | L | LT | T | L | R | R |
| Maximum Queue (ft) | 12 | 41 | 54 | 113 | 63 | 71 | 141 | 24 | 96 |
| Average Queue (ft) | 2 | 19 | 36 | 72 | 31 | 38 | 99 | 9 | 60 |
| 95th Queue (ft) | 16 | 51 | 58 | 132 | 78 | 83 | 154 | 30 | 117 |
| Link Distance (ft) | 566 |  |  | 211 | 211 | 211 |  | 264 |  |
| Upstream BIk Time (\%) |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (tt) |  | 180 | 180 |  |  |  | 100 |  | 100 |
| Storage BIk Time (\%) |  |  |  |  |  |  | 6 |  | 2 |
| Queuing Penalty (veh) |  |  |  |  |  |  | 37 |  | 12 |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | EB | EB | EB | WB | WB | NB | NB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | LT | R | L | TR | L | T | T | R | L | T | T |
| Maximum Queue (ft) | 40 | 36 | 203 | 86 | 138 | 340 | 602 | 555 | 51 | 17 | 321 | 301 |
| Average Queue (ft) | 24 | 14 | 157 | 65 | 66 | 339 | 592 | 497 | 16 | 5 | 264 | 234 |
| 95th Queue (ft) | 45 | 41 | 236 | 104 | 169 | 340 | 606 | 677 | 78 | 19 | 386 | 356 |
| Link Distance (ft) | 211 | 211 | 211 |  | 701 |  | 573 | 573 |  |  | 1108 | 1108 |
| Upstream Blk Time (\%) |  |  | 2 |  |  |  | 92 | 0 |  |  |  |  |
| Queuing Penalty (veh) |  |  | 5 |  |  |  | 0 | 0 |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  | 65 |  | 280 |  |  | 200 | 205 |  |  |
| Storage Blk Time (\%) |  |  |  | 31 | 5 | 88 |  | 3 |  |  | 22 | 13 |
| Queuing Penalty (veh) |  |  |  | 16 | 6 | 611 |  | 3 |  |  | 2 | 10 |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | SB |
| :--- | ---: |
| Directions Served | R |
| Maximum Queue (ft) | 108 |
| Average Queue (ft) | 43 |
| 95th Queue (ft) | 154 |
| Link Distance (ft) |  |
| Upstream Blk Time (\%) |  |
| Queuing Penalty (veh) |  |
| Storage Bay Dist (ft) | 205 |
| Storage Blk Time (\%) |  |

Zone Summary
Zone wide Queuing Penalty: 1005

Intersection: 1: Ghillotti Ave/Standish Ave \& Todd Rd

| Movement | EB | EB | WB | WB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | TR | LTR | L | TR |
| Maximum Queue (ft) | 145 | 204 | 53 | 328 | 39 | 120 | 139 |
| Average Queue (ft) | 99 | 124 | 18 | 247 | 17 | 96 | 58 |
| 95th Queue (ft) | 164 | 243 | 70 | 398 | 46 | 134 | 159 |
| Link Distance (ft) |  | 590 |  | 1159 | 265 |  | 442 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  | 150 |  |  | 100 |  |
| Storage Bay Dist (ft) | 120 |  | 150 | 23 |  | 11 |  |
| Storage Blk Time (\%) | 9 | 4 |  | 23 |  | 9 |  |
| Queuing Penalty (veh) | 37 | 6 |  | 6 |  |  |  |

## Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | EB | EB | EB | WB | WB | NB | NB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | LT | R | L | TR | L | L | T | TR | L | T | T |
| Maximum Queue (ft) | 51 | 55 | 154 | 47 | 40 | 284 | 356 | 253 | 153 | 6 | 174 | 139 |
| Average Queue (ft) | 29 | 29 | 114 | 29 | 20 | 191 | 242 | 147 | 51 | 2 | 126 | 81 |
| 95th Queue (ft) | 60 | 60 | 185 | 54 | 50 | 337 | 480 | 370 | 168 | 9 | 193 | 158 |
| Link Distance (ft) | 211 | 211 | 211 |  | 707 |  | 573 | 573 |  |  | 1108 | 1108 |
| Upstream Blk Time (\%) |  |  | 0 |  |  |  | 1 | 0 |  |  |  |  |
| Queuing Penalty (veh) |  |  | 0 |  |  |  | 0 | 0 |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  | 65 |  | 280 |  |  | 200 | 205 |  |  |
| Storage Blk Time (\%) |  |  |  | 1 | 0 | 3 | 11 | 1 | 0 |  | 1 |  |
| Queuing Penalty (veh) |  |  |  | 0 | 0 | 12 | 43 | 6 | 0 |  | 0 |  |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | SB |
| :--- | ---: |
| Directions Served | R |
| Maximum Queue (ft) | 57 |
| Average Queue (ft) | 35 |
| 95th Queue (ft) | 60 |
| Link Distance (ft) |  |
| Upstream Blk Time (\%) |  |
| Queuing Penalty (veh) |  |
| Storage Bay Dist (ft) | 205 |
| Storage Blk Time (\%) |  |

Zone Summary
Zone wide Queuing Penalty: 119

Intersection: 1: Ghillotti Ave/Standish Ave \& Todd Rd

| Movement | EB | EB | WB | WB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | TR | LTR | L | TR |
| Maximum Queue (ft) | 129 | 175 | 67 | 438 | 50 | 124 | 421 |
| Average Queue (ft) | 85 | 106 | 21 | 311 | 27 | 122 | 340 |
| 95th Queue (ft) | 166 | 215 | 89 | 531 | 59 | 131 | 565 |
| Link Distance (ft) |  | 590 |  | 1159 | 265 |  | 442 |
| Upstream Blk Time (\%) |  |  |  |  |  |  | 20 |
| Queuing Penalty (veh) |  |  | 150 |  |  | 100 | 0 |
| Storage Bay Dist (ft) | 120 |  | 150 | 29 |  | 53 | 3 |
| Storage Blk Time (\%) | 8 | 5 |  | 29 |  | 106 | 13 |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | EB | EB | EB | WB | WB | NB | NB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | LT | R | L | TR | L | L | T | TR | L | T | T |
| Maximum Queue (ft) | 36 | 38 | 208 | 87 | 132 | 320 | 590 | 598 | 260 | 16 | 343 | 314 |
| Average Queue (ft) | 19 | 24 | 172 | 67 | 62 | 273 | 507 | 570 | 247 | 4 | 256 | 226 |
| 95th Queue (ft) | 45 | 51 | 246 | 100 | 146 | 389 | 755 | 675 | 314 | 18 | 374 | 349 |
| Link Distance (ft) | 211 | 211 | 211 |  | 707 |  | 573 | 573 |  |  | 1108 | 1108 |
| Upstream Blk Time (\%) |  |  | 4 |  |  |  | 13 | 19 |  |  |  |  |
| Queuing Penalty (veh) |  |  | 8 |  |  |  | 0 | 0 |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  | 65 |  | 280 |  |  | 200 | 205 |  |  |
| Storage Blk Time (\%) |  |  |  | 20 | 8 | 23 | 28 | 28 | 5 |  | 19 | 9 |
| Queuing Penalty (veh) |  |  |  | 10 | 10 | 90 | 109 | 224 | 32 |  | 2 | 7 |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | SB |
| :--- | ---: |
| Directions Served | R |
| Maximum Queue (ft) | 112 |
| Average Queue (ft) | 48 |
| 95th Queue (ft) | 156 |
| Link Distance (ft) |  |
| Upstream Blk Time (\%) |  |
| Queuing Penalty (veh) |  |
| Storage Bay Dist (ft) | 205 |
| Storage Blk Time (\%) |  |

Zone Summary
Zone wide Queuing Penalty: 652

Queuing and Blocking Report
AM Existing plus Project
Intersection: 1: Ghillotti Ave/Standish Ave \& Todd Rd

| Movement | EB | WB | WB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | L | TR | LTR | LT | R |
| Maximum Queue (ft) | 34 | 25 | 3 | 49 | 97 | 57 |
| Average Queue (ft) | 19 | 9 | 1 | 30 | 65 | 34 |
| 95th Queue (ft) | 43 | 28 | 4 | 56 | 111 | 73 |
| Link Distance (ft) |  |  | 1164 | 265 | 442 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  | 40 |
| Storage Bay Dist (ft) | 120 | 150 |  |  | 24 | 2 |
| Storage Blk Time (\%) |  |  |  |  | 10 | 3 |

Intersection: 2: Todd Rd \& Moorland Ave

| Movement | EB | EB | SB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | TR |
| Maximum Queue (ft) | 17 | 28 | 120 | 67 |
| Average Queue (ft) | 4 | 6 | 71 | 29 |
| 95th Queue (ft) | 20 | 38 | 139 | 74 |
| Link Distance (ft) |  | 1164 | 516 |  |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) | 100 |  |  | 50 |
| Storage Blk Time (\%) |  | 0 | 27 | 0 |
| Queuing Penalty (veh) |  | 0 | 9 | 0 |

Intersection: 3: S Moorland Ave \& Todd Rd/US 101 South Ramps

| Movement | EB | EB | WB | WB | NB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | R | L | TR | L | R | R |
| Maximum Queue (ft) | 131 | 78 | 116 | 166 | 256 | 41 | 9 |
| Average Queue (ft) | 95 | 55 | 75 | 113 | 208 | 30 | 2 |
| 95th Queue (ft) | 147 | 86 | 141 | 185 | 290 | 52 | 15 |
| Link Distance (ft) | 151 | 151 |  | 318 | 251 | 251 |  |
| Upstream Blk Time (\%) | 1 |  |  |  | 6 |  |  |
| Queuing Penalty (veh) | 4 |  |  |  | 19 |  | 150 |
| Storage Bay Dist (ft) |  |  | 260 |  |  |  |  |
| Storage Blk Time (\%) | 53 |  |  |  |  |  |  |

Queuing and Blocking Report
AM Existing plus Project
Intersection: 4: Todd Rd Overcrossing \& US 101 North Off-ramp/Todd Rd

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB | B26 | B26 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | T | R | L | LT | T | L | $R$ | $R$ | T |  |
| Maximum Queue (ft) | 36 | 42 | 77 | 107 | 67 | 61 | 124 | 37 | 71 | 8 | 6 |
| Average Queue (ft) | 20 | 18 | 55 | 73 | 42 | 40 | 82 | 21 | 40 | 2 | 1 |
| 95th Queue (ft) | 48 | 48 | 83 | 126 | 87 | 70 | 137 | 47 | 82 | 19 | 15 |
| Link Distance (ft) | 566 |  |  | 211 | 211 | 211 |  | 264 |  | 127 | 127 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  | 100 |  | 100 |  |  |
| Storage Bay Dist (ft) |  | 180 | 180 |  |  |  | 3 |  | 0 |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  | 11 |  | 1 |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | EB | EB | EB | WB | WB | NB | NB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | LT | R | L | TR | L | T | T | R | L | T | T |
| Maximum Queue (ft) | 71 | 98 | 70 | 32 | 37 | 147 | 104 | 68 | 15 | 15 | 92 | 62 |
| Average Queue (ft) | 47 | 63 | 41 | 12 | 20 | 98 | 56 | 37 | 5 | 6 | 57 | 28 |
| 95th Queue (ft) | 82 | 109 | 78 | 37 | 46 | 158 | 112 | 82 | 18 | 20 | 103 | 71 |
| Link Distance (ft) | 211 | 211 | 211 |  | 701 |  | 573 | 573 |  |  | 1108 | 1108 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  | 65 |  | 280 |  |  | 200 | 205 |  |  |
| Storage Blk Time (\%) |  |  |  |  | 1 |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  | 0 |  |  |  |  |  |  |  |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | SB |
| :--- | ---: |
| Directions Served | R |
| Maximum Queue (ft) | 61 |
| Average Queue (ft) | 43 |
| 95th Queue (ft) | 68 |
| Link Distance (ft) |  |
| Upstream Blk Time (\%) |  |
| Queuing Penalty (veh) |  |
| Storage Bay Dist (ft) | 205 |
| Storage Blk Time (\%) |  |

Zone Summary
Zone wide Queuing Penalty: 57

Intersection: 1: Ghillotti Ave/Standish Ave \& Todd Rd

| Movement | EB | WB | WB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | L | TR | LTR | LT | R |
| Maximum Queue (ft) | 17 | 18 | 1 | 44 | 230 | 59 |
| Average Queue (ft) | 10 | 8 | 0 | 29 | 142 | 48 |
| 95th Queue (ft) | 28 | 24 | 2 | 52 | 269 | 78 |
| Link Distance (ft) |  |  | 1164 | 265 | 442 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  | 40 |
| Storage Bay Dist (ft) | 120 | 150 |  |  | 56 | 4 |
| Storage Blk Time (\%) |  |  |  |  | 36 | 10 |

Intersection: 2: Todd Rd \& Moorland Ave

| Movement | EB | EB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | TR | L | TR |
| Maximum Queue (ft) | 29 | 37 | 2 | 269 | 75 |
| Average Queue (ft) | 13 | 8 | 0 | 186 | 39 |
| 95th Queue (ft) | 35 | 60 | 5 | 387 | 95 |
| Link Distance (ft) |  | 1164 | 151 | 516 |  |
| Upstream Blk Time (\%) |  |  |  | 4 |  |
| Queuing Penalty (veh) |  |  |  | 0 |  |
| Storage Bay Dist (ft) | 100 |  |  |  | 50 |
| Storage Blk Time (\%) |  | 1 |  | 74 | 0 |
| Queuing Penalty (veh) |  | 0 |  | 24 | 1 |

Intersection: 3: S Moorland Ave \& Todd Rd/US 101 South Ramps

| Movement | EB | EB | WB | WB | B24 | NB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | R | L | TR | T | L | R | R |
| Maximum Queue (ft) | 135 | 111 | 219 | 139 | 50 | 249 | 83 | 14 |
| Average Queue (ft) | 105 | 83 | 156 | 89 | 16 | 219 | 42 | 3 |
| 95th Queue (ft) | 160 | 140 | 284 | 271 | 131 | 292 | 135 | 20 |
| Link Distance (ft) | 151 | 151 |  | 318 | 411 | 251 | 251 |  |
| Upstream Blk Time (\%) | 3 | 2 | 1 | 4 | 1 | 8 | 1 |  |
| Queuing Penalty (veh) | 11 | 7 | 0 | 0 | 0 | 25 | 2 |  |
| Storage Bay Dist (ft) |  |  | 260 |  |  |  |  | 150 |
| Storage Blk Time (\%) | 56 |  | 7 | 2 |  |  |  |  |
| Queuing Penalty (veh) | 0 |  | 11 | 6 |  |  |  |  |

Intersection: 4: Todd Rd Overcrossing \& US 101 North Off-ramp/Todd Rd

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB | B26 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | T | R | L | LT | T | L | $R$ | R |  |
| Maximum Queue (ft) | 54 | 58 | 70 | 113 | 100 | 82 | 105 | 47 | 85 | 5 |
| Average Queue (ft) | 28 | 22 | 46 | 78 | 52 | 54 | 71 | 30 | 56 | 1 |
| 95th Queue (ft) | 64 | 63 | 75 | 134 | 111 | 91 | 118 | 57 | 94 | 13 |
| Link Distance (ft) | 566 |  |  | 211 | 211 | 211 |  | 264 |  | 127 |
| Upstream Blk Time (\%) |  |  |  | 0 |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  | 0 |  |  | 100 |  | 100 |  |
| Storage Bay Dist (ft) |  | 180 | 180 |  |  |  | 3 |  | 0 |  |
| Storage Blk Time (\%) |  |  |  |  |  |  | 17 |  | 1 |  |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | EB | EB | EB | WB | WB | NB | NB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | LT | R | L | TR | L | T | T | R | L | T | T |
| Maximum Queue (ft) | 120 | 137 | 92 | 75 | 117 | 214 | 250 | 234 | 50 | 48 | 169 | 142 |
| Average Queue (ft) | 79 | 93 | 59 | 38 | 64 | 167 | 161 | 133 | 16 | 22 | 123 | 80 |
| 95th Queue (ft) | 136 | 159 | 102 | 82 | 135 | 268 | 296 | 257 | 77 | 60 | 186 | 156 |
| Link Distance (ft) | 211 | 211 | 211 |  | 701 |  | 573 | 573 |  |  | 1108 | 1108 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  | 65 |  | 280 |  |  | 200 | 205 |  |  |
| Storage Blk Time (\%) |  |  |  | 3 | 14 | 2 | 0 | 1 |  |  | 0 |  |
| Queuing Penalty (veh) |  |  |  | 4 | 7 | 12 | 1 | 1 |  |  | 0 |  |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | SB |
| :--- | ---: |
| Directions Served | R |
| Maximum Queue (ft) | 79 |
| Average Queue (ft) | 53 |
| 95th Queue (ft) | 88 |
| Link Distance (ft) |  |
| Upstream Blk Time (\%) |  |
| Queuing Penalty (veh) |  |
| Storage Bay Dist (ft) | 205 |
| Storage Blk Time (\%) |  |

Zone Summary
Zone wide Queuing Penalty: 176

Intersection: 1: Ghillotti Ave/Standish Ave \& Todd Rd

| Movement | EB | EB | WB | WB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | TR | LTR | L | TR |
| Maximum Queue (ft) | 90 | 104 | 97 | 216 | 51 | 82 | 39 |
| Average Queue (ft) | 51 | 60 | 41 | 148 | 30 | 53 | 20 |
| 95th Queue (ft) | 99 | 119 | 128 | 253 | 58 | 91 | 47 |
| Link Distance (ft) |  | 590 |  | 1159 | 265 |  | 442 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  | 100 |  |
| Storage Bay Dist (ft) | 120 |  | 150 |  |  | 1 |  |
| Storage Blk Time (\%) | 1 | 0 |  | 9 |  | 1 |  |
| Queuing Penalty (veh) | 2 | 0 |  | 5 |  | 0 |  |

Intersection: 1: Ghillotti Ave/Standish Ave \& Todd Rd

| Movement | EB | EB | WB | WB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | TR | LTR | L | TR |
| Maximum Queue (ft) | 49 | 157 | 61 | 169 | 53 | 114 | 93 |
| Average Queue (ft) | 25 | 104 | 30 | 109 | 35 | 85 | 42 |
| 95th Queue (ft) | 54 | 174 | 80 | 207 | 60 | 129 | 113 |
| Link Distance (ft) |  | 590 |  | 1159 | 265 |  | 442 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  | 100 |
| Storage Bay Dist (ft) | 120 |  | 150 |  |  |  |  |
| Storage Blk Time (\%) |  | 5 |  | 4 |  | 7 |  |
| Queuing Penalty (veh) |  | 2 |  | 2 |  | 5 |  |

Intersection: 1: Ghillotti Ave/Standish Ave \& Todd Rd

| Movement | EB | WB | WB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | L | TR | LTR | LT | R |
| Maximum Queue (ft) | 32 | 23 | 2 | 59 | 125 | 57 |
| Average Queue (ft) | 17 | 12 | 0 | 35 | 71 | 36 |
| 95th Queue (ft) | 39 | 30 | 4 | 68 | 147 | 71 |
| Link Distance (ft) |  |  | 1164 | 265 | 442 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  | 40 |
| Storage Bay Dist (ft) | 120 | 150 |  |  | 27 | 2 |
| Storage Blk Time (\%) |  |  |  | 12 | 3 |  |

Intersection: 2: Todd Rd \& Moorland Ave

| Movement | EB | EB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | TR | L | TR |
| Maximum Queue (ft) | 19 | 50 | 2 | 115 | 61 |
| Average Queue (ft) | 6 | 15 | 0 | 73 | 31 |
| 95th Queue (ft) | 25 | 86 | 5 | 137 | 73 |
| Link Distance (ft) |  | 1164 | 151 | 516 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  | 50 |
| Storage Bay Dist (ft) | 100 |  |  | 29 | 1 |
| Storage Blk Time (\%) |  | 1 |  | 9 | 1 |

Intersection: 3: S Moorland Ave \& Todd Rd/US 101 South Ramps

| Movement | EB | EB | WB | WB | NB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | R | L | TR | L | R | R |
| Maximum Queue (ft) | 149 | 68 | 127 | 193 | 262 | 74 | 24 |
| Average Queue (ft) | 112 | 49 | 86 | 116 | 212 | 36 | 6 |
| 95th Queue (ft) | 177 | 75 | 146 | 212 | 307 | 105 | 26 |
| Link Distance (ft) | 151 | 151 |  | 318 | 251 | 251 |  |
| Upstream Blk Time (\%) | 4 |  |  |  | 11 | 0 |  |
| Queuing Penalty (veh) | 14 |  |  |  | 31 | 0 |  |
| Storage Bay Dist (ft) |  |  | 260 |  |  |  | 150 |
| Storage Blk Time (\%) | 57 |  |  | 0 |  |  |  |
| Queuing Penalty (veh) | 0 |  |  | 1 |  |  |  |

Intersection: 4: Todd Rd Overcrossing \& US 101 North Off-ramp/Todd Rd

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | T | R | L | LT | T | L | $R$ | R |
| Maximum Queue (ft) | 38 | 44 | 86 | 111 | 76 | 65 | 123 | 76 | 62 |
| Average Queue (ft) | 21 | 20 | 54 | 82 | 42 | 42 | 85 | 32 | 41 |
| 95th Queue (ft) | 49 | 53 | 92 | 124 | 90 | 79 | 139 | 103 | 74 |
| Link Distance (ft) | 566 |  |  | 211 | 211 | 211 |  | 264 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  | 0 |  |
| Queuing Penalty (veh) |  |  |  |  |  |  | 100 | 1 |  |
| Storage Bay Dist (ft) |  | 180 | 180 |  |  |  | 5 |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  | 20 |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | EB | EB | EB | WB | WB | NB | NB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | LT | R | L | TR | L | T | T | R | L | T | T |
| Maximum Queue (ft) | 92 | 91 | 79 | 29 | 51 | 145 | 86 | 54 | 13 | 20 | 87 | 42 |
| Average Queue (ft) | 55 | 56 | 48 | 10 | 29 | 107 | 49 | 31 | 4 | 6 | 59 | 22 |
| 95th Queue (ft) | 99 | 105 | 86 | 33 | 58 | 171 | 97 | 64 | 17 | 22 | 97 | 49 |
| Link Distance (ft) | 211 | 211 | 211 |  | 701 |  | 573 | 573 |  |  | 1108 | 1108 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  | 65 |  | 280 |  |  | 200 | 205 |  |  |
| Storage Blk Time (\%) |  |  |  |  | 1 |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  | 0 |  |  |  |  |  |  |  |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | SB |
| :--- | ---: |
| Directions Served | R |
| Maximum Queue (ft) | 65 |
| Average Queue (ft) | 42 |
| 95th Queue (ft) | 71 |
| Link Distance (ft) |  |
| Upstream Blk Time (\%) |  |
| Queuing Penalty (veh) |  |
| Storage Bay Dist (ft) | 205 |
| Storage Blk Time (\%) |  |

Zone Summary
Zone wide Queuing Penalty: 92

Intersection: 1: Ghillotti Ave/Standish Ave \& Todd Rd

| Movement | EB | WB | WB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | L | TR | LTR | LT | R |
| Maximum Queue (ft) | 22 | 20 | 3 | 51 | 219 | 60 |
| Average Queue (ft) | 9 | 8 | 1 | 35 | 132 | 48 |
| 95th Queue (ft) | 29 | 25 | 5 | 61 | 270 | 81 |
| Link Distance (ft) |  |  | 1164 | 265 | 442 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |
| Storage Bay Dist (ft) | 120 | 150 |  |  | 53 | 4 |
| Storage Blk Time (\%) |  |  |  |  | 35 | 10 |

Intersection: 2: Todd Rd \& Moorland Ave

| Movement | EB | EB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | TR | L | TR |
| Maximum Queue (ft) | 45 | 136 | 6 | 191 | 65 |
| Average Queue (ft) | 16 | 43 | 1 | 118 | 29 |
| 95th Queue (ft) | 52 | 197 | 14 | 254 | 77 |
| Link Distance (ft) |  | 1164 | 151 | 516 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  | 50 |
| Storage Bay Dist (ft) | 100 |  |  |  | 50 |
| Storage BIk Time (\%) |  | 5 | 0 | 52 | 0 |
| Queuing Penalty (veh) |  | 2 | 0 | 17 | 0 |

Intersection: 3: S Moorland Ave \& Todd Rd/US 101 South Ramps

| Movement | EB | EB | WB | WB | B24 | NB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | R | L | TR | T | L | R | R |
| Maximum Queue (ft) | 143 | 116 | 198 | 115 | 22 | 254 | 91 | 21 |
| Average Queue (ft) | 112 | 90 | 150 | 69 | 7 | 205 | 40 | 5 |
| 95th Queue (ft) | 166 | 145 | 259 | 186 | 69 | 293 | 122 | 22 |
| Link Distance (ft) | 151 | 151 |  | 318 | 411 | 251 | 251 |  |
| Upstream Blk Time (\%) | 4 | 3 | 1 | 3 |  | 9 | 1 |  |
| Queuing Penalty (veh) | 17 | 14 | 0 | 0 |  | 26 | 1 |  |
| Storage Bay Dist (ft) |  |  | 260 |  |  |  |  | 150 |
| Storage Blk Time (\%) | 55 |  | 4 |  |  |  |  |  |
| Queuing Penalty (veh) | 0 |  | 6 |  |  |  |  |  |

Intersection: 4: Todd Rd Overcrossing \& US 101 North Off-ramp/Todd Rd

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | T | R | L | LT | T | L | R | R |
| Maximum Queue (ft) | 50 | 42 | 63 | 153 | 86 | 88 | 111 | 72 | 84 |
| Average Queue (ft) | 29 | 26 | 45 | 99 | 52 | 58 | 77 | 36 | 51 |
| 95th Queue (ft) | 68 | 54 | 74 | 175 | 93 | 97 | 130 | 86 | 98 |
| Link Distance (ft) | 566 |  |  | 211 | 211 | 211 |  | 264 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  | 100 |  | 100 |
| Storage Bay Dist (ft) |  | 180 | 180 |  |  |  | 3 | 0 |  |
| Storage Blk Time (\%) |  |  |  |  |  |  | 20 | 0 |  |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | EB | EB | EB | WB | WB | NB | NB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | LT | R | L | TR | L | T | T | R | L | T | T |
| Maximum Queue (ft) | 120 | 138 | 75 | 69 | 104 | 238 | 220 | 204 | 22 | 39 | 148 | 116 |
| Average Queue (ft) | 80 | 98 | 50 | 34 | 64 | 174 | 157 | 129 | 10 | 19 | 111 | 71 |
| 95th Queue (ft) | 141 | 168 | 83 | 73 | 119 | 292 | 343 | 290 | 28 | 48 | 170 | 142 |
| Link Distance (ft) | 211 | 211 | 211 |  | 701 |  | 573 | 573 |  |  | 1108 | 1108 |
| Upstream Blk Time (\%) | 0 | 0 |  |  |  |  | 1 |  |  |  |  |  |
| Queuing Penalty (veh) | 0 | 0 |  |  |  |  | 0 |  |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  | 65 |  | 280 |  |  | 200 | 205 |  |  |
| Storage Blk Time (\%) |  |  |  | 2 | 11 | 5 |  | 0 |  |  | 0 |  |
| Queuing Penalty (veh) |  |  |  | 3 | 5 | 22 |  | 0 |  |  | 0 |  |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | SB |
| :--- | ---: |
| Directions Served | R |
| Maximum Queue (ft) | 81 |
| Average Queue (ft) | 54 |
| 95th Queue (ft) | 89 |
| Link Distance (ft) |  |
| Upstream Blk Time (\%) |  |
| Queuing Penalty (veh) |  |
| Storage Bay Dist (ft) | 205 |
| Storage Blk Time (\%) |  |

Zone Summary
Zone wide Queuing Penalty: 179

Intersection: 1: Ghillotti Ave/Standish Ave \& Todd Rd

| Movement | EB | EB | WB | WB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | TR | LTR | L | TR |
| Maximum Queue (ft) | 59 | 108 | 53 | 180 | 55 | 88 | 43 |
| Average Queue (ft) | 41 | 65 | 31 | 126 | 34 | 62 | 24 |
| 95th Queue (ft) | 65 | 122 | 61 | 208 | 67 | 105 | 53 |
| Link Distance (ft) |  | 590 |  | 1159 | 265 |  | 442 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  | 150 |  |  | 100 |  |
| Storage Bay Dist (ft) | 120 |  | 150 | 5 |  | 2 |  |
| Storage Blk Time (\%) |  | 1 |  | 5 |  | 1 |  |
| Queuing Penalty (veh) |  | 1 |  |  |  |  |  |

Intersection: 1: Ghillotti Ave/Standish Ave \& Todd Rd

| Movement | EB | EB | WB | WB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | TR | LTR | L | TR |
| Maximum Queue (ft) | 66 | 125 | 58 | 171 | 61 | 118 | 135 |
| Average Queue (ft) | 31 | 80 | 32 | 108 | 36 | 97 | 59 |
| 95th Queue (ft) | 77 | 146 | 65 | 198 | 69 | 141 | 170 |
| Link Distance (ft) |  | 590 |  | 1159 | 265 |  | 442 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |
| Storage Bay Dist (ft) | 120 |  | 150 |  |  | 100 |  |
| Storage Blk Time (\%) |  | 2 |  | 3 |  | 10 |  |
| Queuing Penalty (veh) |  | 1 |  | 2 |  | 7 |  |

Queuing and Blocking Report
AM Future plus Project
Intersection: 1: Ghillotti Ave/Standish Ave \& Todd Rd

| Movement | EB | WB | WB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | L | TR | LTR | LT | R |
| Maximum Queue (ft) | 74 | 23 | 9 | 53 | 409 | 60 |
| Average Queue (ft) | 42 | 10 | 3 | 37 | 306 | 43 |
| 95th Queue (ft) | 83 | 28 | 15 | 63 | 520 | 85 |
| Link Distance (ft) |  |  | 1164 | 265 | 442 |  |
| Upstream Blk Time (\%) |  |  |  |  | 19 |  |
| Queuing Penalty (veh) |  |  |  |  | 0 |  |
| Storage Bay Dist (ft) | 120 | 150 |  |  |  | 40 |
| Storage Blk Time (\%) | 0 |  |  |  | 91 | 3 |
| Queuing Penalty (veh) | 0 |  |  |  | 67 | 7 |

Intersection: 2: Todd Rd \& Moorland Ave

| Movement | EB | EB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | TR | L | TR |
| Maximum Queue (ft) | 74 | 79 | 17 | 105 | 71 |
| Average Queue (ft) | 41 | 29 | 4 | 49 | 49 |
| 95th Queue (ft) | 86 | 142 | 17 | 140 | 81 |
| Link Distance (ft) |  | 1164 | 151 | 516 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  | 50 |
| Storage Bay Dist (ft) | 100 |  |  | 14 | 8 |
| Storage Blk Time (\%) | 1 | 2 |  | 16 | 4 |

Intersection: 3: S Moorland Ave \& Todd Rd/US 101 South Ramps

| Movement | EB | EB | WB | WB | NB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | R | L | TR | L | R | R |
| Maximum Queue (ft) | 154 | 71 | 192 | 205 | 266 | 114 | 23 |
| Average Queue (ft) | 121 | 49 | 124 | 141 | 234 | 49 | 7 |
| 95th Queue (ft) | 177 | 82 | 216 | 227 | 296 | 140 | 28 |
| Link Distance (ft) | 151 | 151 |  | 318 | 251 | 251 |  |
| Upstream Blk Time (\%) | 7 |  |  |  | 12 | 1 |  |
| Queuing Penalty (veh) | 23 |  |  |  | 46 | 5 |  |
| Storage Bay Dist (ft) |  |  | 260 |  |  |  | 150 |
| Storage Blk Time (\%) | 62 |  | 0 | 0 |  |  |  |
| Queuing Penalty (veh) | 0 |  | 1 | 1 |  |  |  |

Queuing and Blocking Report
AM Future plus Project
Intersection: 4: Todd Rd Overcrossing \& US 101 North Off-ramp/Todd Rd

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | T | R | L | LT | T | L | $R$ | $R$ |
| Maximum Queue (ft) | 19 | 48 | 66 | 138 | 96 | 85 | 136 | 46 | 75 |
| Average Queue (ft) | 4 | 27 | 50 | 93 | 56 | 60 | 96 | 12 | 46 |
| 95th Queue (ft) | 25 | 56 | 77 | 152 | 108 | 102 | 153 | 63 | 84 |
| Link Distance (ft) | 566 |  |  | 211 | 211 | 211 |  | 264 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  | 100 |  | 100 |
| Storage Bay Dist (ft) |  | 180 | 180 |  |  |  | 7 | 0 |  |
| Storage Blk Time (\%) |  |  |  |  |  |  | 25 |  | 1 |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | EB | EB | EB | WB | WB | NB | NB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SB |  |  |  |  |  |  |  |  |  |  |  |
| Directions Served | L | LT | R | L | TR | L | T | T | R | L | T |
| Maximum Queue (ft) | 44 | 38 | 154 | 46 | 52 | 340 | 615 | 517 | 31 | 14 | 169 |
| Average Queue (ft) | 29 | 21 | 109 | 24 | 21 | 337 | 581 | 300 | 10 | 6 | 126 |
| 95th Queue (ft) | 54 | 46 | 170 | 53 | 66 | 365 | 698 | 646 | 35 | 19 | 185 |
| Link Distance (ft) | 211 | 211 | 211 |  | 701 |  | 573 | 573 |  | 162 |  |
| Upstream Blk Time (\%) |  |  | 0 |  |  |  | 80 | 0 |  |  | 1108 |
| Queuing Penalty (veh) |  |  | 0 |  |  |  | 0 | 0 |  |  |  |
| Storage Bay Dist (ft) |  |  |  | 65 |  | 280 |  |  | 200 | 205 |  |
| Storage Blk Time (\%) |  |  |  | 1 | 2 | 79 |  | 0 |  |  |  |
| Queuing Penalty (veh) |  |  |  | 0 | 1 | 260 |  | 0 |  |  |  |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | SB |
| :--- | ---: |
| Directions Served | R |
| Maximum Queue (ft) | 57 |
| Average Queue (ft) | 39 |
| 95th Queue (ft) | 64 |
| Link Distance (ft) |  |
| Upstream Blk Time (\%) |  |
| Queuing Penalty (veh) |  |
| Storage Bay Dist (ft) | 205 |
| Storage Blk Time (\%) |  |

Zone Summary
Zone wide Queuing Penalty: 463

Intersection: 1: Ghillotti Ave/Standish Ave \& Todd Rd

| Movement | EB | WB | WB | NB | SB | SB |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | L | TR | LTR | LT | R |
| Average Queue (ft) | 32 | 10 | 1 | 37 | 462 | 54 |
| Link Distance (ft) |  |  | 1164 | 265 | 442 |  |
| Queuing Penalty (veh) |  |  |  |  | 0 |  |
| Storage Blk Time (\%) | 0 |  |  |  | 96 | 9 |

Intersection: 2: Todd Rd \& Moorland Ave

| Movement | EB | EB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | TR | L | TR |
| Maximum Queue (ft) | 50 | 16 | 12 | 184 | 74 |
| Average Queue (ft) | 28 | 3 | 2 | 99 | 63 |
| 95th Queue (ft) | 58 | 37 | 16 | 230 | 86 |
| Link Distance (ft) |  | 1164 | 151 | 516 |  |
| Upstream BIk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  | 50 |
| Storage Bay Dist (ft) | 100 |  |  |  | 50 |
| Storage BIk Time (\%) |  | 0 | 0 | 33 | 9 |
| Queuing Penalty (veh) |  | 1 | 0 | 61 | 9 |

Intersection: 3: S Moorland Ave \& Todd Rd/US 101 South Ramps

| Movement | EB | EB | WB | WB | NB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | R | L | TR | L | R | R |
| Maximum Queue (ft) | 136 | 106 | 221 | 149 | 222 | 39 | 17 |
| Average Queue (ft) | 92 | 73 | 169 | 75 | 146 | 28 | 3 |
| 95th Queue (ft) | 150 | 119 | 248 | 161 | 238 | 48 | 19 |
| Link Distance (ft) | 151 | 151 |  | 318 | 251 | 251 |  |
| Upstream Blk Time (\%) | 2 | 0 |  |  | 1 |  |  |
| Queuing Penalty (veh) | 7 | 1 |  |  | 3 |  |  |
| Storage Bay Dist (ft) |  |  | 260 |  |  |  | 150 |
| Storage Blk Time (\%) | 54 |  | 0 | 0 |  |  |  |
| Queuing Penalty (veh) | 0 |  | 0 | 0 |  |  |  |

Intersection: 4: Todd Rd Overcrossing \& US 101 North Off-ramp/Todd Rd

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB | B26 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | T | R | L | LT | T | L | R | R |  |
| Maximum Queue ( ft$)$ | 6 | 39 | 52 | 114 | 74 | 64 | 136 | 73 | 121 | 5 |
| Average Queue $(\mathrm{ft})$ | 2 | 19 | 36 | 70 | 37 | 38 | 102 | 23 | 72 | 1 |
| 95th Queue (ft) | 12 | 49 | 57 | 131 | 85 | 74 | 156 | 111 | 138 | 14 |
| Link Distance (ft) | 566 |  |  | 211 | 211 | 211 |  | 264 |  | 127 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  | 100 |  | 100 |  |
| Storage Bay Dist ( ft$)$ |  | 180 | 180 |  |  |  | 8 |  | 3 |  |
| Storage Blk Time (\%) |  |  |  |  |  |  | 49 | 21 |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | EB | EB | EB | WB | WB | NB | NB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | LT | R | L | TR | L | T | T | R | L | T | T |
| Maximum Queue (ft) | 39 | 38 | 217 | 89 | 141 | 340 | 598 | 562 | 91 | 12 | 377 | 348 |
| Average Queue (ft) | 21 | 17 | 176 | 73 | 84 | 337 | 583 | 472 | 23 | 3 | 297 | 266 |
| 95th Queue (ft) | 46 | 44 | 249 | 104 | 197 | 370 | 667 | 720 | 120 | 13 | 420 | 396 |
| Link Distance (ft) | 211 | 211 | 211 |  | 701 |  | 573 | 573 |  |  | 1108 | 1108 |
| Upstream Blk Time (\%) |  |  | 6 |  |  |  | 91 | 0 |  |  |  |  |
| Queuing Penalty (veh) |  |  | 12 |  |  |  | 0 | 0 |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  | 65 |  | 280 |  |  | 200 | 205 |  |  |
| Storage Blk Time (\%) |  |  |  | 42 | 5 | 86 |  | 5 |  |  | 30 | 18 |
| Queuing Penalty (veh) |  |  |  | 22 | 6 | 596 |  | 5 |  |  | 3 | 14 |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | SB |
| :--- | ---: |
| Directions Served | R |
| Maximum Queue (ft) | 218 |
| Average Queue (ft) | 94 |
| 95th Queue (ft) | 269 |
| Link Distance (ft) |  |
| Upstream Blk Time (\%) |  |
| Queuing Penalty (veh) |  |
| Storage Bay Dist (ft) | 205 |
| Storage Blk Time (\%) |  |
| Queuing Penalty (veh) |  |

Zone Summary
Zone wide Queuing Penalty: 1040

Intersection: 1: Ghillotti Ave/Standish Ave \& Todd Rd

| Movement | EB | EB | WB | WB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | TR | LTR | L | TR |
| Maximum Queue (ft) | 134 | 190 | 176 | 392 | 55 | 116 | 158 |
| Average Queue (ft) | 96 | 123 | 82 | 263 | 32 | 96 | 69 |
| 95th Queue (ft) | 153 | 229 | 216 | 432 | 66 | 135 | 193 |
| Link Distance (ft) |  | 590 |  | 1159 | 265 |  | 442 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  | 150 |  |  | 100 |  |
| Storage Bay Dist (ft) | 120 |  | 150 | 27 |  | 14 | 0 |
| Storage Blk Time (\%) | 7 | 8 |  | 27 |  | 10 | 0 |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | EB | EB | EB | WB | WB | NB | NB | NB | NB | SB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | LT | R | L | TR | L | L | T | TR | L | T | T |
| Maximum Queue (ft) | 55 | 57 | 161 | 42 | 55 | 281 | 355 | 217 | 170 | 12 | 168 | 136 |
| Average Queue (ft) | 30 | 31 | 106 | 26 | 23 | 207 | 235 | 135 | 65 | 4 | 129 | 86 |
| 95th Queue (ft) | 65 | 70 | 181 | 53 | 63 | 336 | 407 | 257 | 190 | 16 | 196 | 159 |
| Link Distance (ft) | 211 | 211 | 211 |  | 707 |  | 573 | 573 |  |  | 1108 | 1108 |
| Upstream Blk Time (\%) |  |  | 0 |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  | 0 |  |  |  |  |  | 200 | 205 |  |  |
| Storage Bay Dist (ft) |  |  |  | 65 |  | 280 |  |  | 200 | 205 | 0 | 0 |
| Storage Blk Time (\%) |  |  |  | 1 | 2 | 2 | 7 | 2 | 0 |  | 0 | 0 |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | SB |
| :--- | ---: |
| Directions Served | R |
| Maximum Queue (ft) | 60 |
| Average Queue (ft) | 41 |
| 95th Queue (ft) | 69 |
| Link Distance (ft) |  |
| Upstream Blk Time (\%) |  |
| Queuing Penalty (veh) |  |
| Storage Bay Dist (ft) | 205 |
| Storage Blk Time (\%) |  |

Zone Summary
Zone wide Queuing Penalty: 112

Intersection: 1: Ghillotti Ave/Standish Ave \& Todd Rd

| Movement | EB | EB | WB | WB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | TR | LTR | L | TR |
| Maximum Queue (ft) | 143 | 247 | 164 | 447 | 78 | 124 | 440 |
| Average Queue (ft) | 94 | 155 | 66 | 315 | 47 | 123 | 341 |
| 95th Queue (ft) | 177 | 286 | 175 | 568 | 86 | 127 | 553 |
| Link Distance (ft) |  | 590 |  | 1159 | 265 |  | 442 |
| Upstream Blk Time (\%) |  |  |  |  |  |  | 16 |
| Queuing Penalty (veh) |  |  |  |  |  | 100 | 0 |
| Storage Bay Dist (ft) | 120 |  | 150 |  |  | 54 | 2 |
| Storage Blk Time (\%) | 13 | 11 |  | 29 |  | 54 | 10 |
| Queuing Penalty (veh) | 46 | 12 |  | 19 |  | 109 | 10 |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | EB | EB | EB | WB | WB | NB | NB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | LT | R | L | TR | L | L | T | TR | L | T | T |
| Maximum Queue (ft) | 34 | 48 | 212 | 89 | 164 | 335 | 592 | 597 | 260 | 44 | 344 | 305 |
| Average Queue (ft) | 17 | 21 | 170 | 78 | 97 | 285 | 524 | 553 | 245 | 11 | 276 | 238 |
| 95th Queue (ft) | 41 | 54 | 251 | 101 | 204 | 392 | 737 | 708 | 325 | 80 | 385 | 363 |
| Link Distance (ft) | 211 | 211 | 211 |  | 707 |  | 573 | 573 |  |  | 1108 | 1108 |
| Upstream Blk Time (\%) |  |  | 5 |  |  |  | 14 | 25 |  |  |  |  |
| Queuing Penalty (veh) |  |  | 10 |  |  |  | 0 | 0 |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  | 65 |  | 280 |  |  | 200 | 205 |  |  |
| Storage Blk Time (\%) |  |  |  | 38 | 7 | 17 | 31 | 30 | 7 |  | 24 | 13 |
| Queuing Penalty (veh) |  |  |  | 20 | 9 | 64 | 121 | 241 | 47 |  | 2 | 10 |

Intersection: 5: Santa Rosa Ave \& Todd Rd

| Movement | SB |
| :--- | ---: |
| Directions Served | R |
| Maximum Queue (ft) | 174 |
| Average Queue (ft) | 58 |
| 95th Queue (ft) | 195 |
| Link Distance (ft) |  |
| Upstream Blk Time (\%) |  |
| Queuing Penalty (veh) |  |
| Storage Bay Dist (ft) | 205 |
| Storage Blk Time (\%) |  |

Zone Summary
Zone wide Queuing Penalty: 721

## Appendix G

Speed Survey Data

*Note: All speeds in miles per hour (mph).


[^0]:    ${ }^{1}$ Bay Area Air Quality Management District. 2011. BAAQMD CEQA Air Quality Guidelines. May.

[^1]:    ${ }^{2}$ BAAQMD’s Permit Handbook source specific guidance is available online at http://hank.baaqmd.gov/pmt/handbook/rev02/PH_00_05_11_07.pdf.

[^2]:    ${ }^{3}$ Bay Area Air Quality Management District (BAAQMD), 2012, Recommended Methods for Screening and Modeling Local Risks and Hazards, Version 3.0. May.

[^3]:    Mitigated Construction Off-Site

[^4]:    ${ }^{4}$ OEHHA, 2015. Air Toxics Hot Spots Program Risk Assessment Guidelines, The Air Toxics Hot Spots Program Guidance Manual for Preparation of Health Risk Assessments. Office of Environmental Health Hazard Assessment. February.
    ${ }^{5}$ CARB, 2015. Risk Management Guidance for Stationary Sources of Air Toxics. July 23.
    ${ }^{6}$ BAAQMD, 2016. BAAQMD Air Toxics NSR Program Health Risk Assessment ( HRA) Guidelines. January 2016.

[^5]:    Third trimester of pregnancy

[^6]:    Third trimester of pregnancy

[^7]:    Ghilotti Construction Yard TIS

